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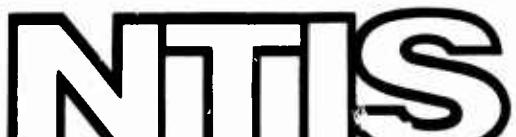
**HORIZONTAL-GRADIENT ACOUSTICAL RAY-
TRACE PROGRAM TRIMAIN**

B. G. Roberts, Jr.

**Naval Research Laboratory
Washington, D. C.**

16 December 1974

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) <p>Interest has arisen in the last few years to develop analytical models of the undersea acoustic environment which are suitable for use on digital computers. To realistically represent the sound-field structure which exists in the ocean, one must consider the variation of sound speed in two dimensions: depth and range. A computer program, TRIMAIN, was written in Fortran IV in which the sound-speed field for a given region is divided into triangular segments of the range-and-depth plane. In each segment the sound-speed field, in terms of $(1/c)^2$, is defined by a linear function of range and depth. The ray paths for this field become parabolic</p>																						

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19. (Cont'd)

Caustics
Spreading loss
Inhomogeneous media
Multiple profiles
Linear segmented bottom
Calcomp plotting
Computer applications

20. (Cont'd)

trajectories in each triangular segment. All the rays are advanced to a given range at one time, and an interpolation in depth is performed to arrive at the intensity values. Four types of intensity calculations are available: a completely random phase summation, a completely coherent phase summation, a statistical influence over depth, and an average over a convergence zone. Additional output options are ray depth distributions, ray printplots, and Calcomp ray plots, including plots of input sound speeds and of bathymetric profiles.

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HORIZONTAL-GRADIENT ACOUSTICAL RAY-TRACE PROGRAM TRIMAIN

INTRODUCTION

The growth in computer capability over the last 15 years coupled with interest in underwater acoustics has prompted the creation of several computer programs for acoustical ray tracing. For short-range calculation, for which the sound-speed profile can be considered to be the same throughout the given domain and the bottom topography can be considered flat, computation time is conserved by using a single profile program which takes advantage of the periodic form of the ray trajectories, such as the program RTRACE [1]. For long-range acoustical ray tracing, for which the bottom profile as well as the horizontal velocity structure is quite varied, a more general program [2-4] is required. One example of this is the program TRIMAIN, the principal features of which are as follows:

- Acoustic velocity gradients in the sound speed field are accounted for by reading in sound-speed profiles as a function of range and depth. Sound-speed profiles may be introduced at any point in range, and there is no limit to the number which may be used, although each new profile slows the program. A maximum of 50 input and internally generated points are allowed per profile. The sound-speed profiles are assumed to be piecewise linear functions of depth and range. An excellent source of sound-speed-profile data is the NODC tapes [5].
- A variable bottom may be read in as a piecewise linear function of depth, with a maximum of 250 points as the end points of the linear pieces.
- The range-and-depth plane is divided into triangular regions whose vertexes are all initially at ranges equal to the ranges of the endpoints of the linear bottom segments.
- The rays are assumed to be parabolic in each triangle, and it is their intersections with the triangle boundaries that are calculated.
- All the rays are advanced at one time to a given range, rather than tracing one ray at a time all the way to the end of the track.
- Four types of intensity calculation are available: type I random phase summation, type I coherent phase summation, type II (average over depth), and type III (average over convergence zone). Unmodified ray theory is used throughout. (Caustics will be discussed later.)
- The volume attenuation in the medium is assumed to follow a modified Marsh-Schulkin formula.
- Bottom-loss values (in dB), may be entered as a function of grazing angle, one value per degree, or the Marine Geophysical Survey (MGS) bottom-loss values may be used by specifying the class and the range to which that value is to be used.
- A bottom-phase-shift table may be entered for coherent phase calculation if known; it is read in as a value in radians, one value per degree.

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- The sea surface is represented as a flat, specularly reflecting boundary with a constant user-specified reflection coefficient and a constant phase shift of 180°.
- A source beam pattern may be read in at 1-degree intervals.

Several output options are available:

- A printplot of intensity vs range,
- A printout of intensity vs range values,
- A printplot of the ray trajectories vs range,
- A Calcomp plot of ray trajectories vs range,
- Ray depth distribution at specified ranges,
- A Calcomp plot of the input sound-speed profiles,
- A printplot of the input, or of the input and interpolated, sound-speed profiles,
- An eigenray printout if intensity calculations are performed,
- Punched cards for intensity values or eigenrays.

Up to ten output control cards may be specified.

The calculated results from TRIMAIN have been compared with experimental results, (Appendix B), and good agreement exists between the two.

The time required to run the program depends on a number of factors, such as the number of rays, the number of range increments, and the output requested. A sample case using 81 rays, 200 range increments, one receiver, and two profiles took 7 minutes and 48 seconds.

The core requirement for the program and system routines is 43,503 decimal locations. Also, some sort of deferred printout equipment is required, such as a drum, or the data may be written on tapes and the tapes printed.

The original development [6] of this computer code was due to Mr. Edward L. Wright, who is now at Harvard Observatory, Cambridge, Massachusetts. The author has added a number of features which were not in the original program and has revised certain sections. The function of each subroutine will be outlined in this report for the convenience of those individuals who might be interested in modifying the program.

BASIC EQUATIONS

The basic differential equations which are solved in TRIMAIN for ray position and time are:

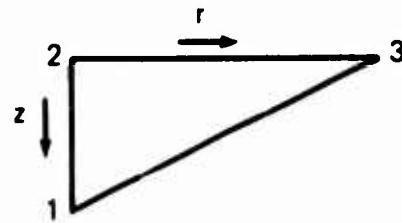
$$n(\vec{r}) = \frac{1}{c(\vec{r})}, \quad (1)$$

$$(d/ds)T = n(\vec{r}), \quad (2)$$

$$(d/ds)[n(\vec{r})(d/ds)\vec{r}] = \vec{\nabla}n(\vec{r}). \quad (3)$$

Eq. (1) states that the index of refraction as a function of range is equal to the reciprocal of the sound speed as a function of range. Eq. (2) is the equation for the ray time, where T is time and ds is arc length. Eq. (3) is the Lagrangian equation, where $\vec{\nabla}$ is the Lagrangian; it gives the ray path and accounts for the refraction.

We will now develop an equation for velocity fit. If we have the triangle



where depth is in the $2 \rightarrow 1$ or z direction and range is in the $2 \rightarrow 3$ or r direction, then the following equations hold:

$$\frac{1}{c_2^2} - \frac{1}{c_1^2} = G_r(r_3 - r_1) + G_z(z_3 - z_1), \quad (4)$$

$$\frac{1}{c_2^2} - \frac{1}{c_1^2} = G_r(r_2 - r_1) + G_z(z_2 - z_1), \quad (5)$$

$$\frac{1}{c^2} = \frac{1}{c_1^2} + G_r(r - r_1) + G_z(z - z_1), \quad (6)$$

where G_r is the gradient in the r direction and G_z is the gradient in the z direction. Eq. (6) gives the reciprocal of the sound speed squared at a range r and depth z in the triangle. We will specialize to the case $r_2 = r_1$, because we will always be getting vertical profiles.

TRIMAIN INPUT

Following will be a list describing the data deck of the program TRIMAIN, and for illustration the sample data deck shown in Fig. 1 will be referred to. The Roman numbers itemizing the list are the card group numbers at the right in Fig. 1.

- I. *Title (columns 1-80).* In the restarting case, the word RESTART is placed in columns 1-7. If a dump is desired if program runs out of time again, DUMP is placed in columns 9-12.
- II. *Source Parameters*

<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Source depth	1-8	In meters. (In Fig. 1 the source depth is 500 meters.)
Frequency	9-13	In kilohertz (0.05 kHz in Fig. 1)

Fig. 1 - Sample data deck of the program TBMAIN

<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Attenuation switch	14	0 (as in Fig. 1) means no volume attenuation; nonzero means $\alpha = 0.0003025f^2 + 44f^2/(4100 + f^2)$ dB/km, where f is the frequency in kilohertz.
Source level	15-19	Level in decibels (0.0 in Fig. 1)
Beam pattern switch (to be referred to later as ITBP)	20	0 (as in Fig. 1) means no beam pattern; nonzero means the beam pattern will be read in later.
Down tilt	21-25	Tilt of the beam-pattern axis in degrees (0.0 in Fig. 1).
Surface loss	26-30	Surface loss in decibels (0.0 in Fig. 1).
Bottom-loss switch	31	1 means an infinite bottom loss, so that no table will be read in; 0 (as in Fig. 1) means a loss table will be read in later.
Bottom-phase switch (ISCP)	32	1 means a bottom-phase-shift table will be read in; 0 (as in Fig. 1) means no table will be read in.
Curved earth (receiver)	33	1 (as in Fig. 1) means a curved earth correction for the receiver; 0 means no curve.
Curved bottom points	34	1 (as in Fig. 1) means a curved earth correction for the bottom; 0 means no curve.
Plot (Calcomp) profiles	35	2 means input and interpolated profiles are plotted; 1 (as in Fig. 1) means only input profiles are plotted; 0 means no plot.
Printplot profiles	36	1 means printplot-input profiles; 0 means no plot; 2 (as in Fig. 1) means printplot-input and interpolated profiles.
Calcomp plot profiles in kilometers or nautical miles	37	1 means plot nm; 0 (as in Fig. 1) means km.
Plot length	38-45	Calcomp plot length in inches (24.0 inches in Fig. 1).

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<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Bottom-reflection termination (NBRS)	46-50	Maximum number of bottom hits allowed before a ray is terminated; if blank (as in Fig. 1) or 0, 2500 will be used.
Surface-reflection termination (NSRS)	51-55	Maximum number of surface hits allowed before a ray is terminated; if blank (as in Fig. 1) or 0, 2500 will be used.
Loss termination (ALIM)	56-65	Maximum loss allowed before a ray is terminated; the input value is a positive number in dB, such as 200.0; if blank (as in Fig. 1) or 0, a value of 300.0 will be used.
Multiple replacement option IA	66	If IA is blank (as in Fig. 1) or 0 and ITBP = 0, angle cards are read from the card reader; if IA is blank or 0 and ITBP = 1, angle fan cards and beam-pattern cards are read from the card reader. If IA = 1 and ITBP = 0, the last set of fan cards for which multiple replacement option LA (in column 71) is 1 will be used, and if ITBP = 1 a new beam pattern will then be read in. If IA = 2, which requires that ITBP = 1, the old beam pattern will be used and a new set of angles will be read. If IA = 3, the old angle set and beam-pattern set is used.
Multiple replacement option IB	67	If IB is blank or 0, bottom-loss cards are read from the card reader, and if ISCP = 1, phase-shift cards are read. Bottom classes 0 through 5 are assumed to have a zero phase shift, so phase-shift cards are not read for these classes. If IB = 1, the old bottom-loss set is used, and a new bottom-phase-shift set is read in if ISCP = 1. If IB = 2, a new bottom-loss set will be read in, and if ISCP = 1, the old bottom-phase-shift set will be used. If IB = 3 and ISCP = 1, the old bottom-phase-shift and bottom loss will be used.

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<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Multiple replacement option IP	68	If IP is blank or 0, a new set of output control cards will be read in; if IP = 1, the old set will be used.
Multiple replacement option ID	69	If ID is blank or 0, a new bottom track will be read, if ID = 1, the old bottom track will be used.
Multiple replacement option IS	70	If IS is blank or 0, a new set of sound-speed profiles will be read; if IS = 1, the old set will be read.
Multiple replacement option LA	71	If LA = 1, the current deck will be used later; if LA is blank or 0, no portion of this deck will be used later. Thus in the following pages the discussion of the various input sections are subject to the provisions of this section.
Restart Option	73-76	If restart capability is desired, the word DUMP is placed in columns 73-76.

III. *Ray Initialization Cards*

A. Fan Cards

<u>Variable</u>	<u>Columns</u>	<u>Remarks</u>
Up-angle limit	1-10	In degrees; the sign convention is + for up and - for down. (In Fig. 1 there are three fan cards, each on a separate line; the three up-angle limits are 15° down, 15° up, and 75° up.)
Down-angle limit (DAL)	11-20	DAL = -DAL for input. (In Fig. 1 the three down-angle limits that pair with the up-angle limits are 75° down, 15° down, and 15° up.)
Angular step	21-30	The step input is always positive. (In Fig. 1 the step is 1° from 75° down to 15° down, 1/4° from 15° down to 15° up, and 1° from 15° up to 75° up.)

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<u>Variable</u>	<u>Columns</u>	<u>Remarks</u>
Continuation Switch	31-35	0 means this is the last fan card; 1 means more cards follow.
Source Level	36-40	Decibels added for this fan to the source level in columns 15-19 on card II. This is left blank (as in Fig. 1) if no additional beam pattern on the transmitter is desired.
Phase	41-45	Phase in radians for this fan.

B. Beam Pattern Cards

If the beam pattern switch on card II (column 20) was nonzero, the beam pattern is read in, 20 values to a card, which is four columns per value, in decibels below the axial value. The first value is on axis, the next 1° off, etc. A blank or zero after the axial value ends the reading; the last nonzero value is extended to all higher angles.

IV. Bottom-Loss Cards

Cards are read with a variable (referred to as RUNTIL) in columns 1-8 in kilometers (in an F8.4 format) and IClass in columns 9-10 (I2 format). RUNTIL is the last range for IClass. (In the Fig. 1 example 457.0 6 means class 6 until 457 km (assuming another RUNTIL after this which is 0.0). *The last RUNTIL must be negative or zero.* The associated class will be used for the rest of the run. The possible values for IClass are 0-9:

0	zero bottom loss
1-5	MGS bottom class loss curves
6-9	user supplied tables.

The first time an IClass of 6 (as in Fig. 1), 7, 8, or 9 is read, a bottom-loss table is read, one value per degree, in decibels, 20 per card (in a 20F4.2 format) until a blank appears. (In Fig. 1 the table with an IClass of 6 is

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. blank
| |
(zero grazing angle) (9 degrees)

When an IClass of 6, 7, 8, or 9 is read in after the first time, the table does not need to be read in again. In reading in a table the last nonzero value is extended

to all higher angles. If ISCP $\neq 0$ on card II, a phase-shift table will be read after each loss table (classes 6-9; classes 0-5 have zero phase shift). The phase-shift table is read in, 20 values per card, 1° per value. The phase shifts are in radians. A zero value terminates read in; the last two nonzero values are used to extrapolate the phase shift to zero. (In Fig. 1 no phase-shift table was read in. The bottom-loss tables in Fig. 1 establish the following:

| Grazing Angle
(degrees) | Loss Until 457 km
(dB) | Loss After 457 km
(dB) |
|----------------------------|---------------------------|---------------------------|
| 0 | 0 | 4 |
| 1 | 1 | 5 |
| 2 | 2 | 6 |
| 3 | 3 | 7 |
| 4 | 4 | 8 |
| 5 | 5 | 9 |
| 6 | 6 | 10 |
| 7 | 7 | 11 |
| 8 | 8 | 12 |
| 9 | 9 | 13 |
| 10 | 10 | 14 |
| 11 | 10 | 14 |
| 12 | 10 | 14 |
| ↓ | ↓ | ↓ |
| 90 | | |

V. Output Control Cards

Output control cards specify the range and depths at which intensities are to be calculated, whether a ray plot or ray tape will be made, whether ray depth distributions will be printed, etc.

| Variable | Columns | Remarks |
|----------|---------|--|
| R1 | 1-6 | First range in kilometers. |
| DR | 7-12 | Range step in kilometers. If DR is negative, the range spacing will be logarithmic, with constant factor $f = 1 + \text{abs}(DR)/R1$. |
| R2 | 13-18 | Last range in kilometers. (In Fig. 1 the ranges specified are 100, 200, ..., 1000 kilometers on the first group V card, 5, 10, 15, ..., 1000 kilometers on the second card, 1, 2, ..., 100 |

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| <u>Variable</u> | <u>Columns</u> | <u>Remarks</u> |
|-----------------|----------------|---|
| | | kilometers on the third card, and 0, 1, 2, ..., 1000 kilometers on the fourth card.) |
| IC | 19-20 | Continuation switch. 0 means this is the last output control card; (as on the last OCC in Fig. 1) otherwise more will be read in. |
| ISCP | 21 | Switch for type I coherent phase; 1 means on, and 0 means off. |
| IT1 | 22 | Switch for type I random phase; 1 means on, and 0 means off. MUST = 1 when ISCP = 1. |
| IT2 | 23 | Switch for type II; 1 means on, and 0 means off. |
| IT3 | 24 | Switch for type III; 1 means on, and 0 means off. |
| IPER | 25 | Switch for type I eigenrays; 1 means on, and 0 means off. |
| LLMR | 26 | 1 means Lloyd's mirror effect is included. |
| JVSR | 27 | 0 means no intensity-vs-range plot for this output control card; 1 means a plot of type I vs range; 2 means a plot of type II vs range; 3 means a plot of type III vs range; 4 means coherent phase vs range. Only one intensity-vs-range plot can be made. |
| IRD | 28 | Switch for ray depth distribution (1 means on, as on the first group V card in Fig. 1), and 0 means off. |
| IRP | 29 | Switch for ray plot. |
| IRT | 30 | Switch for ray tape for Calcomp plot. |

If any of the switches in columns 21-25 are on, receiver depths are needed. The first six, in meters, are on the output control card itself, as follows:

| <u>Variable</u> | <u>Columns</u> |
|-----------------|----------------|
| RCD(1) | 33-40 |
| RCD(2) | 41-48 |
| RCD(3) | 49-56 |
| RCD(4) | 57-64 |
| RCD(5) | 65-72 |
| RCD(6) | 73-80 |

If there are more than six, the next ten depths follow the output control card on one card, and then, if needed, the 17th through 26th on another card. Twenty-six is the maximum available. Receiver depths are read until a zero or blank is found. (In Fig. 1 five receiver depths are specified on each of the first three cards: 50, 150, 250, 350, and 450 meters.) If none of the switches 21-25 are on, then no intensities will be calculated, so no receiver depths are necessary. These and some earlier spaces are then used for the ray plot, as follows:

| <u>Variable</u> | <u>Columns</u> | <u>Remarks</u> |
|-----------------|----------------|--|
| DR | 7-12 | Becomes the spacing in kilometers between lines in the ray plot. |
| R2 | 13-18 | Becomes the end of the ray plot. |
| RCD(1) | 33-40 | Becomes the number of rays to be plotted, $1 \leq N \leq 25$. This must be punched with a decimal point. (On the fourth group V card in Fig. 1, 25 rays are specified to be plotted.) |
| RCD(2) | 41-48 | Becomes the maximum depth for the ray plot, in meters. |

All these variables will be set to default values if not specified because of intensities. The defaults are: 1 kilometer spacing, 15 rays plotted, and the maximum bottom depth. Even if DR and R2 are set, the defaults for number of rays and (as in Fig. 1) maximum depth may be used if the columns are left blank.

VI. Bottom Track

A. Ranges and Depths

There are 10 values to a card, with range and depths in pairs with respective units in kilometers and meters. The first range must be zero. A later blank or zero or negative value terminates the input. As many

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cards as necessary, up to 50 cards for 250 ranges, will be read. Thus R_1 is in columns 1-8 of card 1, D_1 is in columns 9-16 of card 1, R_2 is in columns 17-24, D_2 is in columns 25-32, etc. The format for range and depth is 10F8.4.

VII. Sound-Speed Profiles

A. Range and Title

On the first card for each velocity profile, 0 is placed in column 1 if the curved-earth correction is desired. The range to the profile in kilometers is in columns 2-8. The title is in columns 9-80.

B. Depth and Velocity

There are 10 values per card after the range-and-title card. The first value on the card is the depth in meters for this profile. The second value is the sound speed in meters/second, at the first depth. As many sound speeds as depths are read in. A blank or negative value terminates input. The format for all cards is 10F8.4. (The number of input and internally generated points in a sound-speed profile cannot exceed 50; the number of internally generated points can be reduced by reading in profiles with common depths.)

VIII. Program Termination

An end-of-file card terminates each data set or case. If multiple cases are desired, the program will go back to the first card, after the end-of-file card. To terminate the run two end-of-file cards should be placed after the last case.

CONTROL CARDS FOR TRIMAIN

There are several equip cards, which have different functions (Fig. 2). Some of the cards are used for delayed printout, and some are used to punch cards. When using the program, one should change his job card to the form 7₉ JOB (30), charge, ID, time, rather than the usual form 7₉ JOB, charge, ID, time. The change from JOB to JOB (30) allows 30 additional logical units; without this change the program will abort.

If the output is not desired from a certain unit, it may be omitted by using the BY statement. Thus if one wanted to omit the output from logical unit 35, then one should have 7₉ EQUIP, 35=BY, where BY means bypass. The PR designation on an equip card means that unit will be printed. A PU designation means that logical unit will punch cards. The function for each card is as follows:

7₉ DEMAND, 50000B - This card is required for the restart option.

7₉ EQUIP, 3=PL - This card forces plotting of profiles if the program aborts, if the plot is requested.

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SEQUENCE 66660 STARTED PRINTING 06/06/73 AT 132946 ON LP00
DRUM SCRAP 2,1 COMPUTER ONE, MAX DEMAND IS 54000A VERSION 006 11/24/72
SEQUENCE NUMBER 606660 STARTED AT TIME 132726 DATED 06/06/73
J08(30),81S0162,014BGR,10
DEMAND,500000
COMMENT, THIS JOB PRODUCES DELAYED PRINTOUTS
EQUIP,1=PT,W1,W0,(TEST CASE,1,1,999),DA
EQUIP,3=PL
EQUIP,15=PT,LG,(TEST,1,1,999),DA
EQUIP,16=PT,LG,*,DA
EQUIP,20=PT,F1,RG,(TRIMAIN,C1,01,999)
EQUIP,35=EY
EQUIP,36=EY
EQUIP,37=PR
EQUIP,38=PR
EQUIP,39=PR
EQUIP,41=PR
EQUIP,42=PR
EQUIP,45=EY
EQUIP,46=EY
EQUIP,47=EY
EQUIP,48=EY
EQUIP,49=EY
BINARY DFCK
BANK,(0), LUUP
LOAD,20
RUN,10,10000

Fig. 2 — Example of control cards; this is the front page from the sample run

- 79 EQUIP, 35=BY(PU) - This will punch the bottom track and receiver depths if set equal to PU. Format 10F8.3.
- 79 EQUIP, 36=BY(PU) - This will punch intensity values in 16F5.1 format, for each range point. Each type of intensity will be punched for each receiver.
- 79 EQUIP, 37=PR - This produces a ray depth distribution if requested.
- 79 EQUIP, 38=PR - This produces a printplot of intensity vs range if requested on an output control card.
- 79 EQUIP, 39=PR - This prints the intensity values for the types specified.
- 79 EQUIP, 41=PR - This prints the Type I eigenrays when they are requested.
- 79 EQUIP, 42=PR - This produces the printplot of the ray trajectories when requested.
- 79 EQUIP, 45=BY(PU) - If this is set equal to PU, it will punch type I coherent intensity values for the contouring program. It should be set up for 19 receivers.

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- 79 EQUIP, 46=BY(PU) - If this is set equal to PU, it will punch type I random intensity values for the contouring program. It should be set up for 19 receivers.
- 79 EQUIP, 47=BY(PU) - If this is set equal to PU, it will punch type II intensity values for the contouring program. It should be set up for 19 receivers.
- 79 EQUIP, 48=BY(PU) - If this is set equal to PU, it will punch type III intensity values for the contouring program. It should be set up for 19 receivers.
- 79 EQUIP, 49=BY(PU) - This punches type I eigenrays; it punches everything that is printed in the eigenray printout.

:9 EQUIP, 1=MT,HI,WQ,**,DA--OUTPUT TAPE FOR CALCOMP PLOT OF RAY PATHS

The equip cards may be left in the deck if a certain option is not desired; there will be no output from that unit unless a write operation is performed in the program.

SUBROUTINES

The main, or executive, program TRIMAIN is used chiefly for selecting options and calling the proper subroutine to compute the desired quantities. The subroutines are shown in Fig. 3, and these will be discussed on the succeeding pages. All of the output control cards (group V), title cards (group I), and source depths, frequency, etc. (group II) are read in by the main program. A listing of TRIMAIN and the subroutines is found in Appendix A. A comparison of calculated and experimental values is found in Appendix B.

Subroutine INITRAYS

The subroutine INITRAYS (whose cards are identified in the right margin in Appendix A by INIT 1, INIT 2, ..., INIT 81) reads in the angle cards and the beam-pattern cards and sets up the initial values of each ray's tangent of the angle, depth, phase, and signal level. (card group numbers will be listed in the section). Information from card group II from the main program is passed in the common block /PATTERN/ (INIT 3, Appendix A), which contains the source depth, beam-pattern switch, degrees of down tilt, and source level (in decibels). INITRAYS then reads in card group III, comprising the fan cards and the beam pattern cards. Rays are started from the lowest angle of each fan to the top. If the low angle of a fan equals the highest angle of the previous fan, a continuous ray group results. Otherwise a buffer ray with zero signal strength separates the fans, and type I intensity calculations will not interpolate over the gap.

Subroutine BRLTRD

The subroutine BRLTRD reads in the bottom-loss cards (group IV) and sets up the first loss table. On entry, dummy parameter RB is equated to ISCP (card group II), is

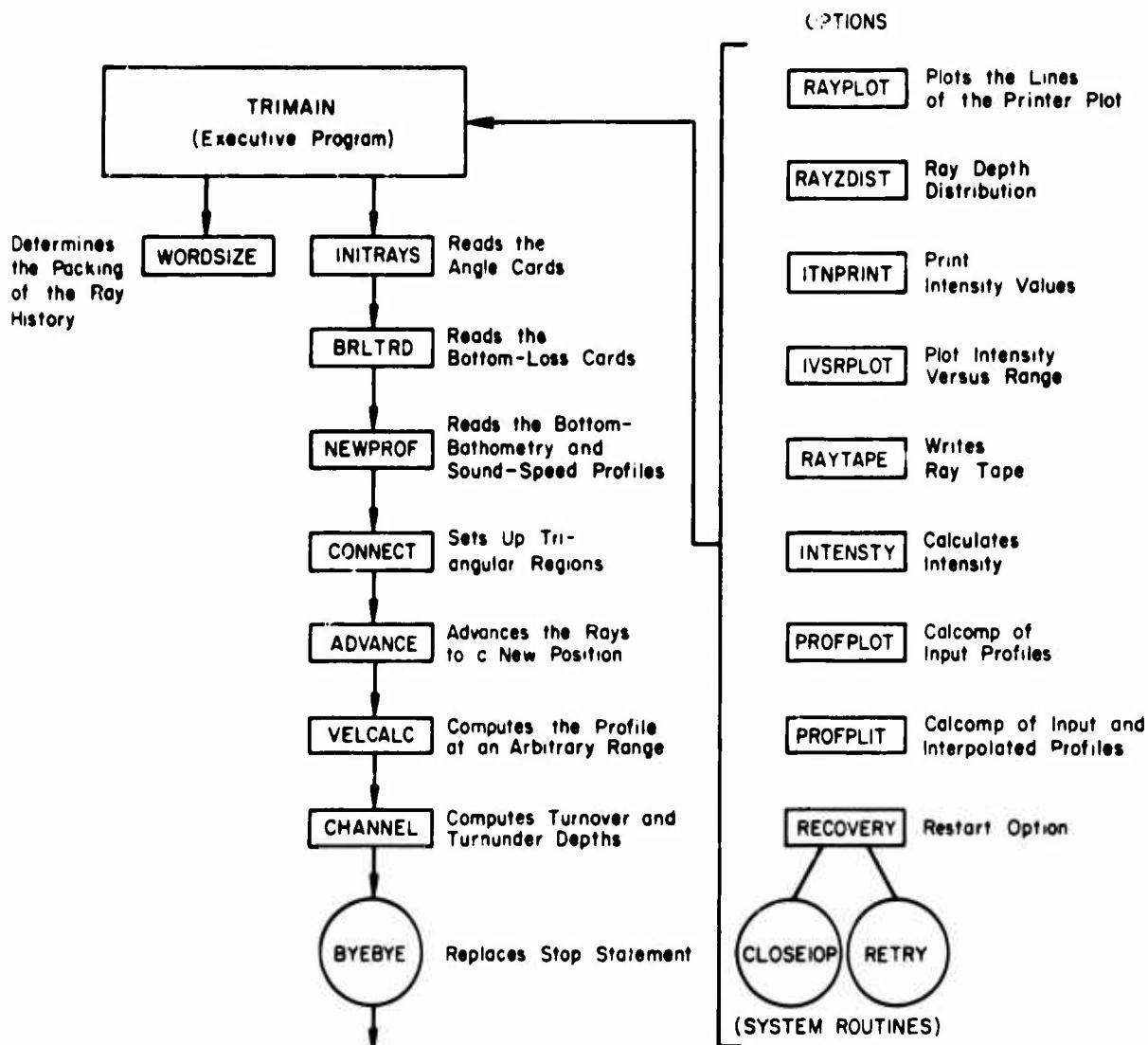


Fig. 3 — Function of each subroutine of the program TRIMAIN

either 1.0 or 0., and determines whether phase-shift tables will be read. On exit, RB is set to the range in kilometers until which the first loss table is to be used. The term ENTRY NWBRLT (as in BLD 146) resets the loss table and RB. TRIMAIN will call NWBRLT whenever the rays pass RB. For example, if there are two loss tables, one for 0 to 100 km and the second for 100 km to the end of the run, BRLTRD will read in both tables, set BRLT and BPST in the common block /MIRRORS/ (BLD 3, Appendix A) and set RB to 100. Later a call to NWBRLT sets BRLT and BPST to the second table of values, and RB to 1.E30 (i.e., 10^{30} km > end of run). Subroutine BRLTRD includes the Marine Geophysical Survey (MGS) classes 0 through 5, plus user classes 6

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through 9 stored in array BR, or user loss and phase classes 6 and 7, stored in arrays BR and BP. If a class 0 through 5 is specified, bottom phase classes do not have to be read in. A maximum of four user classes are available without phase shifts, and two classes are available with phase shifts. If classes 0 through 5 are used, a maximum of 50 cards is allowed.

Subroutine NEWPROF

Subroutine NEWPROF reads the bottom ranges, bottom depths (group VI), and the first two sound-speed profiles (group VII) on the first call. It then interpolates a profile for the first bottom point. Succeeding calls generate a new interpolated profile for each bottom point, unless this would pass the last read-in profile. In that case, a bottom point is interpolated to the profile range, and the profile is returned. A new profile is then read in. Thus the basic action of NEWPROF is to move $R2$ (range to the current profile), $N2$ (number of points in the current profile), $Z2$ (depth array), and $V2$ (sound-speed array) to $R1$ (range to the previous profile), $N1$ (number of points in the previous profile), $Z1$ (depth array for the previous profile), and $V1$ (sound-speed array for the previous profile) and set new values for $R2$, $N2$, $Z2$, and $V2$. It returns the maximum bottom depth in ZMAX. The printed output of NEWPROF is illustrated in Figs. 4a and 4b.

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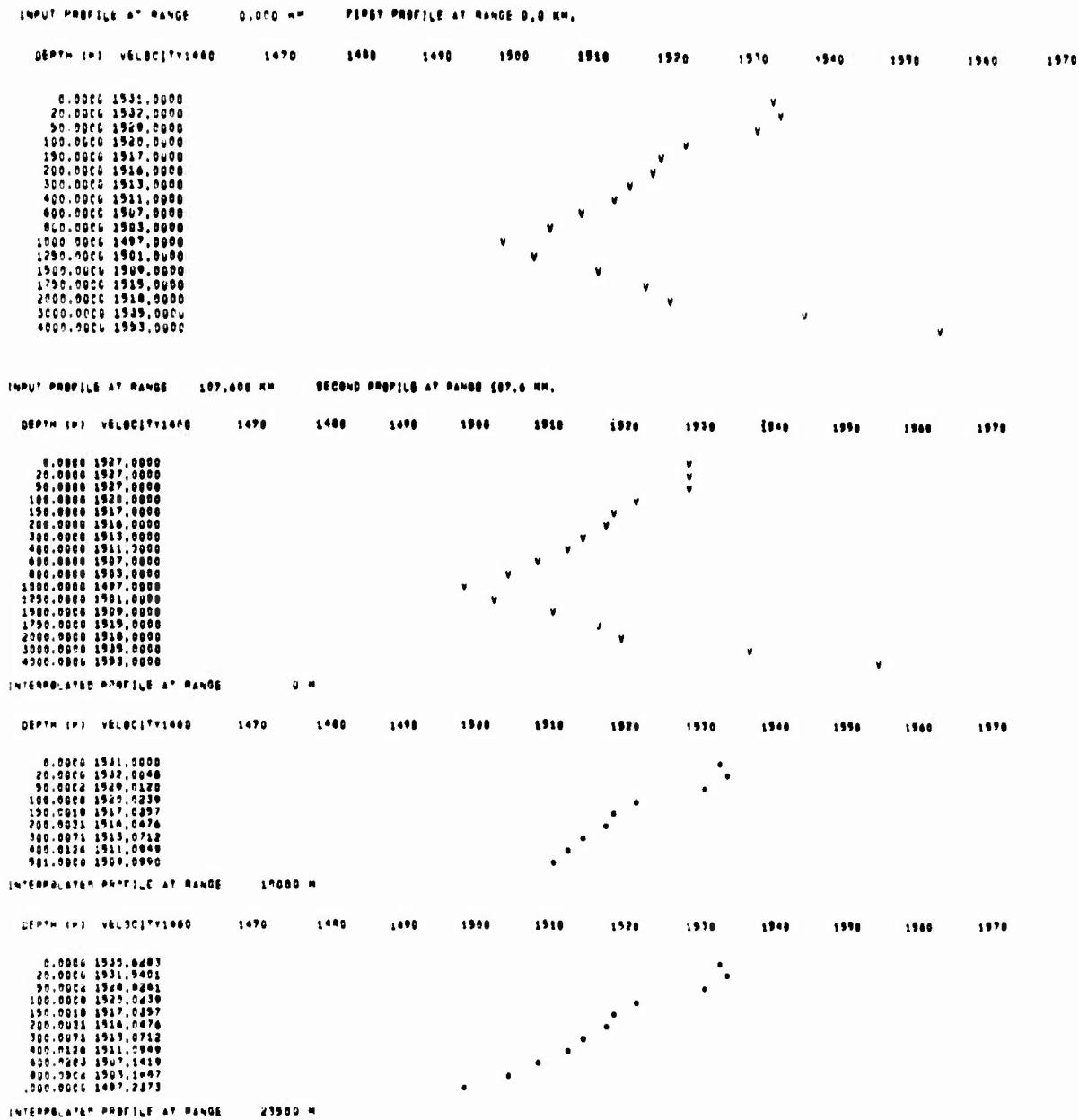


Fig. 4a — Output of NEWPROF. The first two input profiles are those of the sample case given in Fig. 1.

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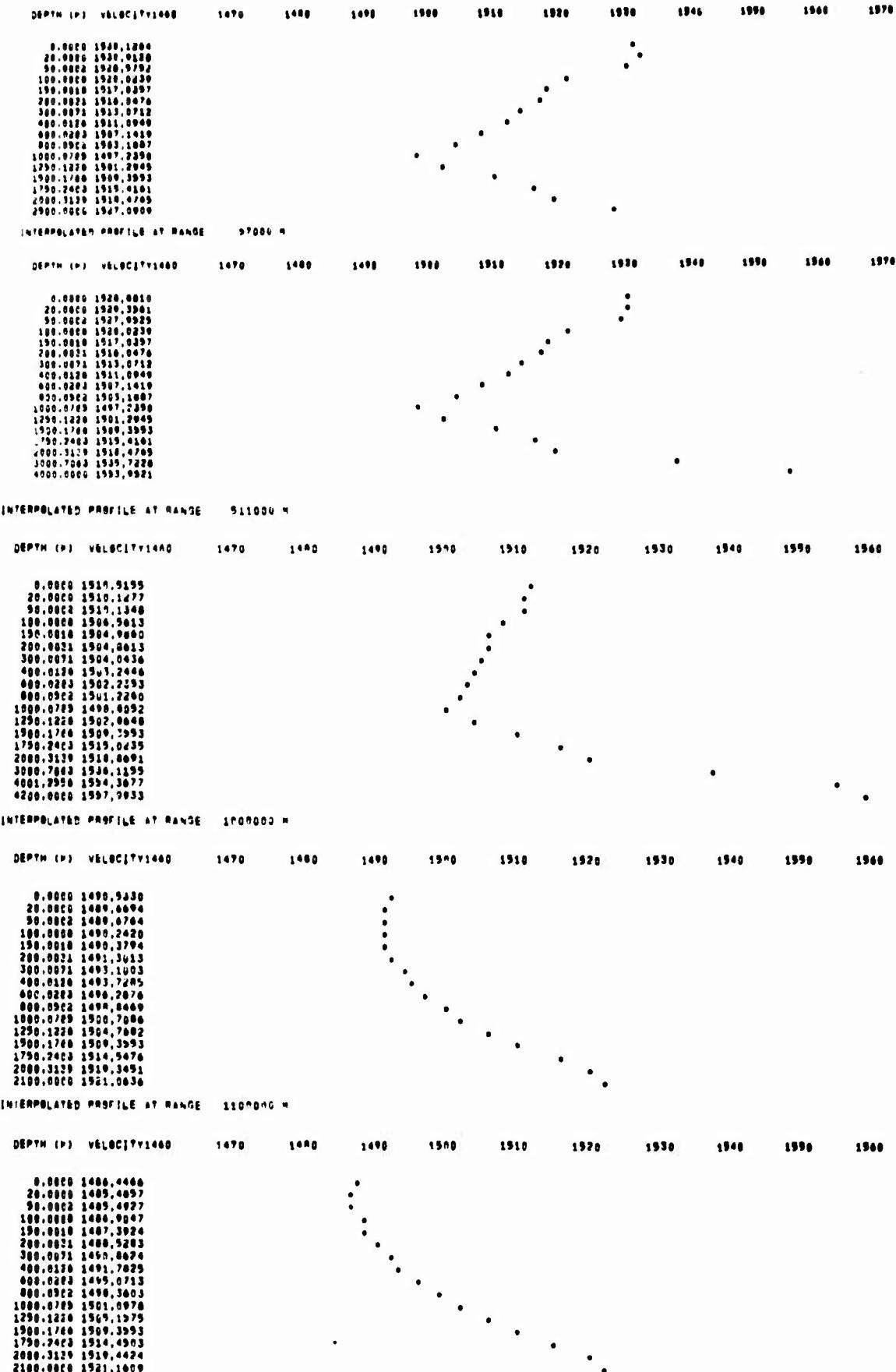


Fig. 4b — Additional portion of the output of NEWPROF shown in Fig. 4a

Subroutine CONNECT

Subroutine CONNECT uses $R1, N1, Z1, V1, R2, N2, Z2$, and $V2$ from NEWPROF and connects the points into triangular (Δ) regions. The coefficients of the triangles go into the common block /TRIANG/ (CONN 3, Appendix A). The variables in TRIANG are the following:

| | |
|--------------|---|
| AP, BP | coefficients of the Δ boundary in the prime frame, which is centered at RZERO and ZZERO and rotated by an angle θ , |
| AL, BL | coefficients of the lower Δ boundary in the ocean frame. |
| ZZERO, RZERO | ocean frame coordinates of the center of the prime frame. |
| AA, BB | coefficients of $1/c^2$ in the prime frame, i.e., $1/c^2 = AA + BBz'$, |
| SST, CCT | sin and cos of θ , the angle between the ocean and the prime frames. |

In the listing of the subroutine, the following conditions are true:

$$AL + BL \cdot R = \text{equation for boundary of triangle},$$

$$AA + BZ \cdot Z + BR \cdot R = \frac{1}{c^2}.$$

A typical network of triangular regions is illustrated in Fig. 5.

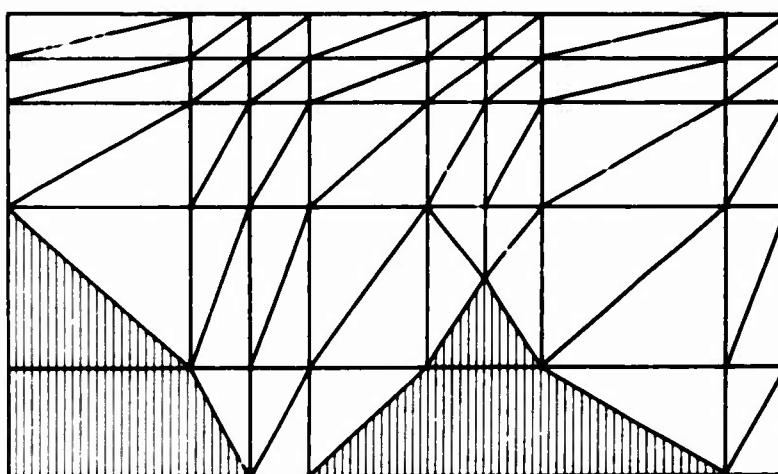


Fig. 5 -- Typical network of triangular regions

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Subroutine WORDSIZE

Subroutine WORDSIZE calculates some machine-dependent quantities. Four numbers are packed into array NCOUNT by using ITN , which is $ITN = \sqrt[4]{1/4} JBIG$, where $JBIG$ is the largest integer, which will fit into one computer word. The four numbers in each location in NCOUNT are: number of turnovers for this ray, number of bottom reflections, number of turnunders, and number of surface reflections. ENTRY RAYTAPE writes one record on the ray tape. The first record will contain the title card. Each record contains:

NRAY (number of ray),
Range (meters),
Bottom depth (meters),
Tan γ (up is positive)
Ray depth (meters),
Signal strength (multiplicative factor),
NCOUNT (ray history),
Travel time (seconds),
Phase (radians).

}

Each one contains NRAY words. All tan γ 's precede all ray depths, etc.

Subroutine ADVANCE

The basic function of subroutine ADVANCE is to advance the rays in the common block /RAYS/ from RSTART to RMAX. The procedure is as follows: First the proper triangle is found, the parabolic path is found, and intersections are calculated with the earliest intersection being used. Then surface and bottom reflections are performed. If ray is not at RMAX, the new triangle is determined, and a loop is made in the procedure to the calculation of intersections.

The explanation of various sections is as follows:

TANSUM (ADVA0012, Appendix A) is the tangent sum formula

$$\tan(\theta_1 + \theta_2) = \frac{\tan \theta_1 + \tan \theta_2}{1 - \tan \theta_1 * \tan \theta_2}$$

DELT gives the time increment of a ray in terms of the range increment DR, the two tangents T and S , and the vertex velocity $CMIS = 1/c_m^2$.

The DO 100 IRAY = 1, NRAY (ADVA0015) (card sequence number) selects each ray in turn.

ADVA0018 checks to see if a ray has been terminated.

ADVA0019 through ADVA0023 move the ray variables into local variables.

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The DO 20 I = 1, NRT! (ADVA0024 through ADVA0030) checks each triangle to see if the ray is in it. If a ray is on a boundary, it is in the layer it is pointing toward.

CT($\cos \theta$), ST($\sin \theta$), (rotation), and ZO and RO (displacement) define the primed frame of reference in which there is no r' gradient.

ZRP and RRP are the initial primed ray position.

CIS = $1/c^2$ at the ray.

Note: that TGR from TGAM (IRAY) is + for up rays and - for down rays, whereas TGRP = DZ'/dr' is + for down rays and - for up rays.

ALPHA (α) is the path curvature:

$$Z' = ZRP + TGRD*(r' - RRP) + ALPHA*(r' - RRP)^2$$

$$TA = 2\alpha = \frac{d^2Z'}{dr'^2}.$$

The quadratic equation solved in advance is

$$C + Py - \alpha y^2 = 0,$$

where $y = DRP = \text{change in } r' = RPNEW - RRP$. ALPHA (α) is often small and is zero for isovelocity layers. For small α the root

$$y = (P - \sqrt{P^2 + 4\alpha C})/2\alpha$$

is unstable. However, if α is small, the iteration $y = (\alpha y^2 - C)/P$ converges fast. The statement $DRP = (\text{ALPHA}*((\text{ALPHA}*DRP**2 - C)/P)**2 - C)/P$ is a double application of the above iteration and is used when

$$F = P - \sqrt{P^2 + 4\alpha C} < P.$$

When $\alpha = 0$, special linear path statements are used (ADVA0055 through ADVA0065 and ADAV0171 through ADVA0174). After statement 40 (ADVA0085), the next position is selected.

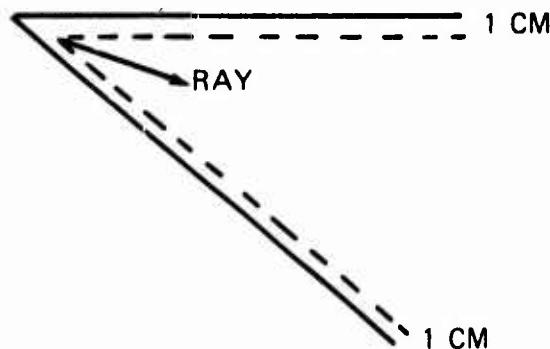
ONUP is true if a ray is on the upper boundary of a layer, meaning within 1 centimeter of the boundary and pointing in. ONLW is true if a ray is on the lower boundary.

There are four possibilities, in RPNEW, ZPNEW, ZNEW, and RNEW arrays. In general, the rule is

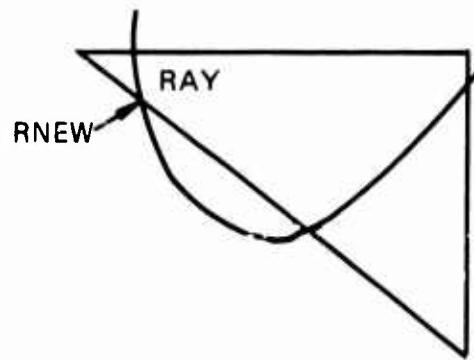
$$\text{RNEW} = \min(\text{RNEW}(k)) \text{ such that } \text{RNEW}(k) > RR.$$

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When a ray is on a boundary however the solution closest to the ray on that boundary is thrown out (ADVA0095, ADVA0096, ADVA0099, and ADVA100). Note, as shown in the following sketch, that a ray can be on both boundaries if it is on a corner.



If RNEW > RMAX, then the ray hits the vertical boundary (following sketch) and one goes to statement 50.



The cards from ADVA0129 to ADVA0163 increment the ray variables and decide on the next triangle.

ADVA0135 checks for vertices.

ADVA0136 decides whether a vertex is over or under.

ADVA0142 through ADVA0148 handles surface reflections.

ADVA0151 through ADVA0161 handles bottom reflections.

Statement 50 starts the vertical boundary section. The boundary in the primed frame is $Z' = AV + BVr'$.

If $ST = 0$, $BV \rightarrow \infty$; hence small ST 's are handled by statement 60.

When two intersections are possible, the one with the smallest depth change is used.

Statement 52 checks for vertices.

The statements ADVA0204 and ADVA0205 (545) check the ray's final depth to be sure it is in the correct layer.

Volume attenuation is approximated by 0.0001α (dB)/km $V\Delta T$ decibels, since one should have $S = \int v dt$ instead of $V\Delta T$.

The local variables are restored in the table ADVA0208 through ADVA0212, and a new ray is taken at statement 100.

Statements 60 through 68 (ADVA0214 through ADVA0235) use an iterative scheme to find the intersection with a vertical boundary. For $ST = 0$ or $\alpha = 0$ the first step is exact. The convergence limit is 1 centimeter, but seven steps are taken at once, so the usual error is very small.

Statement 80 terminates a ray and prints out the message RAY TERMINATED.

Statement 100 is the end of the outer loop of subroutine ADVANCE.

Subroutine PROFPLOT

Subroutine PROFPLOT plots the input velocity profiles and also the bottom track on a Calcomp plot (Fig. 6). They may be plotted in range increments of nautical miles or kilometers. In Fig. 6 the three profiles are at 0, 107.6, and 1135.4 km, which ranges are indicated by + symbols on the abscissa axis. The total plot length is specified to give a suitable scale.

Subroutine RAYZDIST

Subroutine RAYZDIST prints out a ray depth distribution (Fig. 7) each time it is called. The following items will be printed: NRAY - number of ray, NTO - number of turnovers, NTU - number of turnunders, NSR - number of surface reflections, NBR - number of bottom reflections, DEPTH = current depth of ray, THETA = ray angle at the point in degrees, TIME = travel time of ray in seconds to this range. The losses column is $10 \log_{10} SS$, and is initially

$$10 \log_{10} [(\cos \theta_0) \Delta \theta_0] + SORLEV - \text{beam pattern.}$$

If $SORLEV$ = beam pattern = 0 dB, and $\Delta \theta_0 = 1^\circ$, then losses start out -17.6 dB for a horizontal ray. In the plot line, B is the bottom, + is the lower vertex depth, * is the present ray position, - is the upper vertex and S is the surface.

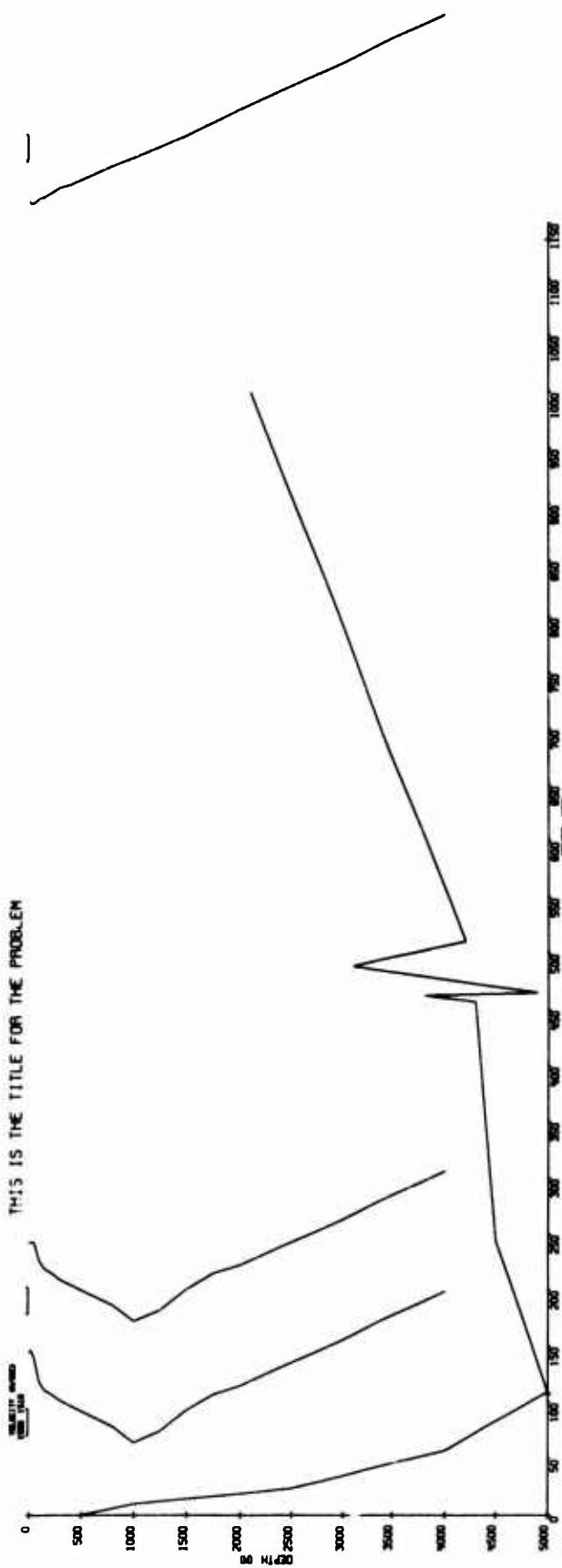


Fig. 6 — Colcomp plot of input profiles and the bottom track

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THIS IS THE TITLE FOR THE PROBLEM

| RAY DEPTH DISTRIBUTION AT 900,000 NM ² | | | | | | BOTTOM DEPTH 3480,000 NM | SCALE 91,000 NM/POSITION | | |
|---|------|------|----|---------|------------|--------------------------|--------------------------|---------|--------|
| LD | NAME | LINE | NU | NSA | NTB | CAPTH | THE114 | TIMB | LNSST |
| 1 | A | 10 | 8 | 18 | 8 | 2001,49 | -9,59039 | 335,563 | -193,9 |
| 2 | A | 10 | 9 | 18 | 8 | 3056,53 | -8,70056 | 339,578 | -182,0 |
| 3 | A | 10 | 9 | 19 | 8 | 2024,42 | -8,52096 | 339,574 | -170,0 |
| 4 | A | 10 | 9 | 19 | 8 | 2301,71 | -7,34799 | 339,533 | -117,3 |
| 5 | A | 10 | 10 | 18 | 8 | 2443,92 | -6,89491 | 334,893 | -110,3 |
| 6 | A | 10 | 10 | 19 | 8 | 1951,47 | -6,24271 | 339,482 | -110,3 |
| 7 | A | 9 | 18 | 8 | 3150,13 | -2,88799 | 334,908 | -112,0 | |
| 8 | A | 10 | 10 | 9 | 3054,21 | 9,53599 | 334,968 | -110,0 | |
| 9 | A | 9 | 18 | 8 | 2191,13 | -6,04790 | 334,968 | -108,0 | |
| 10 | A | 9 | 18 | 8 | 2074,49 | -5,92771 | 334,968 | -108,0 | |
| 11 | A | 9 | 17 | 8 | 241,48 | 19,20774 | 334,433 | -110,0 | |
| 12 | A | 10 | 17 | 8 | 447,48 | 11,46656 | 334,570 | -101,7 | |
| 13 | A | 11 | 18 | 9 | 893,17 | -15,32041 | 334,788 | -97,1 | |
| 14 | A | 10 | 17 | 8 | 2702,50 | 3,68931 | 334,390 | -99,1 | |
| 15 | A | 10 | 17 | 8 | 2676,49 | 3,21929 | 334,390 | -96,1 | |
| 16 | A | 9 | 17 | 8 | 2630,01 | -4,49880 | 334,383 | -93,7 | |
| 17 | A | 10 | 18 | 8 | 472,37 | 11,74638 | 334,044 | -96,9 | |
| 18 | A | 10 | 18 | 8 | 1070,91 | -9,47982 | 334,283 | -96,3 | |
| 19 | A | 10 | 17 | 8 | 2160,52 | -9,53731 | 334,333 | -96,3 | |
| 20 | A | 10 | 17 | 8 | 2154,24 | -1,59813 | 334,341 | -97,1 | |
| 21 | A | 10 | 18 | 8 | 2177,56 | -7,62407 | 334,741 | -99,0 | |
| 22 | A | 10 | 18 | 8 | 2582,61 | -4,89795 | 334,849 | -81,1 | |
| 23 | A | 9 | 18 | 8 | 1897,71 | -8,10919 | 333,708 | -79,4 | |
| 24 | A | 10 | 12 | 8 | 2950,92 | -1,47747 | 333,934 | -79,0 | |
| 25 | B | 11 | 14 | 2 | 7278,16 | 1,91578 | 333,934 | -79,0 | |
| 26 | B | 11 | 12 | 4 | 15,9,44 | 0,52737 | 333,889 | -79,9 | |
| 27 | B | 11 | 15 | 8 | 1726,18 | 4,52578 | 333,472 | -79,0 | |
| 28 | B | 11 | 15 | 8 | 1657,05 | 9,53523 | 333,422 | -76,3 | |
| 29 | B | 11 | 15 | 8 | 8136,77 | 7,76761 | 333,403 | -76,3 | |
| 30 | B | 10 | 14 | 8 | 2113,45 | -7,11216 | 333,576 | -76,1 | |
| 31 | B | 11 | 11 | 5 | 45,47 | -8,82121 | 333,576 | -76,1 | |
| 32 | B | 11 | 11 | 5 | 15,77 | 9,19477 | 333,573 | -76,1 | |
| 33 | B | 11 | 11 | 5 | 1963,11 | -5,40559 | 333,699 | -80,1 | |
| 34 | B | 12 | 9 | 12 | 178,35 | 4,91614 | 333,833 | -80,9 | |
| 35 | B | 12 | 9 | 12 | 497,87 | -6,13716 | 333,464 | -80,9 | |
| 36 | B | 12 | 9 | 11 | 811,07 | -1,74245 | 331,763 | -80,7 | |
| 37 | B | 11 | 8 | 7 | 1876,47 | 8,39702 | 331,453 | -87,1 | |
| 38 | B | 11 | 11 | 8 | 7678,02 | -7,64828 | 331,444 | -85,8 | |
| 39 | B | 10 | 10 | 8 | 2710,67 | 7,75455 | 333,003 | -86,1 | |
| 40 | B | 11 | 3 | 14 | 110,47 | -0,68951 | 333,588 | -96,3 | |
| 41 | B | 11 | 3 | 14 | 145,19 | -0,68957 | 333,549 | -96,3 | |
| 42 | B | 11 | 3 | 14 | 145,21 | 5,31767 | 333,546 | -96,3 | |
| 43 | B | 13 | 5 | 12 | 497,87 | -2,59108 | 333,594 | -80,9 | |
| 44 | B | 12 | 13 | 5 | 678,77 | -3,67482 | 333,466 | -98,4 | |
| 45 | B | 12 | 13 | 5 | 1175,05 | 7,90071 | 333,146 | -94,8 | |
| 46 | B | 11 | 12 | 1 | 1140,81 | 10,63459 | 332,768 | -91,2 | |
| 47 | B | 12 | 13 | 1 | 1627,43 | 8,57312 | 332,718 | -91,9 | |
| 48 | B | 12 | 13 | 1 | 7677,02 | -5,44482 | 332,664 | -88,1 | |
| 49 | B | 11 | 13 | 2 | 1859,31 | 5,93592 | 332,676 | -88,1 | |
| 50 | B | 12 | 4 | 21 | 674,81 | -0,74136 | 331,729 | -80,6 | |
| 51 | B | 12 | 4 | 21 | 15,21,80 | -6,78498 | 333,458 | -80,7 | |
| 52 | B | 12 | 4 | 20 | 92,21 | -5,37935 | 332,976 | -82,1 | |
| 53 | B | 12 | 11 | 1 | 2649,08 | 6,79169 | 332,547 | -97,1 | |
| 54 | B | 11 | 9 | 7 | 1079,24 | -9,82149 | 332,761 | -97,1 | |
| 55 | B | 12 | 12 | 12 | 442,41 | -9,26247 | 332,438 | -97,1 | |
| 56 | B | 12 | 12 | 13 | 1747,39 | -9,30803 | 332,018 | -97,1 | |
| 57 | B | 12 | 12 | 13 | 1747,42 | -9,30802 | 333,811 | -97,1 | |
| 58 | B | 25 | 6 | 6 | 677,35 | -1,04138 | 333,519 | -94,9 | |
| 59 | B | 27 | 6 | 27 | 1092,38 | 1,19947 | 331,641 | -10,2 | |
| 60 | B | 21 | 6 | 22 | 876,26 | -2,23863 | 331,531 | -10,2 | |
| 61 | B | 18 | 5 | 18 | 594,35 | 1,77448 | 333,412 | -97,8 | |
| 62 | B | 15 | 5 | 16 | 595,71 | -0,35794 | 331,229 | -97,8 | |
| 63 | B | 13 | 5 | 14 | 176,29 | -3,47435 | 332,020 | -96,5 | |
| 64 | B | 12 | 5 | 11 | 599,74 | 6,76704 | 332,764 | -95,6 | |
| 65 | B | 11 | 3 | 3 | 169,87 | -8,65463 | 332,509 | -93,7 | |
| 66 | B | 11 | 3 | 3 | 1072,04 | -8,63378 | 332,608 | -93,7 | |
| 67 | B | 11 | 5 | 16 | 169,87 | 6,86484 | 332,659 | -93,7 | |
| 68 | B | 7 | 7 | 5 | 172,36 | -8,84864 | 332,521 | -93,7 | |
| 69 | B | 11 | 6 | 6 | 1612,91 | -8,60132 | 332,470 | -93,1 | |
| 70 | B | 11 | 6 | 6 | 127,24 | -6,98411 | 332,664 | -92,4 | |
| 71 | B | 12 | 2 | 11 | 1655,85 | -6,90874 | 332,839 | -92,3 | |
| 72 | B | 12 | 2 | 12 | 1671,55 | -6,40268 | 332,909 | -92,1 | |
| 73 | B | 12 | 3 | 9 | 1514,07 | 4,64729 | 332,676 | -91,0 | |
| 74 | B | 12 | 4 | 10 | 391,64 | 6,63318 | 332,769 | -91,4 | |
| 75 | B | 15 | 2 | 21 | 976,31 | 9,95293 | 332,970 | -91,1 | |
| 76 | B | 15 | 2 | 21 | 976,34 | 9,70371 | 332,824 | -91,1 | |
| 77 | B | 15 | 3 | 13 | 956,61 | 9,70218 | 332,943 | -91,1 | |
| 78 | B | 15 | 3 | 13 | 745,61 | 5,71244 | 332,494 | -90,3 | |
| 79 | B | 15 | 3 | 13 | 375,62 | 4,45977 | 332,988 | -90,3 | |
| 80 | B | 15 | 3 | 13 | 356,73 | 4,40282 | 332,988 | -90,3 | |
| 81 | B | 15 | 3 | 17 | 47,39 | -0,49111 | 332,992 | -90,3 | |
| 82 | B | 13 | 1 | 1 | 143,51 | 3,09001 | 332,991 | -90,9 | |
| 83 | B | 13 | 0 | 13 | 672,37 | 6,32819 | 332,986 | -90,9 | |
| 84 | B | 12 | 0 | 12 | 1130,06 | -7,02133 | 332,879 | -90,0 | |
| 85 | B | 12 | 0 | 12 | 1130,06 | -7,02133 | 332,843 | -90,0 | |
| 86 | B | 12 | 0 | 12 | 1130,06 | -7,02133 | 332,843 | -90,0 | |
| 87 | B | 12 | 0 | 12 | 1130,06 | -7,02133 | 332,843 | -90,0 | |
| 88 | B | 20 | 31 | 31 | 872,39 | -6,67401 | 333,651 | -90,6 | |
| 89 | B | 26 | 29 | 29 | 956,39 | -2,97769 | 333,611 | -90,1 | |
| 90 | B | 21 | 21 | 21 | 1154,53 | -1,84316 | 333,922 | -90,1 | |
| 91 | B | 13 | 4 | 12 | 184,32 | 1,84316 | 332,924 | -90,1 | |
| 92 | B | 13 | 4 | 12 | 1445,78 | 4,76927 | 333,704 | -90,1 | |
| 93 | B | 13 | 4 | 12 | 1429,05 | 4,49928 | 332,936 | -90,1 | |
| 94 | B | 15 | 0 | 16 | 274,37 | -0,73343 | 333,207 | -90,4 | |
| 95 | B | 25 | 33 | 1032,38 | 1,59446 | 333,671 | -91,1 | | |
| 96 | B | 32 | 0 | 33 | 1032,38 | 1,59446 | 333,671 | -91,1 | |
| 97 | B | 29 | 31 | 31 | 872,39 | -6,67401 | 333,651 | -90,6 | |
| 98 | B | 26 | 29 | 29 | 956,39 | -2,97769 | 333,611 | -90,1 | |
| 99 | B | 21 | 21 | 21 | 1154,53 | -1,84316 | 333,922 | -90,1 | |
| 100 | B | 13 | 4 | 12 | 184,32 | 1,84316 | 332,924 | -90,1 | |
| 101 | B | 13 | 4 | 12 | 1445,78 | 4,76927 | 333,704 | -90,1 | |
| 102 | B | 15 | 0 | 35 | 951,31 | -1,57214 | 333,701 | -90,1 | |
| 103 | B | 10 | 0 | 16 | 593,01 | -1,14184 | 333,397 | -91,2 | |
| 104 | B | 10 | 0 | 17 | 596,93 | 1,77917 | 333,399 | -91,2 | |
| 105 | B | 9 | 28 | 6 | 27,96,02 | 2,72799 | 333,641 | -90,9 | |
| 106 | B | 8 | 21 | 21 | 1170,02 | -6,00779 | 333,529 | -91,0 | |
| 107 | B | 8 | 31 | 0 | 30,92,65 | 2,91301 | 333,672 | -91,3 | |
| 108 | B | 11 | 12 | 0 | 32,1075,79 | -9,51421 | 333,668 | -91,3 | |
| 109 | B | 15 | 19 | 0 | 30,92,65 | -2,91301 | 333,704 | -91,2 | |
| 110 | B | 10 | 0 | 45 | 934,64 | -6,04324 | 333,746 | -91,2 | |
| 111 | B | 12 | 0 | 49 | 1023,44 | -6,95229 | 333,758 | -91,2 | |
| 112 | B | 10 | 0 | 30 | 1001,70 | -6,30050 | 333,670 | -91,2 | |
| 113 | B | 9 | 29 | 0 | 28,916,79 | -1,87119 | 333,649 | -91,5 | |
| 114 | B | 9 | 37 | 0 | 30,1025,63 | 1,63937 | 333,730 | -90,7 | |
| 115 | B | 9 | 35 | 0 | 34,1013,38 | 2,02037 | 333,700 | -90,4 | |
| 116 | B | 8 | 18 | 0 | 10,911,67 | -0,72902 | 333,397 | -91,9 | |
| 117 | B | 8 | 34 | 0 | 34,912,19 | -0,97919 | 333,699 | -90,3 | |
| 118 | B | 8 | 93 | 0 | 57,989,01 | -0,97899 | 333,799 | -90,3 | |
| 119 | B | 8 | 19 | 0 | 19,470,69 | 3,352811 | 333,209 | -90,9 | |

Fig. 7 — Example of the output from RAYZDIST (first of four pages)

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best available copy.

| | | | | | | | |
|-----|---|----|----|---|-------|--------|-------|
| 121 | 1 | 15 | 13 | 0 | 316.2 | 167.93 | -20.7 |
| 122 | 1 | 15 | 13 | 0 | 317.3 | 167.73 | -21.7 |
| 123 | 1 | 15 | 13 | 0 | 318.3 | 167.53 | -21.7 |
| 124 | 1 | 15 | 13 | 0 | 319.3 | 167.33 | -21.7 |
| 125 | 1 | 15 | 13 | 0 | 320.3 | 167.13 | -21.7 |
| 126 | 1 | 15 | 13 | 0 | 321.3 | 166.93 | -21.7 |
| 127 | 1 | 15 | 13 | 0 | 322.3 | 166.73 | -21.7 |
| 128 | 1 | 15 | 13 | 0 | 323.3 | 166.53 | -21.7 |
| 129 | 1 | 15 | 13 | 0 | 324.3 | 166.33 | -21.7 |
| 130 | 1 | 15 | 13 | 0 | 325.3 | 166.13 | -21.7 |
| 131 | 1 | 15 | 13 | 0 | 326.3 | 165.93 | -21.7 |
| 132 | 1 | 15 | 13 | 0 | 327.3 | 165.73 | -21.7 |
| 133 | 1 | 15 | 13 | 0 | 328.3 | 165.53 | -21.7 |
| 134 | 1 | 15 | 13 | 0 | 329.3 | 165.33 | -21.7 |
| 135 | 1 | 15 | 13 | 0 | 330.3 | 165.13 | -21.7 |
| 136 | 1 | 15 | 13 | 0 | 331.3 | 164.93 | -21.7 |
| 137 | 1 | 15 | 13 | 0 | 332.3 | 164.73 | -21.7 |
| 138 | 1 | 15 | 13 | 0 | 333.3 | 164.53 | -21.7 |
| 139 | 1 | 15 | 13 | 0 | 334.3 | 164.33 | -21.7 |
| 140 | 1 | 15 | 13 | 0 | 335.3 | 164.13 | -21.7 |
| 141 | 1 | 15 | 13 | 0 | 336.3 | 163.93 | -21.7 |
| 142 | 1 | 15 | 13 | 0 | 337.3 | 163.73 | -21.7 |
| 143 | 1 | 15 | 13 | 0 | 338.3 | 163.53 | -21.7 |
| 144 | 1 | 15 | 13 | 0 | 339.3 | 163.33 | -21.7 |
| 145 | 1 | 15 | 13 | 0 | 340.3 | 163.13 | -21.7 |
| 146 | 1 | 15 | 13 | 0 | 341.3 | 162.93 | -21.7 |
| 147 | 1 | 15 | 13 | 0 | 342.3 | 162.73 | -21.7 |
| 148 | 1 | 15 | 13 | 0 | 343.3 | 162.53 | -21.7 |
| 149 | 1 | 15 | 13 | 0 | 344.3 | 162.33 | -21.7 |
| 150 | 1 | 15 | 13 | 0 | 345.3 | 162.13 | -21.7 |
| 151 | 1 | 15 | 13 | 0 | 346.3 | 161.93 | -21.7 |
| 152 | 1 | 15 | 13 | 0 | 347.3 | 161.73 | -21.7 |
| 153 | 1 | 15 | 13 | 0 | 348.3 | 161.53 | -21.7 |
| 154 | 1 | 15 | 13 | 0 | 349.3 | 161.33 | -21.7 |
| 155 | 1 | 15 | 13 | 0 | 350.3 | 161.13 | -21.7 |
| 156 | 1 | 15 | 13 | 0 | 351.3 | 160.93 | -21.7 |
| 157 | 1 | 15 | 13 | 0 | 352.3 | 160.73 | -21.7 |
| 158 | 1 | 15 | 13 | 0 | 353.3 | 160.53 | -21.7 |
| 159 | 1 | 15 | 13 | 0 | 354.3 | 160.33 | -21.7 |
| 160 | 1 | 15 | 13 | 0 | 355.3 | 160.13 | -21.7 |
| 161 | 1 | 15 | 13 | 0 | 356.3 | 159.93 | -21.7 |
| 162 | 1 | 15 | 13 | 0 | 357.3 | 159.73 | -21.7 |
| 163 | 1 | 15 | 13 | 0 | 358.3 | 159.53 | -21.7 |
| 164 | 1 | 15 | 13 | 0 | 359.3 | 159.33 | -21.7 |
| 165 | 1 | 15 | 13 | 0 | 360.3 | 159.13 | -21.7 |
| 166 | 1 | 15 | 13 | 0 | 361.3 | 158.93 | -21.7 |
| 167 | 1 | 15 | 13 | 0 | 362.3 | 158.73 | -21.7 |
| 168 | 1 | 15 | 13 | 0 | 363.3 | 158.53 | -21.7 |
| 169 | 1 | 15 | 13 | 0 | 364.3 | 158.33 | -21.7 |
| 170 | 1 | 15 | 13 | 0 | 365.3 | 158.13 | -21.7 |
| 171 | 1 | 15 | 13 | 0 | 366.3 | 157.93 | -21.7 |
| 172 | 1 | 15 | 13 | 0 | 367.3 | 157.73 | -21.7 |
| 173 | 1 | 15 | 13 | 0 | 368.3 | 157.53 | -21.7 |
| 174 | 1 | 15 | 13 | 0 | 369.3 | 157.33 | -21.7 |
| 175 | 1 | 15 | 13 | 0 | 370.3 | 157.13 | -21.7 |
| 176 | 1 | 15 | 13 | 0 | 371.3 | 156.93 | -21.7 |
| 177 | 1 | 15 | 13 | 0 | 372.3 | 156.73 | -21.7 |
| 178 | 1 | 15 | 13 | 0 | 373.3 | 156.53 | -21.7 |
| 179 | 1 | 15 | 13 | 0 | 374.3 | 156.33 | -21.7 |
| 180 | 1 | 15 | 13 | 0 | 375.3 | 156.13 | -21.7 |
| 181 | 1 | 15 | 13 | 0 | 376.3 | 155.93 | -21.7 |
| 182 | 1 | 15 | 13 | 0 | 377.3 | 155.73 | -21.7 |
| 183 | 1 | 15 | 13 | 0 | 378.3 | 155.53 | -21.7 |
| 184 | 1 | 15 | 13 | 0 | 379.3 | 155.33 | -21.7 |
| 185 | 1 | 15 | 13 | 0 | 380.3 | 155.13 | -21.7 |
| 186 | 1 | 15 | 13 | 0 | 381.3 | 154.93 | -21.7 |
| 187 | 1 | 15 | 13 | 0 | 382.3 | 154.73 | -21.7 |
| 188 | 1 | 15 | 13 | 0 | 383.3 | 154.53 | -21.7 |
| 189 | 1 | 15 | 13 | 0 | 384.3 | 154.33 | -21.7 |
| 190 | 1 | 15 | 13 | 0 | 385.3 | 154.13 | -21.7 |
| 191 | 1 | 15 | 13 | 0 | 386.3 | 153.93 | -21.7 |
| 192 | 1 | 15 | 13 | 0 | 387.3 | 153.73 | -21.7 |
| 193 | 1 | 15 | 13 | 0 | 388.3 | 153.53 | -21.7 |
| 194 | 1 | 15 | 13 | 0 | 389.3 | 153.33 | -21.7 |
| 195 | 1 | 15 | 13 | 0 | 390.3 | 153.13 | -21.7 |
| 196 | 1 | 15 | 13 | 0 | 391.3 | 152.93 | -21.7 |
| 197 | 1 | 15 | 13 | 0 | 392.3 | 152.73 | -21.7 |
| 198 | 1 | 15 | 13 | 0 | 393.3 | 152.53 | -21.7 |
| 199 | 1 | 15 | 13 | 0 | 394.3 | 152.33 | -21.7 |
| 200 | 1 | 15 | 13 | 0 | 395.3 | 152.13 | -21.7 |
| 201 | 1 | 15 | 13 | 0 | 396.3 | 151.93 | -21.7 |
| 202 | 1 | 15 | 13 | 0 | 397.3 | 151.73 | -21.7 |
| 203 | 1 | 15 | 13 | 0 | 398.3 | 151.53 | -21.7 |
| 204 | 1 | 15 | 13 | 0 | 399.3 | 151.33 | -21.7 |
| 205 | 1 | 15 | 13 | 0 | 400.3 | 151.13 | -21.7 |
| 206 | 1 | 15 | 13 | 0 | 401.3 | 150.93 | -21.7 |
| 207 | 1 | 15 | 13 | 0 | 402.3 | 150.73 | -21.7 |
| 208 | 1 | 15 | 13 | 0 | 403.3 | 150.53 | -21.7 |
| 209 | 1 | 15 | 13 | 0 | 404.3 | 150.33 | -21.7 |
| 210 | 1 | 15 | 13 | 0 | 405.3 | 150.13 | -21.7 |
| 211 | 1 | 15 | 13 | 0 | 406.3 | 149.93 | -21.7 |
| 212 | 1 | 15 | 13 | 0 | 407.3 | 149.73 | -21.7 |
| 213 | 1 | 15 | 13 | 0 | 408.3 | 149.53 | -21.7 |
| 214 | 1 | 15 | 13 | 0 | 409.3 | 149.33 | -21.7 |
| 215 | 1 | 15 | 13 | 0 | 410.3 | 149.13 | -21.7 |
| 216 | 1 | 15 | 13 | 0 | 411.3 | 148.93 | -21.7 |
| 217 | 1 | 15 | 13 | 0 | 412.3 | 148.73 | -21.7 |
| 218 | 1 | 15 | 13 | 0 | 413.3 | 148.53 | -21.7 |
| 219 | 1 | 15 | 13 | 0 | 414.3 | 148.33 | -21.7 |
| 220 | 1 | 15 | 13 | 0 | 415.3 | 148.13 | -21.7 |
| 221 | 1 | 15 | 13 | 0 | 416.3 | 147.93 | -21.7 |
| 222 | 1 | 15 | 13 | 0 | 417.3 | 147.73 | -21.7 |
| 223 | 1 | 15 | 13 | 0 | 418.3 | 147.53 | -21.7 |
| 224 | 1 | 15 | 13 | 0 | 419.3 | 147.33 | -21.7 |
| 225 | 1 | 15 | 13 | 0 | 420.3 | 147.13 | -21.7 |
| 226 | 1 | 15 | 13 | 0 | 421.3 | 146.93 | -21.7 |
| 227 | 1 | 15 | 13 | 0 | 422.3 | 146.73 | -21.7 |
| 228 | 1 | 15 | 13 | 0 | 423.3 | 146.53 | -21.7 |
| 229 | 1 | 15 | 13 | 0 | 424.3 | 146.33 | -21.7 |
| 230 | 1 | 15 | 13 | 0 | 425.3 | 146.13 | -21.7 |
| 231 | 1 | 15 | 13 | 0 | 426.3 | 145.93 | -21.7 |
| 232 | 1 | 15 | 13 | 0 | 427.3 | 145.73 | -21.7 |
| 233 | 1 | 15 | 13 | 0 | 428.3 | 145.53 | -21.7 |
| 234 | 1 | 15 | 13 | 0 | 429.3 | 145.33 | -21.7 |
| 235 | 1 | 15 | 13 | 0 | 430.3 | 145.13 | -21.7 |
| 236 | 1 | 15 | 13 | 0 | 431.3 | 144.93 | -21.7 |
| 237 | 1 | 15 | 13 | 0 | 432.3 | 144.73 | -21.7 |
| 238 | 1 | 15 | 13 | 0 | 433.3 | 144.53 | -21.7 |
| 239 | 1 | 15 | 13 | 0 | 434.3 | 144.33 | -21.7 |
| 240 | 1 | 15 | 13 | 0 | 435.3 | 144.13 | -21.7 |
| 241 | 1 | 15 | 13 | 0 | 436.3 | 143.93 | -21.7 |
| 242 | 1 | 15 | 13 | 0 | 437.3 | 143.73 | -21.7 |
| 243 | 1 | 15 | 13 | 0 | 438.3 | 143.53 | -21.7 |
| 244 | 1 | 15 | 13 | 0 | 439.3 | 143.33 | -21.7 |
| 245 | 1 | 15 | 13 | 0 | 440.3 | 143.13 | -21.7 |

Fig. 7 (Continued) — Example of the output from RAYZDIST (second of four pages)

NRL REPORT 7827

Table 19 THE TITLE FOR THE PROBLEMS

RAY DEPTH DISTRIBUTION AT 1200.000 KM. ELEVATION DEPTH 2100.000 M. SCALD 99.997 POSITION

| LINE | X | Y | Z | RAY DEPTH | ELEVATION DEPTH | SCALD | POSITION | |
|------|---|----|-----|-----------|-----------------|-----------|----------|--------|
| 10 | 1 | 24 | 18 | 2 | 1214.50 | 15.45244 | 871.329 | -171.9 |
| 11 | 1 | 24 | 19 | 2 | 1188.09 | -12.67774 | 871.764 | +231.9 |
| 12 | 1 | 24 | 20 | 2 | 1144.11 | 13.98467 | 871.150 | +210.4 |
| 13 | 1 | 24 | 21 | 2 | 1120.19 | -12.10937 | 870.035 | +206.2 |
| 14 | 1 | 24 | 22 | 2 | 1104.67 | 11.76964 | 869.966 | +210.9 |
| 15 | 1 | 24 | 23 | 2 | 1092.19 | -12.10937 | 869.966 | +210.9 |
| 16 | 1 | 24 | 24 | 2 | 1085.41 | -11.49413 | 869.966 | +113.0 |
| 17 | 1 | 24 | 25 | 2 | 1077.06 | -11.49413 | 869.497 | +216.0 |
| 18 | 1 | 24 | 26 | 2 | 1072.28 | 15.45244 | 869.497 | +202.4 |
| 19 | 1 | 24 | 27 | 2 | 1064.69 | -12.99370 | 869.701 | +192.5 |
| 20 | 1 | 24 | 28 | 2 | 1057.02 | -12.45474 | 869.701 | +176.1 |
| 21 | 1 | 24 | 29 | 2 | 1048.96 | -15.73572 | 869.117 | +170.7 |
| 22 | 1 | 24 | 30 | 2 | 1041.26 | -17.14141 | 869.787 | -174.1 |
| 23 | 1 | 24 | 31 | 2 | 1033.67 | 14.54566 | 869.421 | -143.0 |
| 24 | 1 | 24 | 32 | 2 | 1026.17 | 14.45244 | 869.421 | -153.0 |
| 25 | 1 | 24 | 33 | 2 | 1018.71 | -17.77426 | 869.511 | +156.7 |
| 26 | 1 | 24 | 34 | 2 | 1011.35 | 9.77426 | 869.511 | +177.0 |
| 27 | 1 | 24 | 35 | 2 | 1004.09 | -17.77426 | 869.749 | +146.2 |
| 28 | 1 | 24 | 36 | 2 | 996.83 | 13.78343 | 869.914 | +155.3 |
| 29 | 1 | 24 | 37 | 2 | 990.58 | -11.16241 | 869.914 | +152.5 |
| 30 | 1 | 24 | 38 | 2 | 984.33 | -11.16241 | 869.921 | +152.5 |
| 31 | 1 | 24 | 39 | 2 | 978.09 | 15.17234 | 869.915 | +143.4 |
| 32 | 1 | 24 | 40 | 2 | 971.85 | -17.52773 | 869.774 | +161.1 |
| 33 | 1 | 24 | 41 | 2 | 965.62 | -11.47667 | 869.774 | +171.1 |
| 34 | 1 | 24 | 42 | 2 | 959.40 | -11.47667 | 869.774 | +171.1 |
| 35 | 1 | 24 | 43 | 2 | 953.18 | -1.47452 | 869.787 | +171.1 |
| 36 | 1 | 24 | 44 | 2 | 946.96 | -1.47452 | 869.787 | +171.1 |
| 37 | 1 | 24 | 45 | 2 | 940.75 | -1.47452 | 869.787 | +171.1 |
| 38 | 1 | 24 | 46 | 2 | 934.53 | -1.47452 | 869.787 | +171.1 |
| 39 | 1 | 24 | 47 | 2 | 928.32 | -1.47452 | 869.787 | +171.1 |
| 40 | 1 | 24 | 48 | 2 | 922.11 | -1.47452 | 869.787 | +171.1 |
| 41 | 1 | 24 | 49 | 2 | 915.90 | -1.47452 | 869.787 | +171.1 |
| 42 | 1 | 24 | 50 | 2 | 909.69 | -1.47452 | 869.787 | +171.1 |
| 43 | 1 | 24 | 51 | 2 | 903.48 | -1.47452 | 869.787 | +171.1 |
| 44 | 1 | 24 | 52 | 2 | 897.27 | -1.47452 | 869.787 | +171.1 |
| 45 | 1 | 24 | 53 | 2 | 891.06 | -1.47452 | 869.787 | +171.1 |
| 46 | 1 | 24 | 54 | 2 | 884.85 | -1.47452 | 869.787 | +171.1 |
| 47 | 1 | 24 | 55 | 2 | 878.64 | -1.47452 | 869.787 | +171.1 |
| 48 | 1 | 24 | 56 | 2 | 872.43 | -1.47452 | 869.787 | +171.1 |
| 49 | 1 | 24 | 57 | 2 | 866.22 | -1.47452 | 869.787 | +171.1 |
| 50 | 1 | 24 | 58 | 2 | 860.01 | -1.47452 | 869.787 | +171.1 |
| 51 | 1 | 24 | 59 | 2 | 853.80 | -1.47452 | 869.787 | +171.1 |
| 52 | 1 | 24 | 60 | 2 | 847.59 | -1.47452 | 869.787 | +171.1 |
| 53 | 1 | 24 | 61 | 2 | 841.38 | -1.47452 | 869.787 | +171.1 |
| 54 | 1 | 24 | 62 | 2 | 835.17 | -1.47452 | 869.787 | +171.1 |
| 55 | 1 | 24 | 63 | 2 | 828.96 | -1.47452 | 869.787 | +171.1 |
| 56 | 1 | 24 | 64 | 2 | 822.75 | -1.47452 | 869.787 | +171.1 |
| 57 | 1 | 24 | 65 | 2 | 816.54 | -1.47452 | 869.787 | +171.1 |
| 58 | 1 | 24 | 66 | 2 | 810.33 | -1.47452 | 869.787 | +171.1 |
| 59 | 1 | 24 | 67 | 2 | 804.12 | -1.47452 | 869.787 | +171.1 |
| 60 | 1 | 24 | 68 | 2 | 797.91 | -1.47452 | 869.787 | +171.1 |
| 61 | 1 | 24 | 69 | 2 | 791.70 | -1.47452 | 869.787 | +171.1 |
| 62 | 1 | 24 | 70 | 2 | 785.49 | -1.47452 | 869.787 | +171.1 |
| 63 | 1 | 24 | 71 | 2 | 779.28 | -1.47452 | 869.787 | +171.1 |
| 64 | 1 | 24 | 72 | 2 | 773.07 | -1.47452 | 869.787 | +171.1 |
| 65 | 1 | 24 | 73 | 2 | 766.86 | -1.47452 | 869.787 | +171.1 |
| 66 | 1 | 24 | 74 | 2 | 760.65 | -1.47452 | 869.787 | +171.1 |
| 67 | 1 | 24 | 75 | 2 | 754.44 | -1.47452 | 869.787 | +171.1 |
| 68 | 1 | 24 | 76 | 2 | 748.23 | -1.47452 | 869.787 | +171.1 |
| 69 | 1 | 24 | 77 | 2 | 742.02 | -1.47452 | 869.787 | +171.1 |
| 70 | 1 | 24 | 78 | 2 | 735.81 | -1.47452 | 869.787 | +171.1 |
| 71 | 1 | 24 | 79 | 2 | 729.60 | -1.47452 | 869.787 | +171.1 |
| 72 | 1 | 24 | 80 | 2 | 723.39 | -1.47452 | 869.787 | +171.1 |
| 73 | 1 | 24 | 81 | 2 | 717.18 | -1.47452 | 869.787 | +171.1 |
| 74 | 1 | 24 | 82 | 2 | 710.97 | -1.47452 | 869.787 | +171.1 |
| 75 | 1 | 24 | 83 | 2 | 704.76 | -1.47452 | 869.787 | +171.1 |
| 76 | 1 | 24 | 84 | 2 | 698.55 | -1.47452 | 869.787 | +171.1 |
| 77 | 1 | 24 | 85 | 2 | 692.34 | -1.47452 | 869.787 | +171.1 |
| 78 | 1 | 24 | 86 | 2 | 686.13 | -1.47452 | 869.787 | +171.1 |
| 79 | 1 | 24 | 87 | 2 | 679.92 | -1.47452 | 869.787 | +171.1 |
| 80 | 1 | 24 | 88 | 2 | 673.71 | -1.47452 | 869.787 | +171.1 |
| 81 | 1 | 24 | 89 | 2 | 667.50 | -1.47452 | 869.787 | +171.1 |
| 82 | 1 | 24 | 90 | 2 | 661.29 | -1.47452 | 869.787 | +171.1 |
| 83 | 1 | 24 | 91 | 2 | 655.08 | -1.47452 | 869.787 | +171.1 |
| 84 | 1 | 24 | 92 | 2 | 648.87 | -1.47452 | 869.787 | +171.1 |
| 85 | 1 | 24 | 93 | 2 | 642.66 | -1.47452 | 869.787 | +171.1 |
| 86 | 1 | 24 | 94 | 2 | 636.45 | -1.47452 | 869.787 | +171.1 |
| 87 | 1 | 24 | 95 | 2 | 630.24 | -1.47452 | 869.787 | +171.1 |
| 88 | 1 | 24 | 96 | 2 | 624.03 | -1.47452 | 869.787 | +171.1 |
| 89 | 1 | 24 | 97 | 2 | 617.82 | -1.47452 | 869.787 | +171.1 |
| 90 | 1 | 24 | 98 | 2 | 611.61 | -1.47452 | 869.787 | +171.1 |
| 91 | 1 | 24 | 99 | 2 | 605.40 | -1.47452 | 869.787 | +171.1 |
| 92 | 1 | 24 | 100 | 2 | 599.19 | -1.47452 | 869.787 | +171.1 |
| 93 | 1 | 24 | 101 | 2 | 592.98 | -1.47452 | 869.787 | +171.1 |
| 94 | 1 | 24 | 102 | 2 | 586.77 | -1.47452 | 869.787 | +171.1 |
| 95 | 1 | 24 | 103 | 2 | 580.56 | -1.47452 | 869.787 | +171.1 |
| 96 | 1 | 24 | 104 | 2 | 574.35 | -1.47452 | 869.787 | +171.1 |
| 97 | 1 | 24 | 105 | 2 | 568.14 | -1.47452 | 869.787 | +171.1 |
| 98 | 1 | 24 | 106 | 2 | 561.93 | -1.47452 | 869.787 | +171.1 |
| 99 | 1 | 24 | 107 | 2 | 555.72 | -1.47452 | 869.787 | +171.1 |
| 100 | 1 | 24 | 108 | 2 | 549.51 | -1.47452 | 869.787 | +171.1 |
| 101 | 1 | 24 | 109 | 2 | 543.30 | -1.47452 | 869.787 | +171.1 |
| 102 | 1 | 24 | 110 | 2 | 537.09 | -1.47452 | 869.787 | +171.1 |
| 103 | 1 | 24 | 111 | 2 | 530.88 | -1.47452 | 869.787 | +171.1 |
| 104 | 1 | 24 | 112 | 2 | 524.67 | -1.47452 | 869.787 | +171.1 |
| 105 | 1 | 24 | 113 | 2 | 518.46 | -1.47452 | 869.787 | +171.1 |
| 106 | 1 | 24 | 114 | 2 | 512.25 | -1.47452 | 869.787 | +171.1 |
| 107 | 1 | 24 | 115 | 2 | 506.04 | -1.47452 | 869.787 | +171.1 |
| 108 | 1 | 24 | 116 | 2 | 509.83 | -1.47452 | 869.787 | +171.1 |
| 109 | 1 | 24 | 117 | 2 | 503.62 | -1.47452 | 869.787 | +171.1 |
| 110 | 1 | 24 | 118 | 2 | 497.41 | -1.47452 | 869.787 | +171.1 |
| 111 | 1 | 24 | 119 | 2 | 491.20 | -1.47452 | 869.787 | +171.1 |
| 112 | 1 | 24 | 120 | 2 | 484.99 | -1.47452 | 869.787 | +171.1 |
| 113 | 1 | 24 | 121 | 2 | 478.78 | -1.47452 | 869.787 | +171.1 |
| 114 | 1 | 24 | 122 | 2 | 472.57 | -1.47452 | 869.787 | +171.1 |
| 115 | 1 | 24 | 123 | 2 | 466.36 | -1.47452 | 869.787 | +171.1 |
| 116 | 1 | 24 | 124 | 2 | 460.15 | -1.47452 | 869.787 | +171.1 |
| 117 | 1 | 24 | 125 | 2 | 453.94 | -1.47452 | 869.787 | +171.1 |
| 118 | 1 | 24 | 126 | 2 | 447.73 | -1.47452 | 869.787 | +171.1 |
| 119 | 1 | 24 | 127 | 2 | 441.52 | -1.47452 | 869.787 | +171.1 |
| 120 | 1 | 24 | 128 | 2 | 435.31 | -1.47452 | 869.787 | +171.1 |
| 121 | 1 | 24 | 129 | 2 | 429.10 | -1.47452 | 869.787 | +171.1 |
| 122 | 1 | 24 | 130 | 2 | 422.89 | -1.47452 | 869.787 | +171.1 |
| 123 | 1 | 24 | 131 | 2 | 416.68 | -1.47452 | 869.787 | +171.1 |
| 124 | 1 | 24 | 132 | 2 | 410.47 | -1.47452 | 869.787 | +171.1 |
| 125 | 1 | 24 | 133 | 2 | 404.26 | -1.47452 | 869.787 | +171.1 |
| 126 | 1 | 24 | 134 | 2 | 398.05 | -1.47452 | 869.787 | +171.1 |
| 127 | 1 | 24 | 135 | 2 | 391.84 | -1.47452 | 869.787 | +171.1 |
| 128 | 1 | 24 | 136 | 2 | 385.63 | -1.47452 | 869.787 | +171.1 |
| 129 | 1 | 24 | 137 | 2 | 379.42 | -1.47452 | 869.787 | +171.1 |
| 130 | 1 | 24 | 138 | 2 | 373.21 | -1.47452 | 869.787 | +171.1 |
| 131 | 1 | 24 | 139 | 2 | 366.99 | -1.47452 | 869.787 | +171.1 |
| 132 | 1 | 24 | 140 | 2 | 360.78 | -1.47452 | 869.787 | +171.1 |
| 133 | 1 | 24 | 141 | 2 | 354.57 | -1.47452 | 869.787 | +171.1 |
| 134 | 1 | 24 | 142 | 2 | 348.36 | -1.47452 | 869.787 | +171.1 |
| 135 | 1 | 24 | 143 | 2 | 342.15 | -1.47452 | 869.787 | +171.1 |
| 136 | 1 | 24 | 144 | 2 | 335.94 | -1.47452 | 869.787 | +171.1 |
| 137 | 1 | 24 | 145 | 2 | 329.73</ | | | |

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| 149 | 1 | 81 | 6 | 67.79115 | -14.19311 | 131.912 -96.6 0 |
|-----|---|-----|---|----------|-----------|-----------------|
| 150 | 1 | 82 | 6 | 68.76525 | -13.39495 | 135.617 -97.1 0 |
| 151 | 1 | 83 | 6 | 69.11727 | -13.89597 | 135.640 -97.4 0 |
| 152 | 1 | 84 | 6 | 69.09531 | -13.31193 | 135.671 -97.7 0 |
| 153 | 1 | 85 | 6 | 69.15931 | -13.81295 | 135.693 -97.9 0 |
| 154 | 1 | 86 | 6 | 69.14531 | -13.32397 | 135.715 -98.1 0 |
| 155 | 1 | 87 | 6 | 69.14531 | -13.82499 | 135.736 -98.3 0 |
| 156 | 1 | 88 | 6 | 69.14531 | -13.33599 | 135.757 -98.5 0 |
| 157 | 1 | 89 | 6 | 69.14531 | -13.83699 | 135.778 -98.7 0 |
| 158 | 1 | 90 | 6 | 69.14531 | -13.34799 | 135.799 -98.9 0 |
| 159 | 1 | 91 | 6 | 69.14531 | -13.84899 | 135.820 -99.1 0 |
| 160 | 1 | 92 | 6 | 69.14531 | -13.35999 | 135.841 -99.3 0 |
| 161 | 1 | 93 | 6 | 69.14531 | -13.86099 | 135.862 -99.5 0 |
| 162 | 1 | 94 | 6 | 69.14531 | -13.37199 | 135.883 -99.7 0 |
| 163 | 1 | 95 | 6 | 69.14531 | -13.87299 | 135.904 -99.9 0 |
| 164 | 1 | 96 | 6 | 69.14531 | -13.38399 | 135.925 -99.9 0 |
| 165 | 1 | 97 | 6 | 69.14531 | -13.88499 | 135.946 -99.9 0 |
| 166 | 1 | 98 | 6 | 69.14531 | -13.39599 | 135.967 -99.9 0 |
| 167 | 1 | 99 | 6 | 69.14531 | -13.89699 | 135.988 -99.9 0 |
| 168 | 1 | 100 | 6 | 69.14531 | -13.40799 | 136.009 -99.9 0 |
| 169 | 1 | 101 | 6 | 69.14531 | -13.90899 | 136.030 -99.9 0 |
| 170 | 1 | 102 | 6 | 69.14531 | -13.41999 | 136.051 -99.9 0 |
| 171 | 1 | 103 | 6 | 69.14531 | -13.92099 | 136.072 -99.9 0 |
| 172 | 1 | 104 | 6 | 69.14531 | -13.42999 | 136.093 -99.9 0 |
| 173 | 1 | 105 | 6 | 69.14531 | -13.93199 | 136.114 -99.9 0 |
| 174 | 1 | 106 | 6 | 69.14531 | -13.44099 | 136.135 -99.9 0 |
| 175 | 1 | 107 | 6 | 69.14531 | -13.94199 | 136.156 -99.9 0 |
| 176 | 1 | 108 | 6 | 69.14531 | -13.45199 | 136.177 -99.9 0 |
| 177 | 1 | 109 | 6 | 69.14531 | -13.95299 | 136.198 -99.9 0 |
| 178 | 1 | 110 | 6 | 69.14531 | -13.46299 | 136.219 -99.9 0 |
| 179 | 1 | 111 | 6 | 69.14531 | -13.96399 | 136.240 -99.9 0 |
| 180 | 1 | 112 | 6 | 69.14531 | -13.47299 | 136.261 -99.9 0 |
| 181 | 1 | 113 | 6 | 69.14531 | -13.97499 | 136.282 -99.9 0 |
| 182 | 1 | 114 | 6 | 69.14531 | -13.48199 | 136.303 -99.9 0 |
| 183 | 1 | 115 | 6 | 69.14531 | -13.98599 | 136.324 -99.9 0 |
| 184 | 1 | 116 | 6 | 69.14531 | -13.49199 | 136.345 -99.9 0 |
| 185 | 1 | 117 | 6 | 69.14531 | -13.99699 | 136.366 -99.9 0 |
| 186 | 1 | 118 | 6 | 69.14531 | -13.50199 | 136.387 -99.9 0 |
| 187 | 1 | 119 | 6 | 69.14531 | -13.99799 | 136.408 -99.9 0 |
| 188 | 1 | 120 | 6 | 69.14531 | -13.51199 | 136.429 -99.9 0 |
| 189 | 1 | 121 | 6 | 69.14531 | -13.99899 | 136.450 -99.9 0 |
| 190 | 1 | 122 | 6 | 69.14531 | -13.51699 | 136.471 -99.9 0 |
| 191 | 1 | 123 | 6 | 69.14531 | -13.99999 | 136.492 -99.9 0 |
| 192 | 1 | 124 | 6 | 69.14531 | -13.52399 | 136.513 -99.9 0 |
| 193 | 1 | 125 | 6 | 69.14531 | -13.99999 | 136.534 -99.9 0 |
| 194 | 1 | 126 | 6 | 69.14531 | -13.53499 | 136.555 -99.9 0 |
| 195 | 1 | 127 | 6 | 69.14531 | -13.99999 | 136.576 -99.9 0 |
| 196 | 1 | 128 | 6 | 69.14531 | -13.53999 | 136.597 -99.9 0 |
| 197 | 1 | 129 | 6 | 69.14531 | -13.99999 | 136.618 -99.9 0 |
| 198 | 1 | 130 | 6 | 69.14531 | -13.54899 | 136.639 -99.9 0 |
| 199 | 1 | 131 | 6 | 69.14531 | -13.99999 | 136.660 -99.9 0 |
| 200 | 1 | 132 | 6 | 69.14531 | -13.55799 | 136.681 -99.9 0 |
| 201 | 1 | 133 | 6 | 69.14531 | -13.99999 | 136.702 -99.9 0 |
| 202 | 1 | 134 | 6 | 69.14531 | -13.56699 | 136.723 -99.9 0 |
| 203 | 1 | 135 | 6 | 69.14531 | -13.99999 | 136.744 -99.9 0 |
| 204 | 1 | 136 | 6 | 69.14531 | -13.57599 | 136.765 -99.9 0 |
| 205 | 1 | 137 | 6 | 69.14531 | -13.99999 | 136.786 -99.9 0 |
| 206 | 1 | 138 | 6 | 69.14531 | -13.58499 | 136.807 -99.9 0 |
| 207 | 1 | 139 | 6 | 69.14531 | -13.99999 | 136.828 -99.9 0 |
| 208 | 1 | 140 | 6 | 69.14531 | -13.59399 | 136.849 -99.9 0 |
| 209 | 1 | 141 | 6 | 69.14531 | -13.99999 | 136.870 -99.9 0 |
| 210 | 1 | 142 | 6 | 69.14531 | -13.60299 | 136.891 -99.9 0 |
| 211 | 1 | 143 | 6 | 69.14531 | -13.99999 | 136.912 -99.9 0 |
| 212 | 1 | 144 | 6 | 69.14531 | -13.61199 | 136.933 -99.9 0 |
| 213 | 1 | 145 | 6 | 69.14531 | -13.99999 | 136.954 -99.9 0 |
| 214 | 1 | 146 | 6 | 69.14531 | -13.61999 | 136.975 -99.9 0 |
| 215 | 1 | 147 | 6 | 69.14531 | -13.99999 | 137.006 -99.9 0 |
| 216 | 1 | 148 | 6 | 69.14531 | -13.62899 | 137.027 -99.9 0 |
| 217 | 1 | 149 | 6 | 69.14531 | -13.99999 | 137.048 -99.9 0 |
| 218 | 1 | 150 | 6 | 69.14531 | -13.63799 | 137.069 -99.9 0 |
| 219 | 1 | 151 | 6 | 69.14531 | -13.99999 | 137.090 -99.9 0 |
| 220 | 1 | 152 | 6 | 69.14531 | -13.64699 | 137.111 -99.9 0 |
| 221 | 1 | 153 | 6 | 69.14531 | -13.99999 | 137.132 -99.9 0 |
| 222 | 1 | 154 | 6 | 69.14531 | -13.65599 | 137.153 -99.9 0 |
| 223 | 1 | 155 | 6 | 69.14531 | -13.99999 | 137.174 -99.9 0 |
| 224 | 1 | 156 | 6 | 69.14531 | -13.66499 | 137.195 -99.9 0 |
| 225 | 1 | 157 | 6 | 69.14531 | -13.99999 | 137.216 -99.9 0 |
| 226 | 1 | 158 | 6 | 69.14531 | -13.67399 | 137.237 -99.9 0 |
| 227 | 1 | 159 | 6 | 69.14531 | -13.99999 | 137.258 -99.9 0 |
| 228 | 1 | 160 | 6 | 69.14531 | -13.68299 | 137.279 -99.9 0 |
| 229 | 1 | 161 | 6 | 69.14531 | -13.99999 | 137.299 -99.9 0 |
| 230 | 1 | 162 | 6 | 69.14531 | -13.69199 | 137.320 -99.9 0 |
| 231 | 1 | 163 | 6 | 69.14531 | -13.99999 | 137.341 -99.9 0 |
| 232 | 1 | 164 | 6 | 69.14531 | -13.69999 | 137.362 -99.9 0 |
| 233 | 1 | 165 | 6 | 69.14531 | -13.99999 | 137.383 -99.9 0 |
| 234 | 1 | 166 | 6 | 69.14531 | -13.70899 | 137.404 -99.9 0 |
| 235 | 1 | 167 | 6 | 69.14531 | -13.99999 | 137.425 -99.9 0 |
| 236 | 1 | 168 | 6 | 69.14531 | -13.71799 | 137.446 -99.9 0 |
| 237 | 1 | 169 | 6 | 69.14531 | -13.99999 | 137.467 -99.9 0 |
| 238 | 1 | 170 | 6 | 69.14531 | -13.72699 | 137.488 -99.9 0 |
| 239 | 1 | 171 | 6 | 69.14531 | -13.99999 | 137.509 -99.9 0 |
| 240 | 1 | 172 | 6 | 69.14531 | -13.73599 | 137.530 -99.9 0 |
| 241 | 1 | 173 | 6 | 69.14531 | -13.99999 | 137.551 -99.9 0 |

THE TOTAL NUMBER OF LINES PRINTED FOR THIS JOB WAS

740

Fig. 7 (Continued) — Example of the output from RAYZDIST (fourth of four pages)

Subroutine CHANNEL

Subroutine CHANNEL calculates CM (vertex velocity) from ZR (ray depth) and T (tangent of the ray angle) and then finds ZTO (ray turnover depth) and ZTU (ray turn-under depth). The entry RCALC then calculates

$$R = \int_{ZTO}^{ZTU} \frac{1}{\tan \theta} dz,$$

where R is the cycle length of the ray, which is used for the type III intensity calculations. The entry WDENS then calculates the probability density $P(z)$ that a ray will be found at a depth z :

$$P(z) = \frac{1}{(\tan \theta)/R},$$

which is the type III depth distribution.

Subroutine VELCALC

Subroutine VELCALC calculates a velocity profile at each selected range for internal calculations (not a profile range or bottom point) using the information in the common block /TRIANG/.

Subroutine RAYPLOT

Each entry to RAYPLOT plots one line of the printer plot. In addition the first entry prints the heading for the plot, determines which rays will be plotted, and sets the scale. NP and ZMAX are used only on the first entry. Fig. 8 is an example of the printer plot.

Subroutine PROFPLIT

Subroutine PROFPLIT plots both the input and interpolated profiles on a Calcomp plot. They may be plotted in nautical miles or kilometers. The total plot length is specified in inches. The bottom track is also plotted.

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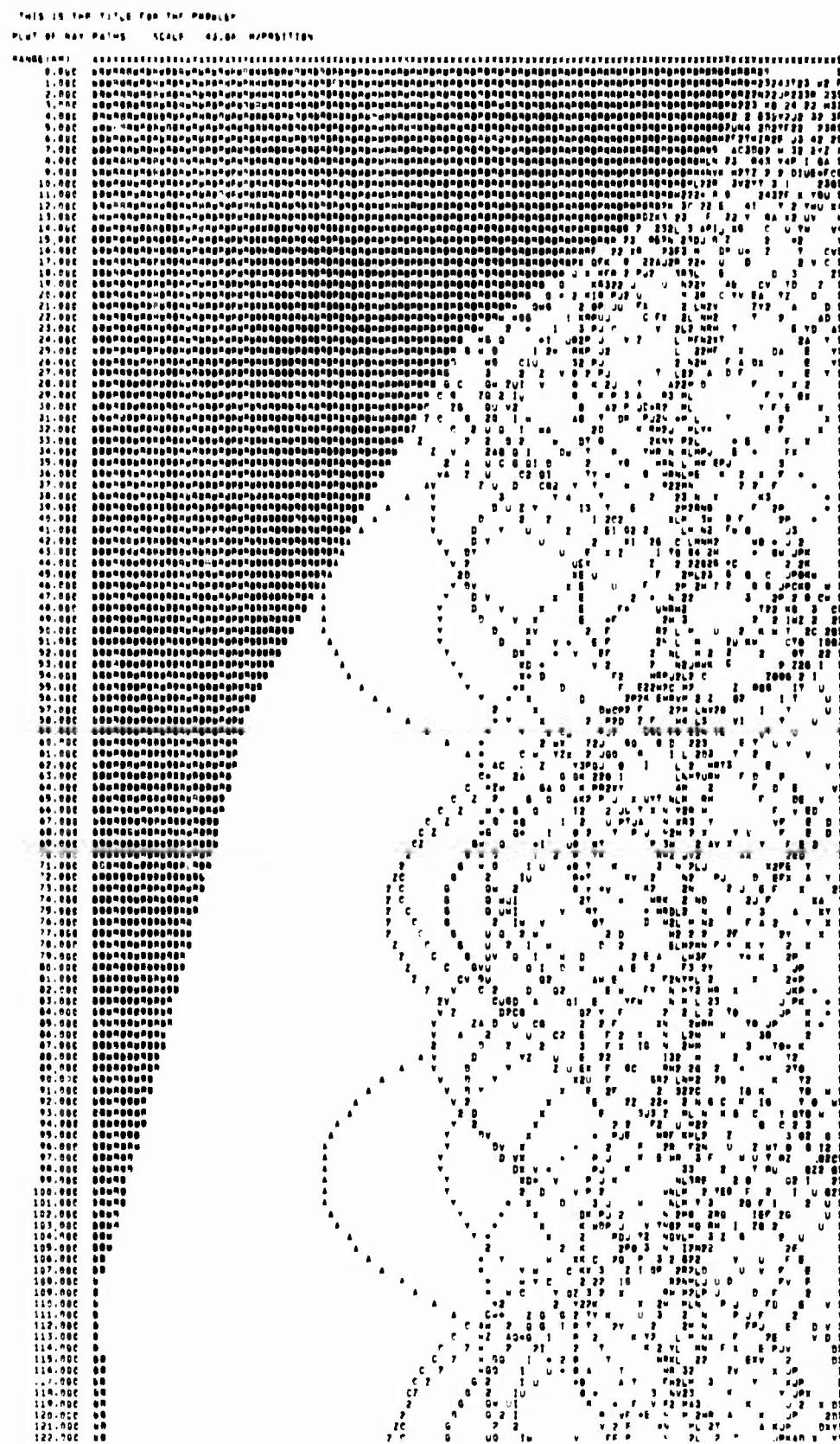
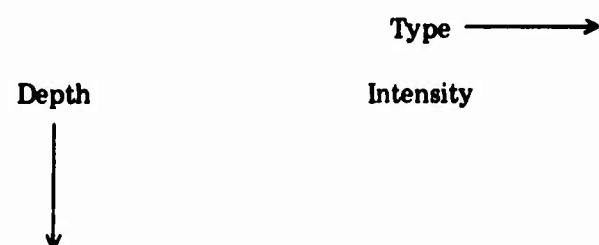


Fig. 8 — Ray plot

Subroutine ITNPRINT

Subroutine ITNPRINT prints out the intensities. If receiver depths are the same for all intensity calculations, a table of intensities such as shown in Fig. 9 is printed. Otherwise a printer plot for each range with the arrangement



is printed.

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| THIS IS THE TITLE FOR THE PROBLEM | | AT DEPTHS | | | | |
|-----------------------------------|------|-----------|---------|---------|---------|---------|
| RECEIVED INTENSITY VS RANGE | | | | | | |
| R(KM) | TYPE | 50,000 | 100,000 | 250,000 | 300,000 | 450,000 |
| 1,000 | R | -97.4 | -97.5 | -97.5 | -97.6 | -97.3 |
| 2,000 | R | -82.3 | -82.0 | -82.7 | -82.7 | -82.4 |
| 3,000 | R | -69.4 | -69.1 | -69.4 | -69.0 | -69.0 |
| 4,000 | R | -67.6 | -69.1 | -68.5 | -69.6 | -69.3 |
| 5,000 | S | -71.0 | -72.3 | -72.0 | -73.6 | -70.0 |
| 6,000 | R | -69.3 | -71.3 | -70.6 | -70.9 | -70.9 |
| 7,000 | R | -70.4 | -69.1 | -68.4 | -72.4 | -72.4 |
| 8,000 | R | -77.4 | -80.1 | -71.6 | -70.6 | -74.2 |
| 9,000 | R | -80.0 | -84.6 | -79.4 | -70.2 | -72.0 |
| 10,000 | R | -78.4 | -89.8 | -76.2 | -79.3 | -79.9 |
| 10,000 | T | -80.1 | -77.9 | -77.3 | -70.6 | -74.3 |
| 10,000 | R | -82.4 | -85.1 | -78.6 | -77.1 | -74.0 |
| 11,000 | R | -89.4 | -87.4 | -87.7 | -80.1 | -78.2 |
| 12,000 | R | -91.6 | -83.8 | -87.7 | -80.8 | -81.2 |
| 13,000 | R | -93.1 | -85.9 | -84.4 | -84.0 | -87.3 |
| 14,000 | R | -94.9 | -86.9 | -87.6 | -87.9 | -84.7 |
| 15,000 | S | -94.6 | -83.7 | -82.6 | -81.6 | -79.4 |
| 16,000 | R | -94.3 | -87.8 | -88.3 | -88.7 | -89.0 |
| 16,000 | R | -92.1 | -88.5 | -87.3 | -86.3 | -86.9 |
| 17,000 | R | -114.7 | -96.4 | -96.6 | -90.0 | -90.5 |
| 18,000 | R | -119.7 | -113.7 | -99.7 | -80.1 | -91.6 |
| 19,000 | R | -113.8 | -114.4 | -93.3 | -85.7 | -89.0 |
| 20,000 | S | -99.5 | -86.7 | -84.1 | -82.3 | -73.9 |
| 20,000 | R | -118.4 | -115.3 | -114.0 | -94.9 | -98.9 |
| 21,000 | R | -129.6 | -117.9 | -121.3 | -123.4 | -88.7 |
| 22,000 | R | -138.0 | -120.1 | -120.3 | -123.3 | -122.9 |
| 23,000 | R | -143.0 | -119.4 | -121.5 | -121.6 | -123.9 |
| 24,000 | R | -145.4 | -127.0 | -121.5 | -123.0 | -123.0 |
| 25,000 | S | -98.2 | -87.8 | -84.5 | -79.3 | -84.1 |
| 25,000 | R | -143.0 | -132.2 | -120.6 | -123.2 | -123.3 |
| 26,000 | R | -142.7 | -139.9 | -121.2 | -127.9 | -125.2 |
| 27,000 | R | -147.1 | -132.7 | -179.0 | -123.7 | -98.9 |
| 28,000 | R | -145.5 | -143.8 | -118.8 | -124.0 | -99.4 |
| 29,000 | R | -147.1 | -141.8 | -109.8 | -123.3 | -99.6 |
| 30,000 | S | -98.0 | -88.7 | -85.3 | -84.6 | -84.9 |
| 30,000 | R | -150.9 | -132.9 | -117.6 | -122.9 | -99.4 |
| 31,000 | R | -159.8 | -134.7 | -116.9 | -123.0 | -121.9 |
| 32,000 | R | -160.2 | -134.1 | -114.6 | -124.0 | -111.2 |
| 33,000 | R | -159.9 | -145.8 | -121.9 | -124.2 | -113.3 |
| 34,000 | R | -160.0 | -136.8 | -123.0 | -114.2 | -114.3 |
| 35,000 | S | -100.8 | -89.3 | -88.0 | -85.2 | -85.6 |
| 35,000 | R | -146.6 | -139.3 | -123.5 | -114.5 | -92.9 |
| 36,000 | R | -146.0 | -165.7 | -121.4 | -117.9 | -94.0 |
| 37,000 | R | -165.6 | -139.5 | -127.5 | -118.5 | -86.3 |
| 38,000 | R | -163.6 | -121.4 | -126.6 | -118.9 | -89.6 |
| 39,000 | R | -164.0 | -124.3 | -124.1 | -119.8 | -89.1 |
| 40,000 | S | -101.6 | -89.9 | -86.6 | -85.8 | -86.2 |
| 40,000 | R | -163.1 | -124.8 | -101.4 | -88.0 | -86.3 |
| 41,000 | R | -164.0 | -104.3 | -88.9 | -78.3 | -88.4 |
| 42,000 | R | -102.3 | -101.7 | -81.3 | -79.9 | -87.0 |
| 43,000 | R | -94.3 | -94.7 | -81.3 | -81.1 | -82.3 |
| 44,000 | R | -96.4 | -96.4 | -84.3 | -80.9 | -83.6 |
| 45,000 | S | -102.3 | -86.6 | -87.1 | -86.3 | -86.7 |
| 45,000 | R | -97.5 | -97.4 | -82.9 | -82.2 | -83.0 |
| 46,000 | R | -98.5 | -99.4 | -79.2 | -81.3 | -83.5 |
| 47,000 | R | -99.1 | -98.9 | -83.1 | -85.0 | -79.0 |
| 48,000 | R | -99.6 | -99.8 | -83.3 | -81.6 | -78.9 |
| 49,000 | R | -100.1 | -100.7 | -81.6 | -87.7 | -84.1 |
| 50,000 | S | -102.9 | -90.9 | -87.6 | -86.8 | -87.1 |
| 50,000 | R | -100.4 | -84.5 | -78.8 | -88.5 | -85.2 |
| 51,000 | R | -99.7 | -85.7 | -75.3 | -88.9 | -89.6 |
| 52,000 | R | -101.3 | -74.0 | -84.3 | -86.7 | -89.1 |
| 53,000 | R | -101.2 | -79.2 | -82.8 | -84.4 | -87.9 |
| 54,000 | R | -100.9 | -85.0 | -82.5 | -84.1 | -89.2 |
| 55,000 | S | -103.4 | -91.3 | -88.0 | -84.9 | -87.5 |
| 55,000 | R | -120.0 | -92.3 | -85.1 | -86.4 | -89.0 |
| 56,000 | R | -103.4 | -91.1 | -85.2 | -86.7 | -86.8 |
| 57,000 | R | -89.1 | -85.3 | -94.2 | -86.3 | -89.2 |
| 58,000 | R | -93.5 | -91.0 | -88.3 | -101.3 | -94.6 |
| 59,000 | R | -99.4 | -93.8 | -94.2 | -100.9 | -96.5 |
| 60,000 | S | -103.9 | -81.7 | -88.3 | -83.1 | -87.9 |
| 60,000 | R | -110.0 | -83.8 | -97.1 | -97.6 | -93.6 |
| 61,000 | R | -110.1 | -94.0 | -97.9 | -98.3 | -98.9 |
| 62,000 | R | -118.4 | -110.1 | -101.5 | -100.5 | -98.8 |
| 63,000 | R | -177.1 | -107.9 | -100.7 | -101.1 | -101.1 |
| 64,000 | R | -108.7 | -108.5 | -97.0 | -102.0 | -102.6 |
| 65,000 | S | -104.3 | -92.0 | -88.7 | -87.9 | -88.3 |
| 65,000 | R | -115.1 | -108.9 | -104.9 | -99.1 | -102.7 |
| 66,000 | R | -128.9 | -114.5 | -113.7 | -100.2 | -100.0 |
| 67,000 | R | -140.4 | -124.1 | -122.0 | -128.9 | -101.5 |
| 68,000 | R | -133.0 | -125.7 | -119.9 | -129.9 | -127.7 |
| 69,000 | R | -135.3 | -123.3 | -122.2 | -130.5 | -119.1 |
| 70,000 | S | -105.1 | -92.4 | -87.0 | -88.3 | -88.6 |
| 70,000 | R | -138.1 | -138.0 | -127.4 | -125.0 | -120.2 |
| 71,000 | R | -138.9 | -130.2 | -129.5 | -116.6 | -111.6 |
| 72,000 | R | -144.4 | -135.2 | -127.4 | -120.2 | -93.4 |
| 73,000 | R | -142.3 | -136.7 | -120.5 | -121.3 | -87.1 |
| 74,000 | R | -140.9 | -143.8 | -130.0 | -123.7 | -87.4 |
| 75,000 | S | -105.3 | -92.7 | -89.3 | -88.9 | -88.9 |
| 76,000 | R | -144.4 | -137.2 | -135.9 | -124.0 | -87.3 |
| 76,000 | R | -139.9 | -138.0 | -130.3 | -123.2 | -81.1 |
| 77,000 | R | -136.4 | -144.6 | -138.8 | -130.2 | -91.6 |
| 78,000 | R | -136.8 | -134.8 | -130.8 | -84.4 | -92.9 |
| 79,000 | R | -136.9 | -141.0 | -130.0 | -82.7 | -87.7 |
| 80,000 | S | -105.6 | -93.0 | -89.6 | -88.6 | -89.2 |
| 80,000 | R | -300.0 | -143.2 | -128.6 | -85.9 | -87.5 |
| 81,000 | R | -400.0 | -301.2 | -90.9 | -83.9 | -87.4 |
| 82,000 | R | -300.0 | -146.5 | -92.1 | -86.2 | -89.5 |
| 83,000 | R | -171.1 | -124.6 | -88.6 | -87.5 | -89.3 |
| 84,000 | R | -111.1 | -111.1 | -88.5 | -91.8 | -89.1 |

Fig. 9 — Example of an output from ITNPRINT (first of three pages). The symbols that the subroutine uses in the second column are R for type I random phase calculations, S for type I coherent phase calculations, 2 for type II calculations, and 3 for type III calculations.

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| | | | | | | |
|---------|---|--------|--------|-------|-------|-------|
| 69.000 | 1 | -109.7 | -93.2 | -89.8 | -89.1 | -89.4 |
| 69.000 | 2 | -113.1 | -113.1 | -95.4 | -95.4 | -93.3 |
| 69.000 | 3 | -101.7 | -102.7 | -95.5 | -93.9 | -97.0 |
| 69.000 | 4 | -103.4 | -103.5 | -97.4 | -97.0 | -97.7 |
| 69.000 | 5 | -104.5 | -104.5 | -98.1 | -97.0 | -96.6 |
| 69.000 | 6 | -109.2 | -109.2 | -94.7 | -97.1 | -91.3 |
| 69.000 | 7 | -106.1 | -93.4 | -90.1 | -88.3 | -89.7 |
| 69.000 | 8 | -105.8 | -105.6 | -97.2 | -96.8 | -99.2 |
| 69.000 | 9 | -109.9 | -103.7 | -96.1 | -94.8 | -99.1 |
| 72.000 | 2 | -106.1 | -99.7 | -91.2 | -90.4 | -93.8 |
| 73.000 | 2 | -106.2 | -106.2 | -89.8 | -79.0 | -98.2 |
| 74.000 | 2 | -106.1 | -106.2 | -88.2 | -88.7 | -95.5 |
| 75.000 | 3 | -106.3 | -93.7 | -92.3 | -89.6 | -95.9 |
| 75.000 | 4 | -106.0 | -91.4 | -97.2 | -90.6 | -93.0 |
| 76.000 | 2 | -109.6 | -91.0 | -88.4 | -87.6 | -91.7 |
| 77.000 | 2 | -88.2 | -88.9 | -89.7 | -91.3 | -92.9 |
| 78.000 | 2 | -103.8 | -89.3 | -90.1 | -90.2 | -91.7 |
| 79.000 | 2 | -103.4 | -87.6 | -87.9 | -90.4 | -90.8 |
| 100.000 | 3 | -106.6 | -93.9 | -90.6 | -89.8 | -90.1 |
| 100.000 | 3 | -106.8 | -93.9 | -90.6 | -89.8 | -90.1 |
| 100.000 | 4 | -112.5 | -97.9 | -90.4 | -89.8 | -95.9 |
| 100.000 | 5 | -107.0 | -94.2 | -90.8 | -90.0 | -90.3 |
| 110.000 | 3 | -109.4 | -95.9 | -91.1 | -88.4 | -90.6 |
| 115.000 | 1 | -106.2 | -93.3 | -91.5 | -88.9 | -90.8 |
| 120.000 | 3 | -106.6 | -93.4 | -91.8 | -89.3 | -91.0 |
| 125.000 | 1 | -107.2 | -93.7 | -92.0 | -89.7 | -91.2 |
| 130.000 | 3 | -107.6 | -91 | -92.2 | -90.5 | -91.4 |
| 135.000 | 1 | -95.5 | -91.1 | -92.1 | -90.5 | -91.7 |
| 140.000 | 3 | -99.8 | -91.8 | -91.6 | -90.4 | -91.9 |
| 145.000 | 3 | -100.1 | -92.2 | -91.9 | -90.8 | -92.1 |
| 150.000 | 3 | -100.3 | -90.5 | -92.4 | -91.0 | -92.3 |
| 155.000 | 3 | -101.4 | -92.9 | -92.7 | -91.2 | -92.4 |
| 160.000 | 3 | -101.7 | -92.7 | -92.9 | -90.6 | -92.6 |
| 165.000 | 3 | -101.9 | -91.1 | -92.3 | -90.9 | -92.7 |
| 170.000 | 3 | -99.2 | -91.6 | -92.3 | -91.4 | -92.0 |
| 175.000 | 3 | -100.3 | -92.6 | -92.8 | -91.5 | -93.1 |
| 180.000 | 3 | -101.0 | -90.4 | -93.1 | -91.0 | -93.2 |
| 185.000 | 3 | -131.4 | -91.8 | -93.4 | -91.9 | -93.4 |
| 190.000 | 3 | -101.6 | -91.4 | -90.8 | -92.1 | -91.4 |
| 195.000 | 3 | -101.9 | -92.3 | -91.5 | -92.3 | -93.5 |
| 200.000 | 3 | -97.6 | -92.7 | -91.8 | -92.5 | -93.7 |
| 205.000 | 3 | -97.8 | -92.7 | -91.8 | -92.5 | -93.7 |
| 210.000 | 3 | -100.1 | -93.3 | -92.6 | -93.0 | -94.0 |
| 215.000 | 3 | -100.0 | -93.3 | -93.1 | -93.2 | -94.1 |
| 220.000 | 1 | -101.2 | -93.6 | -93.5 | -93.3 | -94.2 |
| 225.000 | 3 | -78.3 | -93.9 | -91.9 | -93.4 | -94.4 |
| 230.000 | 3 | -99.1 | -94.2 | -92.3 | -93.6 | -94.4 |
| 235.000 | 3 | -99.3 | -94.4 | -92.9 | -93.7 | -94.5 |
| 240.000 | 3 | -99.5 | -94.6 | -93.0 | -93.7 | -94.6 |
| 245.000 | 3 | -98.1 | -94.8 | -93.6 | -94.0 | -94.8 |
| 250.000 | 3 | -99.2 | -94.7 | -90.6 | -94.1 | -94.9 |
| 255.000 | 3 | -99.6 | -94.3 | -93.1 | -94.3 | -95.0 |
| 260.000 | 3 | -98.5 | -94.4 | -93.5 | -94.4 | -95.1 |
| 265.000 | 3 | -99.2 | -92.8 | -93.7 | -94.5 | -95.0 |
| 270.000 | 3 | -99.2 | -93.7 | -93.9 | -94.6 | -95.2 |
| 275.000 | 3 | -99.6 | -93.8 | -92.1 | -94.7 | -95.3 |
| 280.000 | 3 | -99.6 | -94.2 | -93.5 | -94.8 | -95.4 |
| 285.000 | 3 | -100.0 | -94.7 | -92.7 | -95.0 | -95.5 |
| 290.000 | 3 | -100.3 | -95.0 | -93.6 | -95.1 | -95.6 |
| 295.000 | 3 | -100.6 | -95.3 | -93.8 | -95.2 | -95.7 |
| 300.000 | 3 | -100.4 | -93.7 | -94.0 | -95.3 | -95.8 |
| 305.000 | 3 | -100.4 | -95.0 | -94.0 | -95.3 | -95.9 |
| 310.000 | 3 | -100.7 | -94.6 | -94.1 | -95.4 | -96.0 |
| 315.000 | 1 | -100.9 | -94.8 | -94.4 | -95.5 | -96.1 |
| 320.000 | 3 | -100.6 | -94.0 | -94.7 | -95.6 | -96.2 |
| 325.000 | 3 | -98.4 | -95.1 | -94.9 | -95.7 | -95.4 |
| 330.000 | 3 | -99.8 | -94.6 | -95.1 | -95.9 | -95.4 |
| 335.000 | 4 | -100.3 | -93.3 | -95.2 | -96.0 | -95.7 |
| 340.000 | 3 | -100.6 | -94.9 | -95.3 | -96.0 | -95.9 |
| 345.000 | 3 | -100.9 | -94.7 | -95.2 | -96.1 | -95.6 |
| 350.000 | 3 | -101.1 | -93.8 | -95.4 | -96.2 | -95.5 |
| 355.000 | 3 | -101.2 | -94.7 | -95.6 | -96.2 | -95.9 |
| 360.000 | 3 | -101.4 | -95.0 | -95.7 | -96.2 | -96.1 |
| 365.000 | 3 | -101.3 | -94.5 | -95.8 | -96.3 | -96.2 |
| 370.000 | 1 | -101.6 | -94.7 | -95.9 | -96.4 | -96.3 |
| 375.000 | 3 | -101.8 | -94.9 | -96.0 | -96.5 | -96.4 |
| 380.000 | 3 | -99.2 | -94.8 | -96.1 | -96.6 | -96.3 |
| 385.000 | 3 | -100.2 | -95.0 | -96.2 | -96.6 | -96.6 |
| 390.000 | 1 | -100.8 | -95.2 | -96.2 | -96.8 | -95.3 |
| 395.000 | 1 | -101.0 | -95.7 | -96.3 | -96.8 | -96.1 |
| 400.000 | 1 | -99.7 | -95.5 | -96.4 | -96.9 | -96.5 |
| 405.000 | 1 | -99.7 | -95.5 | -96.4 | -96.9 | -96.5 |
| 410.000 | 3 | -99.2 | -95.9 | -96.5 | -96.2 | -96.8 |
| 415.000 | 3 | -97.8 | -95.9 | -96.6 | -96.0 | -96.9 |
| 420.000 | 1 | -98.1 | -96.1 | -96.7 | -96.2 | -97.0 |
| 425.000 | 3 | -97.6 | -96.2 | -96.8 | -96.3 | -97.1 |
| 430.000 | 3 | -96.8 | -96.3 | -96.9 | -96.5 | -97.1 |
| 435.000 | 1 | -96.9 | -96.9 | -97.0 | -96.2 | -97.2 |
| 440.000 | 3 | -97.4 | -96.6 | -97.0 | -96.7 | -97.2 |
| 445.000 | 3 | -97.8 | -96.7 | -97.1 | -96.9 | -97.3 |
| 450.000 | 3 | -93.9 | -96.9 | -97.3 | -97.0 | -97.4 |
| 455.000 | 3 | -93.2 | -97.0 | -96.4 | -97.1 | -97.5 |
| 460.000 | 3 | -96.1 | -97.0 | -97.4 | -97.2 | -97.6 |
| 465.000 | 3 | -96.0 | -97.1 | -97.9 | -97.3 | -97.6 |
| 470.000 | 3 | -96.4 | -97.2 | -97.5 | -97.4 | -97.7 |
| 475.000 | 3 | -96.6 | -97.2 | -97.6 | -97.4 | -97.7 |
| 480.000 | 1 | -96.3 | -97.3 | -97.6 | -97.5 | -97.0 |
| 485.000 | 1 | -96.9 | -97.4 | -97.7 | -97.4 | -97.8 |
| 490.000 | 1 | -97.1 | -97.1 | -96.7 | -97.3 | -97.9 |
| 495.000 | 3 | -97.5 | -99.7 | -97.2 | -97.6 | -98.0 |
| 500.000 | 3 | -97.5 | -97.6 | -97.4 | -97.7 | -97.4 |

Fig. 9 -- Example of an output from ITNPRINT (second of three pages)

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| | | | | | | |
|----------|---|-------|-------|-------|-------|-------|
| 209.000 | 3 | -96.7 | -97.6 | -97.5 | -97.6 | -97.6 |
| 910.000 | 3 | -97.0 | -97.7 | -97.5 | -97.6 | -97.6 |
| 919.000 | 1 | -97.2 | -97.9 | -97.3 | -97.6 | -97.6 |
| 920.000 | 3 | -97.4 | -97.9 | -97.5 | -97.6 | -97.6 |
| 929.000 | 3 | -97.2 | -98.0 | -97.7 | -98.0 | -97.2 |
| 930.000 | 3 | -97.6 | -97.6 | -97.9 | -98.1 | -97.5 |
| 939.000 | 3 | -96.8 | -97.4 | -96.9 | -98.2 | -97.7 |
| 940.000 | 1 | -96.6 | -97.4 | -96.9 | -98.2 | -97.7 |
| 949.000 | 3 | -96.8 | -97.4 | -96.9 | -98.2 | -97.7 |
| 950.000 | 1 | -96.6 | -97.4 | -96.9 | -98.2 | -97.7 |
| 959.000 | 3 | -97.1 | -97.8 | -97.9 | -98.3 | -97.9 |
| 959.000 | 3 | -97.2 | -97.8 | -98.0 | -98.3 | -97.9 |
| 960.000 | 3 | -97.3 | -97.9 | -98.1 | -97.6 | -99.0 |
| 969.000 | 3 | -96.4 | -97.8 | -97.3 | -98.2 | -99.1 |
| 978.000 | 1 | -96.7 | -97.1 | -96.4 | -98.1 | -99.3 |
| 979.000 | 1 | -94.9 | -97.2 | -96.5 | -97.5 | -99.3 |
| 988.000 | 3 | -96.4 | -97.2 | -96.5 | -97.6 | -99.3 |
| 989.000 | 3 | -96.5 | -97.1 | -96.7 | -97.6 | -99.4 |
| 990.000 | 3 | -96.5 | -97.1 | -96.6 | -98.2 | -97.2 |
| 999.000 | 4 | -96.4 | -97.1 | -96.5 | -98.1 | -96.1 |
| 600.000 | 1 | -96.6 | -98.4 | -98.4 | -98.5 | -97.6 |
| 608.000 | 3 | -96.6 | -98.4 | -98.4 | -98.5 | -97.6 |
| 609.000 | 3 | -97.0 | -98.4 | -98.5 | -98.3 | -97.5 |
| 610.000 | 1 | -97.2 | -98.5 | -98.6 | -98.4 | -97.9 |
| 615.000 | 1 | -97.5 | -98.4 | -98.3 | -98.9 | -98.1 |
| 628.000 | 3 | -97.9 | -98.5 | -98.5 | -99.3 | -98.2 |
| 629.000 | 3 | -97.7 | -98.4 | -98.5 | -97.9 | -98.2 |
| 630.000 | 3 | -97.8 | -98.5 | -98.6 | -99.1 | -98.3 |
| 639.000 | 3 | -97.9 | -98.5 | -98.7 | -97.5 | -98.4 |
| 648.000 | 3 | -98.1 | -98.4 | -98.7 | -98.0 | -98.5 |
| 649.000 | 3 | -98.0 | -98.4 | -98.8 | -98.2 | -98.5 |
| 650.000 | 1 | -98.3 | -98.7 | -98.8 | -98.3 | -98.6 |
| 659.000 | 3 | -98.4 | -98.8 | -98.8 | -98.4 | -98.6 |
| 668.000 | 3 | -98.4 | -98.7 | -98.8 | -98.4 | -98.6 |
| 669.000 | 3 | -98.5 | -98.6 | -98.8 | -98.4 | -98.6 |
| 670.000 | 3 | -98.6 | -98.7 | -98.5 | -98.5 | -98.7 |
| 679.000 | 3 | -98.7 | -98.3 | -98.5 | -98.5 | -98.7 |
| 680.000 | 1 | -98.8 | -98.2 | -98.4 | -98.6 | -98.7 |
| 689.000 | 1 | -98.7 | -98.2 | -98.4 | -98.6 | -98.7 |
| 698.000 | 1 | -97.6 | -98.2 | -98.4 | -99.6 | -99.7 |
| 699.000 | 1 | -98.2 | -98.1 | -98.2 | -98.6 | -99.8 |
| 708.000 | 3 | -98.6 | -98.1 | -98.2 | -98.5 | -99.9 |
| 709.000 | 3 | -98.6 | -98.1 | -98.2 | -98.5 | -99.9 |
| 710.000 | 1 | -98.7 | -98.1 | -98.2 | -98.6 | -99.9 |
| 719.000 | 3 | -98.7 | -98.1 | -98.2 | -98.6 | -99.9 |
| 728.000 | 3 | -98.8 | -98.2 | -98.3 | -98.6 | -99.7 |
| 729.000 | 3 | -99.0 | -98.2 | -98.3 | -98.6 | -97.9 |
| 730.000 | 3 | -99.1 | -98.2 | -98.2 | -93.9 | -99.0 |
| 739.000 | 3 | -99.2 | -98.2 | -98.2 | -96.1 | -99.0 |
| 748.000 | 3 | -99.3 | -98.2 | -98.2 | -99.5 | -96.0 |
| 745.000 | 3 | -98.3 | -98.4 | -98.4 | -98.6 | -97.1 |
| 750.000 | 3 | -98.3 | -98.4 | -98.4 | -97.5 | -97.1 |
| 759.000 | 3 | -98.6 | -98.1 | -98.5 | -97.5 | -97.4 |
| 760.000 | 3 | -98.7 | -98.4 | -98.4 | -97.2 | -97.6 |
| 765.000 | 3 | -98.7 | -98.4 | -98.4 | -98.6 | -97.6 |
| 770.000 | 1 | -98.7 | -98.5 | -98.3 | -98.7 | -97.6 |
| 779.000 | 3 | -98.9 | -98.4 | -98.3 | -98.6 | -97.8 |
| 780.000 | 3 | -99.4 | -98.6 | -98.4 | -98.3 | -97.8 |
| 785.000 | 3 | -98.5 | -98.7 | -98.6 | -95.4 | -97.9 |
| 790.000 | 3 | -98.7 | -98.7 | -98.6 | -98.9 | -98.0 |
| 799.000 | 3 | -98.7 | -98.7 | -98.3 | -94.9 | -98.0 |
| 800.000 | 3 | -98.4 | -98.7 | -98.3 | -95.9 | -98.0 |
| 800.000 | 3 | -98.4 | -98.7 | -98.3 | -98.9 | -98.0 |
| 805.000 | 3 | -97.3 | -98.7 | -98.2 | -98.8 | -97.9 |
| 810.000 | 1 | -98.4 | -98.4 | -98.1 | -98.7 | -97.9 |
| 819.000 | 3 | -98.4 | -98.7 | -98.0 | -98.7 | -97.9 |
| 820.000 | 1 | -98.4 | -98.7 | -98.6 | -98.6 | -97.9 |
| 825.000 | 1 | -98.5 | -98.7 | -98.6 | -98.6 | -97.9 |
| 830.000 | 3 | -98.6 | -98.4 | -97.3 | -98.9 | -97.6 |
| 839.000 | 3 | -98.7 | -98.7 | -97.9 | -98.6 | -97.8 |
| 840.000 | 3 | -98.8 | -98.7 | -97.8 | -98.6 | -97.9 |
| 845.000 | 3 | -98.8 | -98.5 | -99.0 | -98.5 | -98.1 |
| 850.000 | 1 | -98.9 | -98.8 | -99.0 | -99.5 | -98.1 |
| 859.000 | 1 | -98.9 | -98.8 | -99.0 | -23.5 | -98.1 |
| 860.000 | 1 | -98.9 | -98.5 | -99.0 | -98.3 | -98.3 |
| 865.000 | 3 | -98.4 | -98.4 | -99.0 | -98.2 | -98.5 |
| 870.000 | 1 | -98.4 | -98.4 | -98.0 | -98.1 | -98.7 |
| 879.000 | 1 | -98.0 | -98.4 | -98.9 | -98.1 | -98.7 |
| 880.000 | 1 | -98.1 | -98.4 | -98.9 | -94.7 | -98.7 |
| 885.000 | 3 | -98.4 | -98.4 | -98.9 | -98.0 | -98.6 |
| 890.000 | 3 | -98.3 | -98.4 | -98.8 | -97.7 | -98.6 |
| 895.000 | 1 | -98.4 | -98.5 | -98.8 | -97.4 | -98.6 |
| 900.000 | 1 | -97.6 | -98.7 | -98.8 | -97.2 | -98.7 |
| 900.000 | 1 | -97.6 | -98.7 | -98.8 | -97.2 | -98.7 |
| 905.000 | 3 | -97.0 | -98.4 | -98.8 | -97.1 | -98.7 |
| 910.000 | 1 | -97.7 | -98.4 | -98.8 | -94.8 | -98.6 |
| 919.000 | 1 | -98.1 | -98.4 | -98.8 | -98.4 | -98.6 |
| 920.000 | 3 | -98.2 | -98.4 | -98.8 | -94.3 | -98.5 |
| 929.000 | 3 | -98.3 | -98.5 | -98.7 | -94.2 | -98.2 |
| 930.000 | 1 | -98.3 | -98.5 | -98.8 | -94.2 | -98.6 |
| 935.000 | 1 | -98.2 | -98.5 | -98.8 | -98.2 | -98.7 |
| 940.000 | 1 | -98.4 | -98.5 | -98.8 | -98.2 | -98.7 |
| 945.000 | 1 | -98.5 | -98.5 | -98.8 | -98.5 | -98.1 |
| 950.000 | 1 | -98.9 | -98.8 | -99.0 | -99.5 | -98.1 |
| 959.000 | 1 | -98.4 | -98.4 | -99.0 | -23.5 | -98.1 |
| 960.000 | 4 | -98.6 | -98.5 | -98.8 | -98.3 | -98.6 |
| 965.000 | 1 | -97.9 | -98.1 | -98.5 | -98.9 | -98.6 |
| 970.000 | 1 | -97.9 | -98.1 | -98.5 | -98.9 | -98.6 |
| 979.000 | 1 | -97.9 | -98.1 | -98.4 | -98.9 | -98.6 |
| 980.000 | 1 | -98.1 | -98.2 | -98.4 | -98.9 | -98.7 |
| 985.000 | 1 | -98.1 | -98.2 | -98.3 | -94.8 | -98.7 |
| 990.000 | 1 | -98.4 | -98.4 | -98.6 | -97.7 | -98.6 |
| 995.000 | 1 | -98.4 | -98.5 | -98.6 | -97.4 | -98.6 |
| 1000.000 | 1 | -97.6 | -98.7 | -98.8 | -97.2 | -98.7 |
| 1000.000 | 3 | -98.3 | -98.1 | -98.4 | -98.9 | -98.7 |
| 1000.000 | 3 | -98.3 | -98.1 | -98.4 | -98.9 | -98.7 |

Fig. 9 — Example of an output from ITNPRINT (third of three pages)

Subroutine IVSRPLOT

Subroutine IVSRPLOT plots intensity versus range (Fig. 10). The first entry prints the heading, chooses the correct type of calculation, and then plots a line or the first range. Each succeeding call plots just a line for another range. Only one type may be plotted per data case.

Subroutine INTENSTY

Subroutine INTENSTY calculates all intensities. The switches ISCP, IT1, IT2, and IT3 determine what is calculated. When one selects coherent phase (ISCP = 1) one must also select random phase (IT1 = 1). Coherent phase intensity takes the phase of the ray into account in the calculations. If SL is a function of the random-phase sound level, then the coherent sound level is $(\sqrt{SL} \cdot \cos(P))^2 + (\sqrt{SL} \cdot \sin(P))^2$, where P is the phase angle. To get each, set IT2 = 1 for type II calculations and IT3 = 1 for type III calculations.

The only caustic correction which is applied to type I calculations is a ray-separation criterion: if two rays are closer together than 0.001 meter in depth, the eigenray for these two rays is thrown out. Type II and Type III intensity calculations do not have caustics.

Subroutine RECOVERY

Subroutine RECOVERY has two entry points: DUMP and RESTART. Its function is to enable one to restart a program. DUMP writes all the core locations on a tape when it is called, and RESTART restores core to its previous condition when it is called by reading the tape from DUMP.

Subroutine RETRY

Subroutine RETRY enables one to restart a program in which the multiple replacement option has been used (as was discussed for card II in the Input Description). Its chief function is to read any profile cards which have not yet been read and to write them on logical unit 6 for subroutine NEWPROF to read when required.

Subroutine CLOSEIOP

The function of subroutine CLOSEIOP is to alleviate a systems problem in punching intensity cards when using RESTART. Without this subroutine the cards would be punched in binary instead of BCD when RESTART is called. This subroutine might not be required in another computer system, if the proper modeing of logical units is accomplished automatically.

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THIS IS THE TITLE FOR THE PROBLEM
REFLECTIVE INTENSITY VS RANGE

REFLECTIVE AT EARTH PLOTS AS

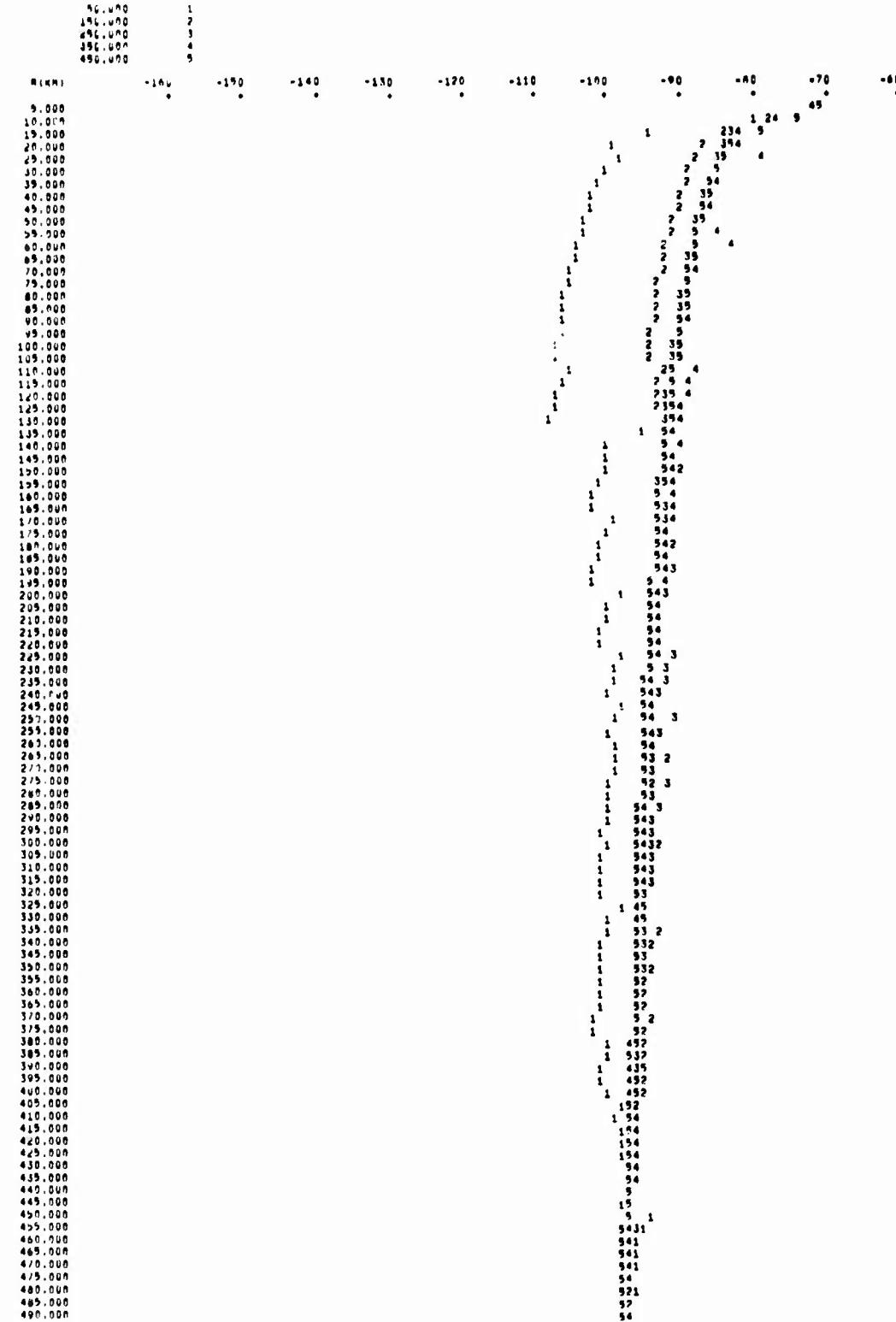


Fig. 10 -- Example of the output from IVSRPLOT

Subroutine BYEBYE

Subroutine BYEBYE is called in place of the Fortran statement STOP to terminate the program. It was written to avoid a CDC3800 systems problem when DUMP is called in the executive program. It might not be necessary to have this in another computer system, in which case the STOP statement could be reinserted, if desired.

DIFFERENT INTENSITIES IN TRIMAIN

In subroutine RAYZDIST (ray depth distribution) a quantity is printed titled LOSSES (Fig. 6). This quantity is equal to $10 \log_{10} (S)$, where S represents all the losses due to bottom interactions, surface interactions, and volume attenuation. Spreading loss is not included in these figures.

In subroutine INTENSTY a quantity is printed for the eigenray printout called SL (DB). If we let $SS(I)$ denote the quantity called S in RAYZDIST for the current ray and $SS(I-1)$ denote S for the previous ray, then we let $S1 = \text{secant (current ray angle)} [SS(I-1)]$ and let $DS = \text{secant (previous ray angle)} [SS(I)-S1]$. The ray depth at a given point may be identified as $ZZ(I)$. So if we are considering ray I , then $Z1 = ZZ(I-1)$ and $DZ = ZZ(I) - Z1$. If ZR is the receiver depth, then we let $F = (ZR - Z1)/DZ$. We let RMAX be the range to this point in meters. Then we define a quantity $SL = (S1 + F DS)/[\text{RMAX ABS}(DZ)]$. Thus the quantity printed for $SL(\text{DB})$ is $10 \log_{10} (SL)$.

The third parameter which is printed is the type I intensity and is derived in subroutine INTENSTY. This set consists of summing all the eigenrays, or the SL , for a given receiver and range point and then computing

$$10 \log \sum_{i=1}^N SL_i \text{ (incoherent or random phase sum),}$$

where N is the number of eigenrays determined for this point. If the Lloyd's mirror switch is not on, the final intensity value can be arrived at as stated, but if the Lloyd's mirror switch is on, each eigenray is multiplied by a factor before they are summed; thus it is not always possible to sum the eigenrays as printed to arrive at the final intensity.

The type II intensity calculation was initially proposed [2] using a Gaussian distribution, which smears a ray over a displaced bundle of intensity. DZBAR is a size parameter for that smearing and is defined by $DZBAR = SDZ/SW$, where we are using the mean absolute difference between ray depths, weighted by the signal strength of the ray, such that

$$SW = \sum_{i=2}^{\text{NRAY}} w_i = \sum_{i=2}^{\text{NRAY}} \min (SS_i, SS_i - 1),$$

which is the sum of the weights, and

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$$SDZ = \sum_{i=2}^{NRAY} Wi (ZZ_i - ZZ_{i-1})$$

which is the sum of the weighted mean differences.

If DZBAR is less than a wavelength, then DZBAR is set equal to a wavelength. $DZM = ZB/\sqrt{NRAY}$, where ZB is the bottom depth and $NRAY$ is the number of rays traced. If DZBAR is greater than DZM , then $DZBAR = DZM$. This is a check to see that DZBAR is not a large fraction of the bottom depth. If 100 rays were traced, then DZBAR would never be larger than 1/10 of the bottom depth.

If RMAX is the range of this point, then let $F = 2.0 * RMAX * DZBAR$. Let $ER = e^{-ZR/DZBAR}$, where ZR is the receiver depth, let $EB = e^{-ZB/DZBAR}$, and let $EZ = e^{-ZZ(I)/DZBAR}$. Now $SL = B * sec\theta * SS(I)/F$ where B is the volume attenuation. If a ray is close to the bottom, it does not get its full share of the intensity, since the intensity is distributed exponentially on either side of the ray. Thus, it is necessary to renormalize the distribution by saying $SL = SL/(1 - .5 * ((EB/EZ) + EZ))$.

We now want to calculate the quantity $A = e^{-ABS(ZZ(I)-ZR)/DZBAR}$, which expression is always less than 1.0. The final expression for each ray is then $S_i = SL * A$. The final intensity at a receiver is given by computing, in subroutine ITNPRINT,

$$10 \log \sum_{i=1}^N S_i .$$

In calculating the Type III intensity [2] it is assumed that a current velocity profile prevails to represent a local average over a convergence zone, which wipes out the phase of a ray. The ray turnover and turnunder depths are calculated for each ray, and then the ray cycle length is computed. Next the expression $SL = B * SS(I)/RMAX$ is computed to get cylindrical spreading. If a given receiver is between the turnunder and turnover depths, entry WDENS is called, which returns the parameter S , the signal strength parameter, which represents the probability density that the ray is at this depth. This probability density $T = 1/ABS(TAN\theta)$ is normalized in WDENS by dividing by the ray cycle length. The cylindrical spreading term is multiplied by signal-strength parameter S_i to get a contribution for each ray which is then summed as

$$10 \log \sum_{i=1}^N SL_i * S_i$$

to arrive at the final values.

EIGENRAY OUTPUT OPTION

The computer coding for the eigenray output option appears within the subroutine INTENSTY. If a request is made either for type I random intensity or type I coherent intensity, then it is possible to obtain an eigenray output (Fig. 11) by setting column 25 on the output control card (card group V in Fig. 1) equal to 1. The concept of an eigenray may be envisioned as an interpolated ray which will strike a receiver and is found by linearly interpolating between two rays which bracket a receiver. For certain cases eigenrays will be formed from rays which do not bracket a receiver. This is caused primarily by consecutive rays which have different histories; in this case there is some ray between the two existing rays which would give an eigenray if it were traced. Thus the program extrapolates a value. The program prefers two rays with the same history which bracket a receiver. This represents an IQUAL of 1. If it cannot achieve this, if the next ray history is different from the current ray history, if the previous ray history is the same as the current ray history, and if the receiver is within a distance of 1/2 the ray separation, a forward extrapolation is performed and IQUAL = 2. The same condition may happen on the first two rays of a set, and in this condition IQUAL = 3. If an interpolated ray is found later, the IQUAL = 3 ray will be thrown out, and the IQUAL = 1 ray used. This is indicated by ** after the IQUAL = 1, and the ray which is replaced is the last ray with a 3* at the same receiver depth. The number which is listed for NRAY is the current ray number, and this forms an eigenray in conjunction with the previous ray. The NBR column gives the number of bottom reflections for this ray. The NTU column is the number of turnunders for this ray. NSR gives the number of surface reflections and NTO gives the number of turnovers. RANGE is the distance in meters from the source to this receiver. DEPTH is the ray depth for a given receiver at this range. THETA is an interpolated value for the ray arrival angle at the receiver. TIME is the travel time in seconds to this receiver from the source and is also an interpolated value between the travel times for two rays bracketing a receiver. SL(DB) is discussed in the preceding section of this report.

| EIGENRAY SET | | | | TEST CASE FOR INTENSITY | | | | | | | |
|--------------|-----|-----|-----|-------------------------|---------|----------|----------|-----------|--------|-------|-----|
| NRAY | NBR | NTU | NSR | NTO | RANGE | DEPTH | THETA | TIME | SL(DB) | IQUAL | REM |
| 8 | 0 | 7 | 7 | 0 | 370000 | 350.0000 | -10.6075 | 248.56510 | -106.4 | 3 | * |
| 8 | 0 | 7 | 7 | 0 | 370000 | 700.0000 | -9.6028 | 248.60291 | -106.5 | 1 | |
| 17 | 0 | 11 | 0 | 10 | 370000 | 350.0000 | 5.4116 | 249.38608 | -99.5 | 2 | |
| 17 | 0 | 11 | 0 | 10 | 370000 | 700.0000 | 5.1751 | 249.36221 | -94.5 | 1 | |
| 28 | 0 | 7 | 7 | 0 | 370000 | 350.0000 | 9.4668 | 248.56477 | -107.9 | 1 | |
| 28 | 0 | 7 | 7 | 0 | 370000 | 700.0000 | 8.9163 | 248.52686 | -107.9 | 1 | |
| 17 | 0 | 22 | 0 | 21 | 740000 | 700.0000 | 6.7384 | 498.73885 | -103.7 | 2 | |
| 26 | 0 | 22 | 22 | 0 | 1110000 | 350.0000 | 4.3020 | 746.19729 | -113.1 | 1 | |
| 26 | 0 | 22 | 22 | 0 | 1110000 | 700.0000 | 4.4851 | 746.16336 | -113.1 | 1 | |

Fig. 11 — Example of an eigenray printout

THE LLOYD'S MIRROR OPTION FOR RECEIVERS

Some examples of the Lloyd's mirror beam pattern are presented in Fig. 12. The receiver depth is at the point where all the lines converge for each plot.

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FREQUENCY = 50 HERTZ RECEIVER DEPTH= 18.280 FREQUENCY = 50 HERTZ RECEIVER DEPTH= 91.440



FREQUENCY = 100 HERTZ RECEIVER DEPTH= 18.280 FREQUENCY = 100 HERTZ RECEIVER DEPTH= 91.440

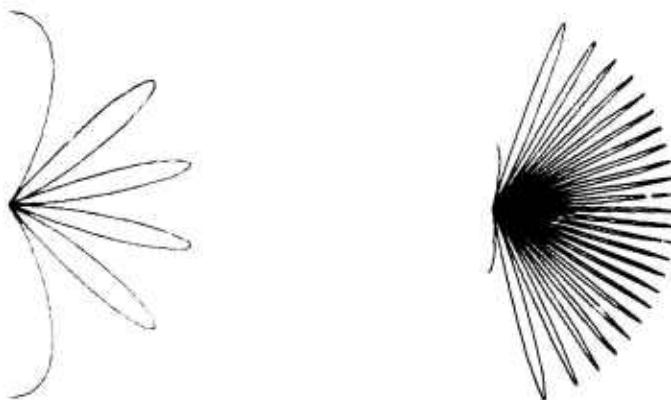


Fig. 12 — Examples of Lloyd's mirror beam patterns for receivers

The computer coding for the Lloyd's mirror option for receivers appears within the subroutine INTENSTY. The switch LLMR, in column 26 of the output control cards, is a receiver Lloyd's mirror switch. When the switch is off (0 or blank), the old intensity is returned, and when on (nonzero), the beam pattern

$$2 \sin^2 \left(\frac{2\pi z}{\lambda} \sin \theta \right) ,$$

where z is the depth, is used for type I random phase, type I coherent phase, Type II, and Type III intensity calculations for all receiver depths. For Type I and II calculations, θ is the ray angle, and for Type III calculations Snell's law is used to calculate the ray angle at the receiver. One can calculate some intensities with and some without the Lloyd's mirror by specifying them on different output control cards.

ADDITIONAL INSTRUCTIONS FOR THE RESTART OPTION

If the restart option is desired, a tape for output must be provided and a backup tape can be provided. Logical unit 15 is the primary output tape. Logical unit 16 is the backup output tape. Logical unit 17 may be used as a second backup tape, but this is optional. If the tape on logical unit 15 was bad when the program attempted the dump and it had to write on logical unit 16 or 17, then that tape would become logical unit 15 for restart. Logical units 16 and 17 may be omitted if you are sure you have a good tape on logical unit 15. The control deck should then have these cards:

79 EQUIP, 15 = MT, LO, **, DA

79 EQUIP, 16 = MT, LO, **, DA (optional)

79 EQUIP, 17 = MT, LO, **, DA (optional)

For dumping on tape the job request form should be as follows:

| <u>Logical Unit No.</u> | <u>Input</u> | <u>Output</u> | <u>Save</u> | <u>Tape No.</u> (if not specified, the Computation Center sells you one and assigns a number) |
|----------------------------|-------------------------------------|-------------------------------------|-------------------------------------|---|
| 15 | <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | Number for tape |
| 16 (Optional) | <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | Number for tape |
| 17 (Optional) | <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | Number for tape |
| 20 (Program tape) | <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | 573 |
| 1 (Used only for ray tape) | <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | Number for tape |

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In addition the second card in each case should contain the word DUMP in columns 73 through 76 if a restart capability is desired. If the program runs out of time, one may restart it according to the following procedure.

1. Change the job request form for logical units 15 and 1 as follows:

| Logical Unit No. | Input | Output | Save | Tape No. |
|------------------|-------------------------------------|-------------------------------------|-------------------------------------|-----------------|
| 15 | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | Number for tape |
| 1 | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | Number for tape |

However, the output block for logical unit 15 is checked only if a dump is desired again if the program runs out of time, and the input block for logical unit 1 is checked only if the ray tape is being restarted.

2. The first card after your run card must contain RESTART in columns 1 through 7. If a dump is desired again if the program aborts because of lack of time, DUMP is entered in columns 9 through 12 of the same card. One looks through the listing and determines what cards were read last, pulls out all these cards and places the remaining cards behind the card containing the word RESTART. If the multiple replacement option is being used, the profile remaining to be read should be read in from the case in which $LA = 1$. For the next case all cards would have to be read in again. Also the run must have progressed at least one range increment before dump can be called. Thus, if these conditions are not met, the entire deck must be resubmitted. Also, if the last data card read was an end-of-file card, then the first data card read must be the restart card and then the end-of-file card is read. If multiple replacement is being used, one should have the restart card and then a blank card followed by a card with the word START in columns 1 through 5, followed by remaining data. This can be determined by looking at the comment which is printed at the end of the program. Reference 7 is a more complete writeup on the restart option.

CAUTIONS TO THE USER

The following are some cautions to the user:

- If you have six receivers, then you must insert a blank card after the output control card containing the six receivers.
- The number of input and internally generated points in a sound-speed profile cannot exceed 50. The number of internally generated points can be reduced by reading in profiles with common depths.
- Do not read in the second speed-profile at a range less than the second bottom point; otherwise a diagnostic is printed and program aborts. Thus the range to your second bottom point should equal or be less than the range to the second profile.

- The source depth and sound-speed depth for any profile should not be the same; otherwise a diagnostic is printed and the program aborts. To correct this fault, change the source depth by 0.01 meter.
- The first bottom point must be at range zero.
- The maximum number of rays which may be traced is 1000.
- If the program runs for a long time and produces no results, you have specified too large a distance between bottom points or output values and the program is forced to set up long thin triangles. In this case there is difficulty in arriving at the proper ray intersections with the triangles. To correct this condition, insert either additional bottom points or additional output at shorter range increments.

PROGRAM TRIPLT

Program TRIPLT performs a Calcomp plot of the ray trajectories (Fig. 13). It reads an output tape from the main program and plots selected rays to a given range. Cubic splines are employed to give the proper trajectories. A maximum of 512 rays and a maximum of 2000 range increments may be plotted. A portion of the range may be plotted by specifying the number of records (one record being one range increment). A description of the input follows.

The input ray tape should be read in on logical unit 1. Thus the first equip card should be

79 EQUIP, 1 = *MT*, density, *RO*, label.

Logical unit 2 should be equipped for the disk file as 79 EQUIP, 2 = *DF*.

Logical unit 10, the plot unit, may be equipped as 79 EQUIP, 10 = *PL* or 79 EQUIP, 10 = *MT*, *LO*, label, *DA* (to write an output tape to be plotted later).

The job request form should be checked as follows:

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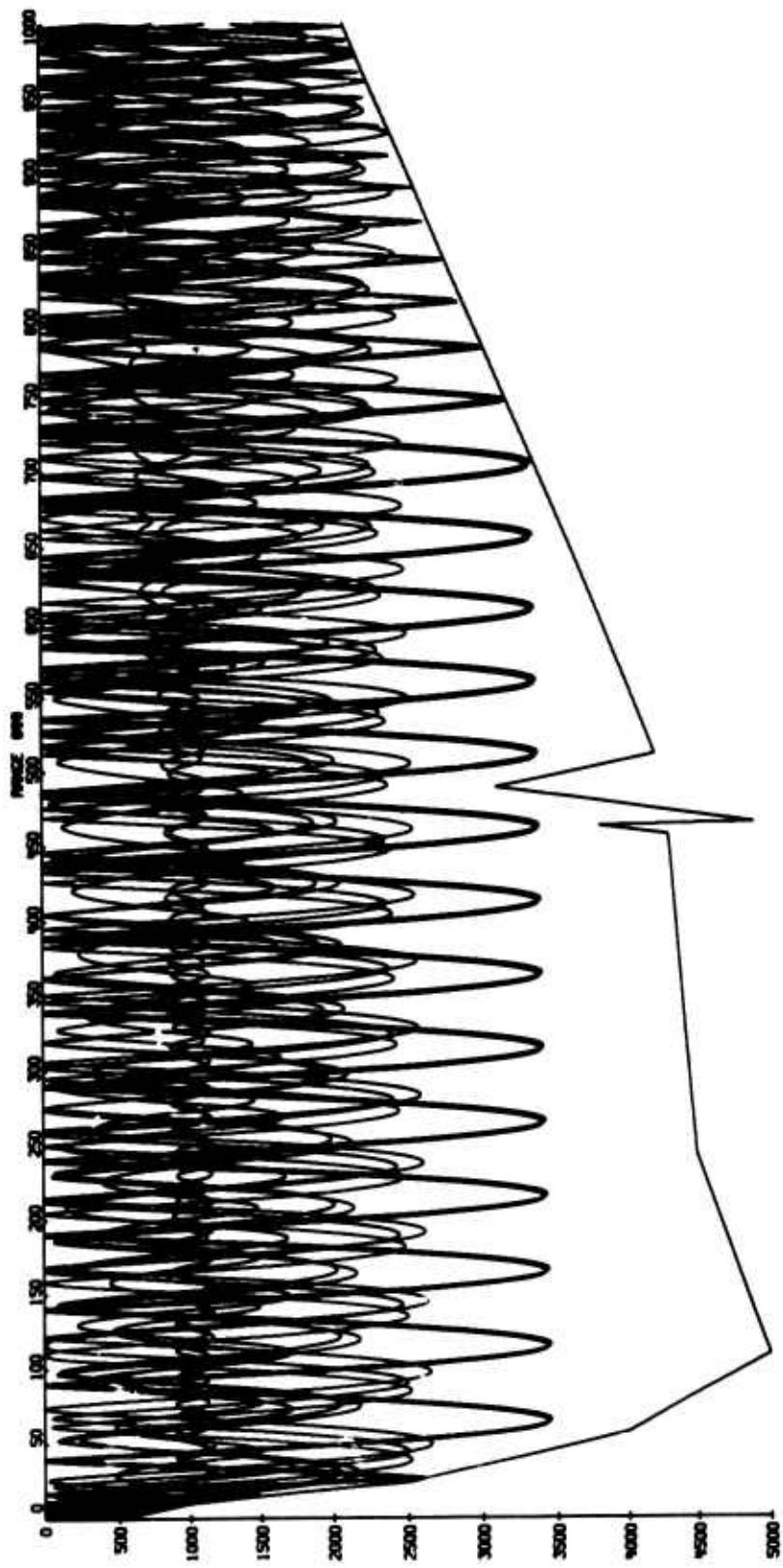


Fig. 13 — Example of a Calcomp plot

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| <u>Logical Unit No.</u> | <u>Input</u> | <u>Output</u> | <u>Save</u> | <u>Tape Serial No.</u> |
|-------------------------|-------------------------------------|-------------------------------------|-------------------------------------|------------------------|
| 1 | <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | Input Tape No. |
| 2 | <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <i>DF</i> |
| 10 | <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | Output Tape No. |

Logical unit 10 need be specified only if writing an output tape; if the plot is to be done on line, the 79 EQUIP, 10 = *PL* may be used or the card may be omitted. Computer 1 should be specified on the job request form also, because it contains the plotter package. The data deck input is as follows:

| <u>First-card Columns</u> | <u>Variable</u> | <u>Meaning</u> |
|----------------------------|-----------------|--|
| 1-2 | ITNC | Total number of cases. |
| <u>Second-card Columns</u> | <u>Variable</u> | <u>Meaning</u> |
| 1-8 | AL | Plot length in inches, which must be <120.0. |
| 9-16 | ZMAX | Maximum depth of plot, in either feet or meters. |
| 17-20 | NRMAX | Number of records to be plotted. There is one record for each range increment on the tape. Plots for a portion of the range from range ZERO may be made by specifying the number of records to that point. To plot the entire range a number may be specified which is larger than the actual number but less than 2001. |
| 21-25 | IKNM | If IKNM < 0, the range scale will be plotted in nautical miles; if IKNM > 0, the range scale will be in kilometers. |
| 26-30 | IFMC | If IFMC < 0, the depth scale will be plotted in feet; if IFMC > 0, the depth scale will be plotted in meters. |

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| <u>Second-card
Columns</u> | <u>Variable</u> | <u>Meaning</u> |
|--------------------------------|-----------------|---|
| 31-35 | NFSK | Number of files to skip on the tape before plotting this case. |
| 36-40 | ITTR | If ITTR < 0, a title card is read to replace the title on the tape; if ITTR > 0, the title from TRIMAIN will be used for the title. |
| 41-45 | NSR1 | Maximum number of surface hits allowable. The ray will be terminated at this surface hit. If this is left blank, the previous limits from TRIMAIN will be used. |
| 46-50 | NBR1 | Maximum number of bottom hits allowable, analogous to NSR1. |
| 51-60 | ALIM1 | Maximum dB loss allowed per ray, similar to NSR1 and NBR1. It is read in as a positive floating-point number, such as 200.0. |

| <u>Third-card
Columns
(If ITTR < 0)</u> | <u>Variable</u> | <u>Meaning</u> |
|--|-----------------|---|
| 1-80 | TITLE | Title of the plot. This card is omitted if ITTR > 0 in columns 36 through 40 of the second card; if this card is omitted, the fourth card becomes the third card. |

| <u>Fourth-card
Columns
(or Third-card
Columns if
ITTR > 0)</u> | <u>Variable</u> | <u>Meaning</u> |
|---|-----------------|---|
| 1-4 | NRPLOT(1) | Number of the first ray to be plotted, which corresponds to the number of the ray in the program TRIMAIN. |
| 5-8
... | NRPLOT(2) | Number of the second ray to be plotted. |

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| Fourth-card
Columns
(or Third-card
Columns if
ITTR > 0) | Variable | Meaning |
|---|------------|---|
| 76-80 | NRPLOT(20) | Number of the 20th ray to be plotted. |
| ... | ... | |
| Additional-card
Columns | Variable | Meaning |
| 1-80 | NRPLOT(N) | Numbers of the rays to be plotted, continued 20 per card until the desired number N is reached. |

An end of file card terminates each case. The cards beginning with the second card are repeated ITNC times for multiple cases.

REFERENCES

1. E.B. Wright, "Acoustic Transmission Loss by Single-Profile Raytracing (Program RTRACE)", NRL Report (7815), 1974.
2. "The Hudson Laboratories Ray Tracing Program," Technical Report 150, Hudson Laboratories of Columbia University, Dobbs Ferry, New York.
3. J.J. Cornyn, Grass: "A Digital-Computer Ray-tracing and Transmission-Loss Prediction System," Volume 1-Overall Description," NRL Report 7621, Dec. 1973.
4. H. Weinberg, "A Continuous-Gradient Curve Fitting Technique for Acoustic-Ray Analysis," J. Acoust. Soc. Am. 50, 971 (1971).
5. B.G. Roberts, Jr., "Retrieval Program for Archival Nansen-Cast Data," NRL Report 7633, 1973.
6. E.L. Wright, "Ray-tracing with Horizontal and vertical Gradients," J. Acoust. Soc. Am. 48, 92(A) (1970).
7. D.P. Shannon, and A.B. Mays, "A 3800 Subroutine to Allow a Restart Capability for Computer Programs," NRL Research Computation Center Computer Note 46, 1970.

Appendix A

LISTING OF THE PROGRAM

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PROGRAM TRIMAIN
DIMENSION JUNK(10), R1(10),DR(10),R2(10),STRCD(26,10),JNRC(10),INTTRIM
1   (10),IT(6,10),IRT(10),IRD(10),ISCP(6),Z(2,50),V(2,50),T(9) TRIM 1
1 EQUIVALENCE (ISCP,ISCPFQ) TRIM 2
COMMON /MIRRORS/ FSRL,BRLT(200),BPST(200) TRIM 3
COMMON /INFO/ RSTART,RMAX,OMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG, TRIM 4
1 ISCP,IT1,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT TRIM 5
COMMON /PREFIL/ RONE,N1,Z1(50),V1(50),RTL0,N2,Z2(50),V2(50),IBOTC,TRIM 6
1!PFL TRIM 7
COMMON /LEDDRESS/ LNRC,RCD(100),DINT(400) TRIM 8
COMMON /PRG/ IPRAP,IKNM,PLTL,RM,IPC0,IFPR TRIM 9
DATA (LTRT=1),(LTER=41),(LTPR=42),(LPIN=60) TRIM 10
COMMON /PATTERN/ SD,ITRP,DATA,SORLEV TRIM 11
COMMON /PIDEF/ PI,DTR,TWOP1 TRIM 12
COMMON /LIMITS/R1,DR,P2 TRIM 13
COMMON /TITLE/ ITITLE(10) TRIM 14
COMMON /ABC/PU\CHDB (16),INCR,NARS,NSRS,ALIM,IFT,IFT1 TRIM 15
COMMON /IFC/ IFE,IA,IB,IP,ID,IS,LA TRIM 16
COMMON /RANST/ RTWCH,IREC,IFSK,SDS TRIM 17
PI=4.*ATAN(1.) SIFT=0 SIFT1=0 S IPC0=0 STWOP1=PI+PI*SDTR=180./PI TRIM 18
1 READ 900,ITITLE IOPY=ITITLE(1) S WRITE (19) ITITLE TRIM 19
REWIND 19 TRIM 20
IF (EOF, 60) 155, 2 TRIM 21
2 IF (IOPT.EQ.8HRESTART )GO TO 104 S GO TO 122 TRIM 22
900 FORMAT(10A8) TRIM 23
155 IF (IFE.EQ.1) GO TO 152 S IFE=1 S GO TO 1 TRIM 24
122 PRINT 901,ITITLE S RSTART=0,0 SRMAX=0.0 S NPLT=0 TRIM 25
901 FORMAT(*1HORIZONTAL GRADIENT RAY TRACE *,10A8) TRIM 26
READ 902,SD,FKHZ,IATT,SORLEV,ITRP,DATA,SLDR,IABOT,ISCP,NRECUR,
1 IBOTC,IPFL,IPRAP,IKNM,PLTL,NBRS,NSRS,ALIM,IA,IR,IP,ID,IS,LA,IOPTRIM 27
AL1=ALIM S SDS=SD
FSPL=0.**(-.1*SLDB) SIF(ALIM,NE,0,0)ALIM=PBWRF(1,0,0,(-ALIM/0,0))TRIM 28
902 FORMAT(F8.3,F5.3,11,F5.2,11,2F5.2,7I1,F8.3,2I5,F10.3,6I1,1X,A8) TRIM 29
OMEGA =2000.,PI*FKHZ SIF (ALIM,EQ,0,0)ALIM=1.0E-30 S S2=FKHZ**2 TRIM 30
PRINT 903,SD,SORLEV,FKHZ,ITRP,DATA,NBRS,NSRS,AL1,IA,IB,IP,ID,IS,LATRIM 31
1,IOPTRIM 32
903 FORMAT(*0$OURCE DEPTH*,F8.2,* LEVEL*,F6.1,* FREQ(KHZ)*,F6.3,* BEATRIM 33
1MPATTERN *,12,3X,*ANGLE*,F5.1,5X,*NARS*=,15,5X,*NSRS*=,15,5X,*DB*TRIM 34
2LIMIT*,F10.3,/,5X,*IA*=,I1,5X,*IB*=,I1,5X,*IP*=,I1,5X,*ID*=,I1,5X,*IS*=,I1,5X,*LA*=,I1,5X,*IOPTR*=,A8) TRIM 35
35X,*IS*=,I1,5X,*LA*=,I1,5X,*IOPTR*=,A8) TRIM 36
IF (NRECUR.GT.0.AND.IBOTC.GT.0)SD=SD*(1.+.5*SD/6371221.3) TRIM 37
ATT=0.0003025*S2 +44.*S2/(4100.+S2) TRIM 38
IF(IATT.EQ.0) ATT=0 S IF (NBRS.EQ.0) NBRS=2500 S IVSR=0 TRIM 39
PRINT 904,ATT,SLDB S IF (NSRS.EQ.0) NSRS=2500 TRIM 40
904 FORMAT(*0$OLUME ATTENUATION*,F10.6,* DB/KM,* SURFACE LOSS*,F7.2,1 * DB,*) TRIM 41
1 CALL INITRAYS S DR 985 J=1,10 SR1(J)=0.0 SDR(J)=0,0 TRIM 42
985 R2(J)=0.0 SIF(IABOT,NE,0) GO TO 15 S RR=ISCP TRIM 43
CALL BRLTRD(RB) SIF (LA,EQ,1,0,IR,EQ,1,IR,EQ,3) REWIND 9 TRIM 44
IF (LA,EQ,1,0R,IR,GE,2) REWIND 8 S GO TO 1A TRIM 45
15 PRINT 905 TRIM 46
RR=1.E30 TRIM 47
905 FORMAT(*0$OTTOM ABSORBS ALL INCIDENT SOUND ENERGY*) TRIM 48
18 N=1 SIF (IP,EQ,0,AND,LA,EQ,0,0R,LA,EQ,1) LPC=60 SIF(IP,EQ,1)LPC=4 TRIM 49
20 IF(LPC,EQ,60)READ(LPC,906)R1(N),DR(N),R2(N),IC,(IT(I,N),I=1,6),JVSTRIM 50
IR,IRD(N),IPR,IRT(N),IPRAY,(STRCD(I,N),I=1,6) TRIM 51

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1R,IRD(N),IRP, INT(N),IPRAY,(STRCD(1,N),I=1,6),JVSTRIM 57
!F(LA,EQ.1)WRITE( 4) R1(N),DR(N),R2(N),IC,(IT(1,N),I=1,6),JVSRTTRIM 58
1,IRD(N),IRP, INT(N),IPRAY,(STRCD(1,N),I=1,6) TRIM 59
906 FORMAT(3F6.2,12,11!1,1X,6FB,4) TRIM 60
INT(N)=0 TRIM 61
D0 22 I=1,5 TRIM 62
22 INT(N)=INT(N)+IABS(IT(I,N)) TRIM 63
IF (IT(5,N),GT,0) IPER=IT(5,N) TRIM 64
IF(INT(N),EQ,0) GO TO 30 TRIM 65
PRINT 907,R1(N),DR(N),R2(N),(IT(1,N),I=1,6) TRIM 66
IF(DR(N).LT,0.) DR(N)=-1.+DR(N)/R1(N) TRIM 67
IH=6 TRIM 68
23 IF(STRCD(1H,N).GT,0.,) GO TO 25 TRIM 69
24 IH=IH+1 TRIM 70
IF(STRCD(1H,N).GT,0.,) GO TO 26 TRIM 71
IF(1H,LE,1) 26,24 TRIM 72
25 IL=IH+1 TRIM 73
IH=IH+10 TRIM 74
IF(LPC,EQ,60) READ (LPC,908,(STRCD(1,N),I=IL,IH) TRIM 75
IF(LPC,EQ, 4) READ (LPC) (STRCD(1,N),I=IL,IH) TRIM 76
IF(LA,EQ,1) WRITE ( 4) (STRCD(1,N),I=IL,IH) TRIM 77
C THE SWITCH ITIM IS NOW LLMR, THE LLOYDS MIRROR SWITCH FOR ALL TRIM 78
C RECEIVERS ON A GIVEN RANGE PLOT CARD TRIM 79
907 FORMAT(*OUTPUT RANGES*,3F6.2,5H ISCP,12.4H IT1,12,4H IT2,12,4H *)TRIM 80
13,12.5H IPER,12,5H LLMR,12) TRIM 81
908 FORMAT(10F6.2) TRIM 82
GO TO 23 TRIM 83
26 JNRC(N)=IH TRIM 84
PRINT 909,(STRCD(1,N),I=1,IH) TRIM 85
IF (NRECUR.LE,0) GO TO 29 TRIM 86
D0 31 I=1,IH TRIM 87
31 STRCD (1,I)=STRCD(I,N)*(1.+5*STRCD(1,N)/6371221.3) TRIM 88
909 FORMAT(*GRCD*,10F9.2) TRIM 89
29 IF(JVSR,EQ,0) GO TO 27 TRIM 90
PRINT 910,JVSR TRIM 91
910 FORMAT(*0)INTENSITY VERSUS RANGE PLOT WILL BE MADE FOR TYPE*,13) TRIM 92
IF(IVSN,NE,0) PRINT 911 TRIM 93
911 FORMAT(5H ***,*CAUTION*** ONLY THE LAST I VS R PLOT WILL BE MADE*)TRIM 94
JVSR=JVSR TRIM 95
NVSR=N TRIM 96
27 IF(IRP,EQ,0) GO TO 28 TRIM 97
NTPLT=15 TRIM 98
ZMAX=0. TRIM 99
DRPLT=1. TRIM 100
RLPLT=1.E6 TRIM 101
PRINT 915 TRIM 102
28 IF(IRD(N),NE,0) PRINT 912 TRIM 103
IF(IRT(N),NE,0) PRINT 913 TRIM 104
615 FORMAT (*ORAY PLOT WILL BE MADE*) TRIM 105
912 FORMAT(*ORAY DEPTH DISTRIBUTION WILL BE MADE*) TRIM 106
913 FORMAT(*ORAY TAPE WILL BE MADE*) TRIM 107
GO TO 40 TRIM 108
30 IF(IRP,EQ,0) GO TO 33 TRIM 109
NTPLT=STRCD(1,N)+1 TRIM 110
IF(NTPLT.LT,1) NTPLT=15 TRIM 111

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ZMAX=STRCD(2,N)
DRPLT=DR(N)
RLST=R2(N)
RLPLT=RLST
PRINT 915
PRINT 914,R1(N),DR(N),R2(N)
33 IF(IRD(N).GT.IRT(N),EQ,0) GO TO 35
PRINT 914,R1(N),DR(N),R2(N)
914 FORMAT(*0OUTPUT RANGES*,3F10.4)
IF(IRD(N),NE,0) PRINT 912
IF(IRT(N),NE,0) PRINT 913
GO TO 40
35 N=N+1
40 IF(IC,EQ,0) GO TO 45
N=N+1
IF (N,GT,10)41,20
41 PRINT 42
42 FORMAT (1HO,*NUMBER OF OUTPUT CONTROL CARDS EXCEEDS 10, PROGRAM
1 ABORTED*)
CALL BYEBYE
43 NR=N   S IF (LA,EQ,1.0P,IP,EQ,1) REWIND 4
JRT=0
RMAX1=0.
D=1.0   S D1=DRPLT   S DELTM=0.0   S ICA=0   S DELTA=0.0
D= 47 I=1,NR
IF (DR(I),LT,D) D=DR(I)   S IF (DR(I),LT,D1) D1=DR(I)
IF(R2(I).GT,RLST) RLST=R2(I)
IF(IT(2,I),EQ,0) GO TO 47
IF(R2(I).GT,RMAX1) RMAX1=R2(I)
47 JRT=JRT+IRT(I)
D=D/2.0
CALL INIT
CALL NEWPROF(ZM)
CALL NEWPROF
CALL CONNECT
IF(ZMAX,EQ,0.) ZMAX=ZM
RPLT=1.E6
IF(NTPLT,EQ,0) GO TO 49
RPLT=DRPLT
CALL RAYPLBT(NTPLT,ZMAX)
49 IF(JRT,EQ,0) GO TO 51
CALL RAYTAPE
51 NOLD=-10
J=0
NINT=1
C     IF ALL THE INTENSITY CALCULATIONS HAVE THE SAME RCDS
C     A TABULAR FORMAT WILL BE USED
D= 55 I=1,NR
IF(INT(I),EQ,0) GO TO 55
IF(J,EQ,0) J=1
IF(J,EQ,1) GO TO 55
IF(JNRC(I),NE,JNRC(J)) GO TO 54
K=JNRC(I)
D= 53 L=1,K
IF(ABS(STRCD(L,I)-STRCD(L,J)),GT,,1) GO TO 54
53 CONTINUE

```

TRIM 113
TRIM 114
TRIM 115
TRIM 116
TRIM 117
TRIM 118
TRIM 119
TRIM 120
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TRIM 122
TRIM 123
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TRIM 164
TRIM 165
TRIM 166
TRIM 167
TRIM 168

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      GO TO 55
54   NINT=2
      GO TO 95
55   CONTINUE
99   RMAX=0,
100  RN=1.E6
      DE 103 I=1,NR
      IF(R1(I).LT.RN) RN=R1(I)
103  CONTINUE
      RSTART=RMAX
      RMAX=AMIN1(,001*RTW0,RPLT,RN)*1000.
      RT=.001*(RMAX+1.)
      IF(RT.GT.RLST*D)    GO TO 140
      IF (IOP1.EQ.8H DUMP ) GO TO 104
      TILT=TLT
      TLTP=TILT
      TILT=TIMELEFT(1)
      DELT=TLTP-TILT
      IF (DELT.LT.0.0) GO TO 108
      ICA=ICA+1
      FICA=ICA
      DELTA=DELTA+DELT
      DELTM=DELTA/FICA
108  RER=(RLST-(RSTART/1000.0))/D1
      TOTIME=RER+DELM=2.0
      TOTIMM=TOTIME/60.0
      IF (TLT.LE.90.0+DELM AND .TOTIME.GE.30.0+DELM) 107,104
107  IF (JRT.NE.0) BACKSPACE 1  S CALL DUMP
      PRINT 105,TLT,TOTIMM
105  FORMAT(1H0,♦PROGRAM ABRTED, INSUFFICIENT RUN TIME, TIME REMAINING♦)
      1G=.,F10.3,♦ SECONDS.,5X,♦ESTIMATED TIME TO FINISH RUN♦,F10.3,
      2♦ MINUTES♦)
      PRINT 101,RTW0M
101  FORMAT (1H0,♦REMOVE DATA DECK THROUH PROFILE AT RANGE♦,F10.3,♦ KMTR)
      1 BEFORE RESTARTING CASE♦,/)
      IF (IFE.EQ.1) PRINT 106
      IF (IS.EQ.1,AND.IFE,FQ.0) PRINT 132
112  FORMAT (1H0,♦INSERT BLANK CARD AFTER RESTART CARD, FOLLOWED BY A CTRIM 205
      1ARD WITH WORD START IN COLUMNS 1-8, FOLLOWED BY REMAINING DATA♦,/)
      106  FORMAT (1H0,♦INSERT END OF FILE CARD AFTER RESTART CARD BEFORE RESTRIIM 207
      1ARTING CASE♦,/)
      IF (IFE.EQ.1) GO TO 111
109  READ 900,JUNK
      IF (EOF,60)111,109
111  CALL BYEBYE
104  IF (IOP1.NE.8HRESTART ) GO TO 102
      IF (IOP1.EQ.8HRESTART ) CALL RESTART  S CALL CLOSE(0P
      PRINT 901,ITITLE      S DO 113 J=1,10
113  JUNK(J)=ITITLE(J)  S READ (19) ITITLE
      REWIND 19
      IF (ITITLE(1).EQ.8HRESTART ,AND.IS.EQ.1,AND.IFE.EQ.0) CALL RETRY
      IOP1=ITITLE(2)
      IF (IOP1.EQ.8H      ) IOP1=IOP1      S DO 114 J=1,10
114  ITITLE(J)=JUNK(J)  S IF (JRT,EQ.0) GO TO 102  S DO 121 J=1,IFSK
121  CALL SKIPFILE (1)  S DO 123 J=1,IREC
123  READ (1)
102  CALL ADVANCE S IF(RMAX>1.LT,RTW0) GO TO 110      S CALL NEWPROF

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CALL CONNECT
110 IF(RT,LT,RPLT) GO TO 115      S CALL RAYPLOT
RPLT=RPLT+DRPLT
115 IF(RPLT.GT.RLPLT+.1) RPLT=1,E6
IF(RT,LT,RN) GO TO 135
D8 130 I=1,NR
IF(R1(I),GT,RT) GO TO 130
IF(INT(I),EQ,0) GO TO 128
IF(I,EO,NOLD) GO TO 120
LNRC=JNRC(I)
D8 117 J=1,LNRC
117 RCD(J)=STRCD(J,I)
D8 119 J=1,6
119 ISCPEQ(J)@IT(J,I)
120 CALL INTENSTY
CALL ITNPINT(NINT)
IF(I,EO,NVSR) CALL IVSRPLOT(IVSR)
NOLD=1
125 IF(IRD(I),NE,0) CALL RAYZDIST (NTPLT)
IF(IRT(I),NE,0) CALL RAYTAPE
IF(DR(I).LT,0.) GO TO 126
R1(I)*R1(I)+DR(I)
GO TO 127
126 R1(I)=R1(I)+DR(I)
127 IF(R1(I).GT.R2(I)+.001) R1(I)=1.56
130 CONTINUE
135 IF(RT,GT,RB) CALL NWBRLT(RB)
GO TO 100
140 IF(JRT,EO,0) GO TO 150
ENDFILE LTRT
ENDFILE LTRT
BACKSPACE LTRT
150 IF (INCR,GT,1,AND,INCR.LE.16) 151,153
151 INCR@INCR=1
WRITE (36,919) (PLANCHOR(I)),I=1,INCR
919 FORMAT (16F5.1)
153 IF (IFE,EO,1) GO TO 158
IF (LA,EO,1,@R,IS,EO,1) GO TO 160
157 READ 900,JUNK
IF (EOF,60) 158,157
160 IF (LA,EO,1,@R,IS,EO,0;AND,LA,EO,0) LPM=60
IF (IS,EO,1) LPM=6
176 IF(LPM,EO,60)READ (LPM,1903) NCUR,RB,TI
IF(LPM,EO, 6)READ (LPM)      NCUR,RB,TI
IF(EOF,LPM) 177,178
177 IF (LA,EO,1) ENDFILE 6
REWIND 6
GO TO 158
178 IL=1  S IF (LA,EO,1) WRITE (6)      NCUR,RB,TI
179 IH=IL+4
IF(LPM,EO,60)READ(LPM,1900)(Z(2,I),V(2,I),I=IL,IH)
IF(LPM,EO, 6)READ(LPM)      (Z(2,I),V(2,I),I=IL,IH)
IF(LA,EO,1)WRITE ( 6)      (Z (2,I),V (2,I),I=IL,IH)
IF(V (2,IH).LE,0.) GO TO 176
IL=IL+5
GO TO 179

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| | |
|---|----------|
| 1603 FORMAT(I1,F7.3,9A8) | TRIM 281 |
| 1600 FORMAT(10F0.4) | TRIM 282 |
| 1598 IFPR1=IFPR S IF ((IFPR.NE.1) IPPR=1 S IF ((IPFL.EQ.0) GO TO 159
IF ((IPPR1.EQ.0.AND.IPFL.EQ.1) CALL PROFPL07 (2.0,5,1)
IF ((IPFL.EQ.2.AND.IFPR1.EQ.0) CALL PROFPL07 (2.0,5,1)) | TRIM 283 |
| 1599 IFE=1 S IFT1 =IFT1+1 S IF ((IS.EQ.0) GO TO 1 | TRIM 284 |
| 1601 READ 900,JUNK S IF (EMF,60) 1,161 | TRIM 285 |
| 1602 IF ((IPC0.NE.0) CALL STOPPLAT | TRIM 286 |
| CALL BYEBYE | TRIM 287 |
| END | TRIM 288 |
| | TRIM 289 |
| | TRIM 290 |

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5.4DS TRIMAIN

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| | IDENT | TRIMAIN |
|------------------|---------|---------|
| PROGRAM LENGTH | 04624 | |
| ENTRY POINTS | TRIMAIN | 01572 |
| BLOCK NAMES | | |
| MIRRORS | 00621 | |
| INFO | 00024 | |
| PROFIL | 00316 | |
| LOUDNESS | 00765 | |
| PRO | 00006 | |
| PATTERN | 00004 | |
| PIDEF | 00003 | |
| LIMITS | 00036 | |
| TLE | 00012 | |
| ABC | 00026 | |
| IFC | 00007 | |
| RANST | 00004 | |
| EXTERNAL SYMBOLS | | |
| 000ENTRY | | |
| THEND, | | |
| 02007111 | | |
| 01010100 | | |
| 000DICT, | | |
| INITRAYS | | |
| BRLTRD | | |
| AYEBYE | | |
| INIT | | |
| NEWPROM | | |
| CONNECT | | |
| RAYPLOT | | |
| RAYTAPE | | |
| TIMELEFT | | |
| DUMP | | |
| RESTART | | |
| CLOSEIOP | | |
| RETRY | | |
| SKIPFILE | | |
| ADVANCE | | |
| INTENSTY | | |
| ITNPRINT | | |
| IVSRPLOT | | |
| RAYZDIST | | |
| NWRBLT | | |
| PROFPLDT | | |
| PREFPLIT | | |
| STOPPLOT | | |
| POWRF | | |
| MIN1F | | |
| ATANF | | |
| C001FE0F | | |
| EFT, | | |
| BSP, | | |
| REW, | | |
| TSH, | | |
| TSB, | | |
| STH, | | |
| STB, | | |
| SLG, | | |
| SLI, | | |
| ONSINGL, | | |

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| CLOSEIOP | | | | 07/12/73 | ED 00000 | PAGE NO. | 1 |
|-----------------------|-------------|----------|-----------|----------|----------|----------|----|
| PROGRAM LENGTH | IDENT | CLOSEIOP | | | | | |
| ENTRY POINTS CLOSEIOP | 00012 | | | | | C1OP | 1 |
| EXTERNAL SYMBOLS | 00004 | | | | | | |
| TOP. | | | | | | | |
| | ENTR | CLOSEIOP | | | | | |
| | EXT | IOP. | | | | | |
| 00008 | SAVEAQ | BSS | 2 | | | C1OP | 2 |
| 00002 | 90 1 77777 | SAVE12 | ENI | 00,1 | | C1OP | 3 |
| 50 0 00000 | | | | | | C1OP | 4 |
| 00003 | 77 2 00000 | DLDA | SAVEAQ | | | C1OP | 5 |
| 12 0 P00000 | | | | | | C1OP | 6 |
| 00004 | 00 0 00000 | CLOSEIOP | OCT | 0 | | C1OP | 7 |
| 00 0 00000 | | | | | | C1OP | 8 |
| 00005 | 77 2 00000 | DSTA | (0)SAVEAQ | | | C1OP | 9 |
| 20 0 P00000 | | | | | | C1OP | 10 |
| 00006 | 56 1 P00002 | SIU | SAVE12+1 | | | C1OP | 11 |
| 50 1 00017 | | | | | | C1OP | 12 |
| 00007 | 04 1 00043 | ENI | 19,1 | | | C1OP | 13 |
| 50 0 00000 | + | END | 39,1 | | | C1OP | 14 |
| 00010 | 63 0 00031 | 63 | 318 | | | C1OP | 15 |
| 03 0 X77777 | + | 03 | (8)IOP. | | | C1OP | 16 |
| 00011 | 55 1 P00007 | IJP | 0-201 | | | | |
| 75 0 P00002 | | UJP | SAVE12 | | | | |
| | | END | | | | | |

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SUBROUTINE HFTRY
DIMENSION T,TLF(2),ZIL(2,50),VIL(2,50)
15 READ 1,10
1 FORMAT (A8)
IF (HEF,60) 15,14
14 IF (IL,EU,BNSTANT) 1,10,75
GO TO 15
75 LFN#60
76 IF (LPA,EU,60)READ (LFN,903) NCUR,RB,TITLE
IF (EGF,LHN) 77,78
77 ENDFILE A
REWIND A
GO TO 82
78 IL=2 8      WRITE (6) NCUR,RB,TITLE
79 IL=IL+4
IF (LPA,EU,60)READ (LFN,900) (ZIL(2,I),VIL(2,I),I=IL,1H)
WHITE ( 6) (ZIL(2,I),VIL(2,I),I=IL,1H)
IF (VIL(2,1H),LE,0,) GO TO 76
IL=IL+5
GO TO 78
900 FORMAT(10FR.4)
903 FORMAT (I1,F7.3,9AB)
82 RETURN
END

```

| | |
|------|----|
| RETY | 1 |
| RETY | 2 |
| RETY | 3 |
| RETY | 4 |
| RETY | 5 |
| RETY | 6 |
| RETY | 7 |
| RETY | 8 |
| RETY | 9 |
| RETY | 10 |
| RETY | 11 |
| RETY | 12 |
| RETY | 13 |
| RETY | 14 |
| RETY | 15 |
| RETY | 16 |
| RETY | 17 |
| RETY | 18 |
| RETY | 19 |
| RETY | 20 |
| RETY | 21 |
| RETY | 22 |
| RETY | 23 |
| RETY | 24 |

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DS RETRY

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PROGRAM LENGTH

IDENT

RETRY

ENTRY POINTS RETRY

00346

EXTERNAL SYMBOLS

00340

THEND,
QSCICT,
QSCIFER,
EFT,
REN,
TSR,
STA,
SLC,
SLI,
ONSINGL,

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SUBROUTINE INITRAYS
DIMENSION VBP(91)
COMMON /PATTERN/ SE,ITFP,DATE,SERLEV
COMMON /PDEF/ PI,PTR,TNCP
COMMON /RAYS/ NRAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),
1 ACTH(1000),PHASE(1000)
COMMON /IFC/ IFE,IA,IB,IP,IC,IS,LA
NRAY=0
EG=1000
PRINT 905
905 FORMAT (I0, 6AMD, GAMC, DGAMD, IC, SL, PHASE 0)
IF ((IA,EO,0,ARC,LA,EC,C,ER,LA,EG,1,ER,IA,EO,2) .LPC=60
IF ((IA,EO,1,SH,IA,EG,3) .LPC=2
10 IF (LPC,EO,60)READ (LFC,900)GAMLD,GAMDU,DGAMD,IC,SL,PH
IF (LPC,EO, 2)READ (LFC)      GAMLD,GAMDU,DGAMD,IC,SL,PH
IF (LA,EG,1)WRITE ( 2)      GAMLD,GAMDU,DGAMD,IC,SL,PH
PRINT 906,GAMLD,GAMDU,DGAMD,IC,SL,PH
906 FORMAT (1HU, 3F10.4, 15, 2F7.2)
SL=10,00,(1*(SL+SERLEV))
IFF#1
IF (ARS(UG+GAMC),LT,,0C1) GE T0 20
IF (NRAY,IEQ,0) GO TO 15
NRAY=NRAY+1
SS(NRAY)=0,
15 EG=EGAMU-GAMC
SEG=S+(EG/DTR)
IFF#0
20 G=EG+LGAMD
S=S\A(G/DTR)
NRAY=NRAY+1
IF (NRAY,GT,1000) GE T0 100
TGAM(NRAY)=S/SCRT(1,.S+S)
ZZ(NRAY)=SD
TIME(NRAY)=C,
ACTR(NRAY)=C
PHASE(NRAY)=PF/DTW
SS(NRAY)=SL+,5*ABS(S-SEG)
IF (IFF,NE,0) SS(NRAY+1)=SS(NRAY+1)+SL+,5*ABS(S-SEG)
IFF#1
0G=G
SEG=S
IF ( (G + ,0000001) ,LT, GAMLD ) GO TO 20
IF ((C,NE,0) GE T0 10
23 IF (ITBP,IEQ,0) GO TO 25
IL=1
25 IL=IL+1
IF ((IA,EG,0,ARC,LA,EC,C,ER,LA,EG,1,ER,IA,EO,1) .LP =60
IF ((IA,EG,2) .LP#7
IF (LP,EU,60)READ(LF ,901)(VBP(I),I=IL,1H)
IF (LP,EU, 7)READ(LF )      (VEP(I),I=IL,1H)
IF (LA,EU,1)WRITE( 7)      (VBF(I),I=IL,1H)
PRINT 907,(VBP(I),I=IL,1H)
907 FGMAT(=0VBF +,20)9,1)
IF (VBP(1H),EC,0,) GE T0 27
IL=IL+2U
GE T0 25
INIT 1
INIT 2
INIT 3
INIT 4
INIT 5
INIT 6
INIT 7
INIT 8
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INIT 55
INIT 56

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| | | |
|-----|---|---------|
| 27 | IF(IH,EU,1) GE TO 28 | INIT 57 |
| | IF(VBP(IH),EC,0,) GE TO 27 | INIT 58 |
| 28 | GE 29 I=IH,9C | INIT 59 |
| 29 | VBP(I+1)=VBP(IH) | INIT 60 |
| | GE 31 I=1,NRAY | INIT 61 |
| | DBABS(D)R=ATAN(TGAM(I))+CATD) | INIT 62 |
| | NAD | INIT 63 |
| | DBDn | I-IT 64 |
| | D=(1,-D)*VBP(N+1)*[-VBF(N+2) | INIT 65 |
| 31 | SS(I)=SS(I)+10,=-(-1,E-1*D) | INIT 66 |
| 35 | PRINT 903,(I,TGAM(I)),SS(I),PHASE(I),I=1,NRAY) | INIT 67 |
| | IF (LA,EU,1,ER,IA,EG,1,UR,IA,EC,3) REWIND 2 | INIT 68 |
| | IF (LA,EU,1,ER,IA,GE,2) REWIND 7 | INIT 69 |
| | RETURN | INIT 70 |
| 100 | IF(IC,EU,0) GE TO 28 | INIT 71 |
| | READ 904,IC | INIT 72 |
| | GE TO 100 | INIT 73 |
| 900 | FORMAT (3F10.4, I5, 2F5,2) | INIT 74 |
| 901 | FORMAT(20E4,1) | INIT 75 |
| 902 | FORMAT(*0 INITIAL TAN GAMMA, SIGNAL LEVEL, AND PHASE//) | INIT 76 |
| 903 | FORMAT (2F11.0, 3F15.5) | INIT 77 |
| 904 | FORMAT(18X,12) | INIT 78 |
| | END | INIT 79 |
| | | INIT 80 |
| | | INIT 81 |

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S INITRAYS

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ED 0

| PROGRAM LENGTH | IDENT | INITRAYS |
|----------------|-------|----------|
| ENTRY POINTS | 01026 | INITRAYS |
| BLOCK NAMES | 00220 | |
| PATTERN | 00004 | |
| PICDEF | 00003 | |
| RAYS | 13561 | |
| IFC | 00007 | |

EXTERNAL SYMBOLS

TMERC,
Q2CL7111
Q1C1010U
Q1C0310U
QBLCLCT,
SURTF
S1AF
ATAAF
HEW,
TSW,
TSA,
STW,
STA,
ONSINGL,

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SUBROUTINE HBLTRD(FB) \$ COMMON /PIDEF/ PI,DTR,INAP!
 COMMON /INFO/ IDUM(2),EMEGA,ICMH(17)
 COMMON /M14HCR5/ PERL,EMLT(200),BPST(200)
 DIMENSION DR(50),LG(50),CTSTR(600),HR(91,4),BP(91,4),ISW(4),
 1 RHL(50),ICL(50),DTM(600)
 COMMON/ABC/PLRCHUB(10),INCR,NBRS,NSRS,ALIM,IFT,IFT1
 COMMON /IC/ IFE,IA,IJIP,IC,IS,LA
 EQUIVALENCE (LR,DTSTR(551)),(DG,DTSTR(501)),(ICL,DTSTR(451)),
 1 (RBL,DTSTR(401)),(ISW,DTSTR(397)),(RR,DTSTR),(ISCP,DTSTR(396)),BLRD 1
 2 (IE,DTSTR(395)),(IB,DTSTR(394)),(K,DTSTR(393)),BLRD 2
 3 (IL,DTSTR(392)),(IH,DTSTR(391)),(IG,DTSTR(390)),BLRD 3
 EQUIVALENCE (R,DTSTR(389)),(T,DTSTR(388)),(F,DTSTR(387)),(PH),
 1 DTSTR(386)),(DLE,DTSTR(385)),(R,DTSTR(384)),BLRD 4
 2 (RN,DTSTR(383)) \$ EQUIVALENCE (BH,DTSTR(183))
 DATA ((DTSTRH(I),I=501,600)=
 1 19., 35., 40., 52., 6(90.),BLRD 5
 2 19., 25., 35., 45., 55., 5(90.),BLRD 6
 3 11., 20., 25., 35., 45., 56., 4(90.),BLRD 7
 4 11., 20., 30., 40., 55., 5(90.),BLRD 8
 5 5., 7.5, 16.5, 17.5, 19., 20., 21., 22.5, 2(90.),BLRD 9
 1 0., 3.7, 4.5, 7(6.),BLRD 10
 2 0., 2.3, 4.6, 6.5, 6(8.),BLRD 11
 3 0., 3., 4.4, 6.7, 8.5, 5(10.),BLRD 12
 4 2., 5.2, 7.7, 9.8, 6(12.),BLRD 13
 5 4., 5.2, 12., 12.8, 13.4, 13.7, 13.9, 3(14.),BLRD 14
 DATA ((UTSTRH(I),I=401,500)=
 1 18., 30., 40., 50., 55., 5(90.),BLRD 15
 2 17., 20., 30., 40., 50., 55., 4(90.),BLRD 16
 3 13., 20., 35., 45., 52.5, 5(90.),BLRD 17
 4 7.5, 11., 20., 25., 30., 34., 4(90.),BLRD 18
 5 2.5, 5., 7.5, 15., 17.5, 20., 22., 3(90.),BLRD 19
 1 0., 2.6, 4.4, 5.4, 6(6.),BLRD 20
 2 0., 1.3, 4.6, 7., 8.5, 5(9.),BLRD 21
 3 3., 5.3, 8.7, 10.3, 6(11.),BLRD 22
 4 3., 4., 10.4, 12.7, 13.7, 5(14.),BLRD 23
 5 8., 11.7, 20., 14.1, 15., 15.8, 4(16.),BLRD 24
 DATA ((UTSTRH(I),I=301,400)=
 1 19., 25., 35., 45., 51., 5(90.),BLRD 25
 2 18., 25., 35., 45., 55., 5(90.),BLRD 26
 3 14., 20., 30., 40., 50., 53., 4(90.),BLRD 27
 4 8., 12., 20., 22.5, 26., 5(90.),BLRD 28
 5 2.5, 4.5, 7.5, 10., 14.5, 17.5, 20., 23., 2(90.),BLRD 29
 1 0., 1.5, 3.2, 5.1, 6(6.),BLRD 30
 2 0., 2.8, 5.5, 7.6, 6(9.),BLRD 31
 3 3., 5., 7.5, 9.4, 10.8, 5(11.),BLRD 32
 4 3., 6.1, 12.2, 13.2, 6(14.),BLRD 33
 5 9., 10., 12., 13.9, 16., 17.1, 17.7, 3(18.),BLRD 34
 DATA ((UTSTRH(I),I=201,300)=
 1 18., 23., 30., 40., 50., 55., 4(90.),BLRD 35
 2 17., 20., 25., 30., 35., 45., 55., 3(90.),BLRD 36
 3 13., 23., 30., 35., 42.5, 45., 50., 3(90.),BLRD 37
 4 9., 12.5, 20., 22.5, 27., 5(90.),BLRD 38
 5 2.5, 4.5, 7.5, 10., 14.5, 17.5, 20., 23., 2(90.),BLRD 39
 1 3., 4., 6., 7.4, 5(8.),BLRD 40
 2 0., 1.7, 3.2, 5.6, 6.8, 8.8, 4(10.),BLRD 41
 3 3., 6.6, 8., 9.1, 10.4, 10.7, 4(11.),BLRD 42

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4 7.1 0.. 12.. 13.1, 6(14.,) BLRD 97
5 0.. 10.. 12.. 13.9, 16.. 17.1, 17.7, 3(18.,) BLRD 98
DATA ((DTSTA(I),I=101,200)) BLRD 99
1 2.5, 10.. 12.5, 15.. 20.. 25.. 30.. 35.. 40.. 90.. BLRD 60
2 2.5, 7.5, 12.5, 20.. 25.. 32.5, 37.5, 42.5, 2(90.), BLRD 61
3 2.5, 5.. 7.5, 12.5, 17.5, 22.5, 27.5, 32.5, 2(90.), BLRD 62
4 2.5, 7.5, 10.. 11.5, 13.. 19.. 20.. 24.. 2(90.), BLRD 63
5 2.5, 5.. 8.5, 10.. 12.5, 15.. 20.. 22.5, 27.5, 90.. BLRD 64
1 3.5, 5.4, 6.. 6.6, 7.7, 8.6, 9.4, 9.8, 2(10.), BLRD 65
2 6.5, 8., 9.5, 11.. 11.9, 13.. 13.4, 3(13.5), BLRD 66
3 7.. 9.4, 11.5, 14.. 14.7, 15.1, 15.4, 3(15.5), BLRD 67
4 9.. 13.5, 15.2, 16.. 16.6, 17.. 17.4, 3(17.5), BLRD 68
5 11.. 13.6, 16.. 17.. 18.1, 18.8, 19.6, 19.8, 2(20.,) BLRD 69
DATA ((UTSTH(I),I=1,100)) BLRD 70
1 7.5, 11.. 13.5, 15.. 17.5, 20.. 25.. 27.5, 2(90.), BLRD 71
2 7.5, 10.. 11.5, 14.. 15.. 17.5, 20.. 25.. 29.5, 90.. BLRD 72
3 7.5, 12.. 15.. 18.. 20.. 22.5, 25.. 27.. 90.. 90.. BLRD 73
4 7.5, 10.. 14.. 17.5, 20.. 22.5, 25.. 28.. 90.. 90.. BLRD 74
5 2.5, 5.5, 8.. 10.. 15.. 17.5, 20.. 23.. 90.. 90.. BLRD 75
1 6.5, 8.6, 9.8, 10.8, 11.. 11.7, 12.7, 3(13.), BLRD 76
2 7.. 8.8, 10.. 10.6, 11.1, 11.9, 12.5, 13.4, 2(14.), BLRD 77
3 8.. 11.. 12.8, 14.. 14.8, 15.4, 15.8, 3(16.), BLRD 78
4 9.. 11.. 13.5, 14.2, 15.6, 16.2, 16.6, 3(17.), BLRD 79
5 10.. 13.. 15.. 16.. 17.8, 18.4, 18.7, 3(19.,) BLRD 80
IF (IFT1(EU,1) GE TE 2 BLRD 81
DE 1 J#1,600 BLRD 82
1 CTM(J)=LTSTH(J) BLRD 83
IFT#1
GE TE 3 BLRD 84
2 DE 4 J#1,600 BLRD 85
4 CTSTR(J)=UTH(J) S I#80 BLRD 86
3 FR=0MEGA/TWUPI S IF(FR,LT,300,) GE TE 25 BLRD 87
IF(FR,GT,1500,) GW TE 10 S IF(FR,LT,750,) GE TE 5 S I#801 BLRD 88
GE TE 20 BLRD 89
5 IC=401 S GE TE 20 BLRD 90
10 IF(FR,L,2750,) GE TE 15 S IC=101 S IF(FR,GT,6000,) I#01 BLRD 91
GE TE 20 BLRD 92
15 IC=201 BLRD 93
20 DE 24 I#5(1,600 S CTSTR(I)=CTSTR(IQ) BLRD 94
24 IC=IC+1 BLRD 95
25 DE 30 I#1,500 BLRD 96
30 CTSTR(I)=0, S ISCP=HE BLRD 97
IF (Iw,EQ,0,4EC,LA,EC,C,ER,LA,EC,1,ER,IJ,EQ,2) LPB#60 BLRD 98
IF (Iw,EQ,1,ER,IJ,EC,3) LPB#9 BLRD 99
40 I#01 S IF(LPB,EC,60)READ (LPB,900)RBL(I#),ICL(I#) BLRD 100
IF(LPB,EC,9)READ (LPB) RBL(I#),ICL(I#) BLRD 101
IF(LA,EU,1)WRITE ( 9) RBL(I#),ICL(I#) S IF(RBL(I#)) 41,41,42 BLRD 102
IF(LA,EU,1)WRITE ( 9) RBL(I#),ICL(I#) S IF(RBL(I#)) 41,41,42 BLRD 103
41 RBL(I#)=1,ES0 BLRD 104
42 IF(ICL(I#)) 43,43,44 BLRD 105
43 ICL(I#)=0 S GE TE 60 BLRD 106
44 IF(ICL(I#)=9) 46,46,45 BLRD 107
45 ICL(I#)=ICL(I#)/10 BLRD 108
46 IF(ICL(I#)=5) 60,60,47 BLRD 109
47 K=ICL(I#)+5 S IF(I#W(K)) 48,48,60 BLRD 110
48 I#W(K)=2 S I#=1 BLRD 111
49 I#=I#+1 Y S IF(LPB,EC,60)READ (LPB,901)(BR(I,K),I#I#,I#H) BLRD 112

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IF (LPP, EQ, 0) HEAD (LFB) (BR (I, K), I=IL, IH)
IF (LA, EQ, 1) WRITE ( 9, (BR (I, K), I=IL, IH)  S IL=IL+20
IF (BR (IH, K)) 51,51,49
50 IF (BR (IH, K)) 51,51,53
51 IH=IH+1  S IF (IH) 52,52,50
52 IH=1
53 D6 54 I=IH,90
54 BR (I+1, K)=BR (IH, K)  S IL=1  S IF (ISCP) 60,60,55
55 IH=IL+1  S IF (IJ, EG, 0, AND, LA, EG, 0, OR, LA, EQ, 1, OR, IJ, EQ, 1) LPP=60
IF (IJ, GE, 2) LPP=85  IF (LPP, EG, 60) READ (LPP, 901) (BP (I, K), I=IL, IH)
IF (LPP, EQ, K) READ (LPP) (BP (I, K), I=IL, IH)
IF (LA, EQ, 1) WRITE (8) (BP (I, K), I=IL, IH)  S IL=IL+20
IF (BP (IH, K)) 55,60,55
60 IF (RBL (IB), LT, 1, E15) GE TO 40  S DO 65 K=6,9
IF (ISW (K=5)) 65,65,61
61 PRINT 902, K=5 PRINT 903, (I, BR (I+1, K=5), BP (I+1, K=5), I=E, 90)
65 CONTINUE  S PRINT 900 S UP 70 I=2, IB  S RN=RBL (I=1)
PRINT 904, H, RH, ICL (I=1)
70 RBRN  S PRINT 905, H, ICL (IH)  S IE=1
71 IC=ICL (IE)  S IF (IC) 76,76,80
72 DO 77 I=1, 200  S BRLT (I)=1,
77 BPST (I)=0,  S GO TO 100
78 DO 99 I=1, 200  S TO [TR=ATAN (0.01*(I-1))  S K=IC=5  S IF (K) 81,81,95
80 IL=10*IC  S IF (DG (IL=9), GE, T) GO TO 93
81 IF (DG (IL=8), GE, T) CG TO 92  S IL=IL+1  S GO TO 82
82 DCB=CB (IL=9)*(T-DG (IL=9))*(DB (IL=8)-DB (IL=9))/(DG (IL=8)-DG (IL=9))
83 GE TO 94
84 DCB=CB (IL=9)
85 PHI=0,  S GO TO 9M
86 NOT  S FOFEN  S DCB=ER (N+1, K)+F=(BR (N+2, K)+BR (N+1, K))  S PHI=0,
87 IF (ISCP, NE, 0) PHI=BP (N+1, K)+F=(BP (N+2, K)+BP (N+1, K))
88 BPST (I)=PHI
89 BRLT (I)=10, **(I-1)[CE]
90 RB=RBL (IE)  S RETURN  S ENTRY AWRRLT  S IE=IE+1
91 IF (IC=ILL (IE)) 75,100,75
900 FORMAT (F8,4,12)
901 FORMAT (Z0F4,2)
902 FORMAT ($8HUSER SUPPLIED BOTTOM LOSS TABLE CLASS ,15/1X
1 3(2HG,6X,2HCH,7X,3HFH1,10X))
903 FORMAT (3(F10,3,F6,3,YY))
904 FORMAT ($H FHFH, F10,2,3H TO, F10,2,16H KM BOTTOM CLASS,15)
905 FORMAT ($H FHFH, F10,2,3H TO, 3X,23HENU OF RUN BOTTOM CLASS,15)
END

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BRLTRD

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ED 0

| | ICENT | BRLTRD |
|------------------|-------|--------|
| PROGRAM LENGTH | 03503 | |
| ENTRY POINTS | 02361 | |
| | 03321 | |
| BLOCK NAMES | | |
| PIPEF | 00003 | |
| INFL | 00024 | |
| MIRRORS | 00021 | |
| ABC | 00026 | |
| ITP | 00007 | |
| EXTERNAL SYMBOLS | | |
| N1C1010U | | |
| THEAD, | | |
| 01003100 | | |
| C2007111 | | |
| 080LICT, | | |
| A1A0F | | |
| TSR, | | |
| TSR, | | |
| STH, | | |
| STB, | | |
| 0NSINGL, | | |

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SUBROUTINE WORD SIZE
COMMON /RAYS/ ARAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),
1 NCOUNT(1000),PHASE(1000) WORD 1
1 COMMON /INF0/ RSTART,RMAX,EMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1 ISGP,IT1,IT2,IT3,IPEN,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT WORD 2
1 COMMON /TRIANG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZER0(100), WORD 3
1 RZER0(100),AA(100),BB(100),SST(100),CCT(100),NTR WORD 4
COMMON /TLE/ STITLE (10) WORD 5
COMMON/ABC/PLANCHB (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1 WORD 6
COMMON /RANST/ RDUM,IREC,IFSK,SCUM WORD 7
DATA (JBIG=3777777777777777), (IENT=0) , (IFSK=-1) WORD 8
ENTRY INIT WORD 9
IF (IFT1,EQ,0) GO TO 2 WORD 10
JBIG=3777777777777777 3 IENT=0 WORD 11
2 ITN=SQR((SORT(JBIG/4,)) WORD 12
ITN2=ITN+2 WORD 13
ITN3=ITN2+ITN WORD 14
IBIG=ITN3+ITN WORD 15
RETURN WORD 16
ENTRY RAY TAPE WORD 17
ZB=AL(NTR)+BL(NTR)+RMAX WORD 18
IF (IENT,NE,0) GO TO 1 WORD 19
WRITE (LTRT)STITLE,AL,IP,ABRS,NSRS,ITN WORD 20
IENT=1 3 IREC=1 3 IFSK=IFSK+1 WORD 21
1 WRITE (LTRT) NRAY,RMAX,ZB,(TGAM()),I=1,NRAY),(ZZ()),I=1,NRAY),
1 (SS()),I=1,NRAY),(NCOUNT(),I=1,NRAY),(TIME(),I=1,NRAY),
2 (PHASE()),I=1,NRAY) 3 IREC=IREC+1 WORD 22
2 RETURN WORD 23
END WORD 24
WORD 25
WORD 26
WORD 27
WORD 28
WORD 29

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S WORDSIZE

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ED 0

| | IDENT | WORDSIZE |
|------------------|---|--|
| PROGRAM LENGTH | 00217 | |
| ENTRY POINTS | INIT
RAYTYPE
WORDSIZE | 00012
00044
00005 |
| BLOCK NAMES | RAY8
INFO
TRIANG
TLE
ABC
RANST | 13561
00024
02261
00012
00026
00004 |
| EXTERNAL SYMBOLS | 01010100
THEAD,
080CICT,
SQRTF
STB,
SLC,
ONSINCL, | |

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SUBROUTINE NEWPROF(ZMAX)                               NEWP  1
COMMON /INFO/ RSTART,RMAX,OMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,    NEWP  2
1  ISGP,IT1,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT      NEWP  3
COMMON /PROFIL/ R1,N1,Z1(50),V1(50),R2,N2,Z2(50),V2(50),IBATC,IPFLNEWP  4
COMMON /INPUT/ RBOT(250),ZBOT(250),ZIL(2,50),VIL(2,50),NN(2),ICON(2)NEWP  5
1,50)
COMMON /TLE/STITLE (10)                             NEWP  6
COMMON /PRB/ IPROP,KNM,PLTL,RH,IPCB,IFPR             NEWP  7
DIMENSION TITLE(9),PM(3),LIN (114)                  NEWP  8
COMMON/ABC/PUNCHDB (16),INCR,NSRS,NSRS,ALIM,IFT,IFT1      NEWP  9
COMMON /IFC/ IFE,IA,IB,IK,ID,IS,LA                   NEWP 10
COMMON /RANST/ RS,NDUMM,SDS                         NEWP 11
DATA (NBPT=0),(IFE0F=0),(LIN=114(1H)),(IFT2=0),(IRH=0)      NEWP 12
IFE=IFE0F S IF (IFT1,EG,IFT2) GO TO 952   S IRH=0  S IFT2=IFT1  NEWP 13
992 IF (IFT1,EG,0,OR,IRH,EG,1) GO TO 950   S NBPT=0 S IFE0F=0 S IFE=IFE0FNEWP 14
IRH=1  S N2=0  S R2=0.0  S N1=0  S R1=0.0  S IFPR=0  NEWP 15
DO 991 J=1,114                                     NEWP 16
991 LIN(J)=1H                                      NEWP 17
990 IF(NBPT,GT,0) GO TO 20                          NEWP 18
C          FIRST ENTRY, READ IN BOTTON TRACK          NEWP 19
1L=1 S IF ((ID,EG,0,AND,LA,EG,0,OR,LA,EG,1) LP1=60S IF((ID,EG,1)LP1=5)NEWP 20
2  IL=IL+4                                         NEWP 21
IF(LPI,EG,60)READ (LPI ,900) (RBOT(),ZBOT(),I=IL,1H)        NEWP 22
IF(LPI,EG,5)READ (LPI )   (RBOT(),ZBOT(),I=IL,1H)        NEWP 23
IF(LA,EG,1)WRITE ( 5)   (RBOT(),ZBOT(),I=IL,1H)        NEWP 24
IF(RBOT(1H),LE,0,) GO TO 3 S IL=IL+5 S GO TO 2          NEWP 25
3  IH=IH+1  S IF(RBOT(1H),LE,0,) GO TO 3           S NBPT=IH  NEWP 26
IF ((LA,EG,1,OR,1,DE,0,1) REWIND 5                 NEWP 27
PRINT 901,(RBOT(),ZBOT(),I=1,NBPT)  S IF ((IBATC,LE,0) 30 TO 1  NEWP 28
DO 3 I=1,NBPT                                     NEWP 29
9  ZBOT()=ZBOT()*(1.+5*ZBOT()/.6371221.3)          NEWP 30
1  CONTINUE S WRITE (35,611),STITLE,(RBOT(J),ZBOT(J),J=1,NBPT)  NEWP 31
FORMAT (10A8,/,1,0F8.3)                           NEWP 32
611 FORMAT (10F8.3)                                NEWP 33
ZMAX=0, SD0 4 I=1,NBPT                           NEWP 34
IF(ZBOT(),GT,ZMAX) ZMAX=ZBOT()                  NEWP 35
4  CONTINUE                                         NEWP 36
IBPT=0 S IF ((IS,EG,0,AND,LA,EG,0,OR,LA,EG,1) LPN=60  NEWP 37
NN(2)=0 S IF ((IS,EG,1) LPN=6  NEWP 38
DO 55 I=1,2                                     NEWP 39
DO 55 J=1,50                                     NEWP 40
ZIL(1,J)=0.0                                     NEWP 41
VIL(1,J)=0.0                                     NEWP 42
55 ICON(1,J)=0                                     NEWP 43
NN(1)=0                                         NEWP 44
NIB=0                                           NEWP 45
DR 56 J=1,50                                     NEWP 46
Z1(J)=0.0                                       NEWP 47
V1(J)=0.0                                       NEWP 48
Z2(J)=0.0                                       NEWP 49
56 V2(J)=0.0                                     NEWP 50
ASSIGN 6 TO IRET                                 NEWP 51
GO TO 70                                         NEWP 52
C          AT 70 IS THE READIN AND CONNECT ROUTINE, RETURN IS TO IRET  NEWP 53
6  ASSIGN 20 TO IRET                                NEWP 54
GO TO 70                                         NEWP 55
                                         NEWP 56

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20    IBPT=IBPT+1
      IF (IBPT.LE.NBPT) GO TO 21
      RBT=.001*R2+100,
      IFPR=1
      GO TO 22
21    RBT=RBT(IBPT)
      ZBT=ZBT(IBPT)
      IF (RM,LE,RBT.AND.,IFE0F,EO.1,AND.RS,NE.0.0) IFPR=1
22    IF (RBT,LE,RB) GO TO 25
C     GET NEW INPUT PROFILE
      ASSIGN 23 TO IRET
      GO TO 70
23    IF (IBPT.GT.NBPT) GO TO 25
      IBPT=IBPT+1
      ZBT=ZBT+(RA-RBT)*(ZBT-ZBT(IBPT))/(RBT-RBT(IBPT))
C     THIS IS THE BOTTOM DEPTH AT PROFILE RANGE
      RBT=RA
25    R1=R2
      N1=N2
C     MOVE PROFILE 2 TO PROFILE 1
      DO 27 I=1,N2
      Z1(I)=Z2(I)
27    V1(I)=V2(I)
      R2=1000.+RBT
      FA=(RB+RBT)/(RB-RA)
      FB=1.+FA
      N2=1
29    IF (ICON(1,N2).GT.AN(1)) ICON(1,N2)=NN(1)
      IF (ICON(2,N2).GT.AN(2)) ICON(2,N2)=NN(2)
      Z=FA*ZIL(1,ICON(1,N2))+FB*ZIL(2,ICON(2,N2))
      V=FA*VIL(1,ICON(1,N2))+FB*VIL(2,ICON(2,N2))
      IF (N2.GT.1.AND.Z.LT.ZZ(N2-1)) 125,126
125  Z=Z2(N2-1)
      V=V2(N2-1)
126  IF (Z.GT.ZBT-.1.) GO TO 35
      Z2(N2)=Z
      V2(N2)=V
      N2=N2+1
      IF (N2.LE.NIB) GO TO 29
C     EXTRAPOLATION TO BOTTOM
      Z2(N2)=ZBT
      M=N2-1
31    M=M-1
      Z=Z2(M)
      IF (ABS(Z-Z2(N2-1)).LT.1,E-5*Z) GO TO 31
      V=V2(M)
      V2(N2)=V2(M)+(ZBT-Z)*(V2(N2-1)+V)/(Z2(N2-1)-Z)
      GO TO 40
35    Z2(N2)=ZBT
      V2(N2)=V2(N2-1)+(ZBT-ZZ(N2-1))*(V-V2(N2-1))/(Z-Z2(N2-1))
C     REMOVE DUPLICATE POINTS
40    M=2
      IDC=0
42    IF (Z2(M).GT.Z2(M-1)+0.0001) GO TO 45
      IDC=1
      N2=N2+1
      NEWP  97
      NEWP  98
      NEWP  99
      NEWP  60
      NEWP  61
      NEWP  62
      NEWP  63
      NEWP  64
      NEWP  65
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      NEWP 101
      NEWP 102
      NEWP 103
      NEWP 104
      NEWP 105
      NEWP 106
      NEWP 107
      NEWP 108
      NEWP 109
      NEWP 110
      NEWP 111
      NEWP 112

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DO 44 I=M,N2
Z2(I)=Z2(I+1)
V2(I)=V2(I+1)
M=M+1
IF(M.LE.N2) GO TO 42
IF (IDC,GT,0) GO TO 40
IF (Z2(N2+1),EQ,0,0) GA TO 46
N5=N2+1
DO 47 I=N5,50
Z2(I)=0.0
47 V2(I)=0.0
48 IF ((IPROP,EQ,0,0R,IPROP,EQ,1)) GO TO 54
PRINT 902,R2
PRINT 914
DO 7 J=1,N2
NV=V2(J)-1455.5
IF (NV.LT.4.0R.NV,GT,114) GO TO 48
LIN(NV)=1H
PRINT 915,Z2(J),V2(J),LIN
LIN(NV)=1H
GO TO 7
48 PRINT 915,Z2(J),V2(J)
7 CONTINUE
54 IF (IPFL,EQ,1) CALL PRAFPLOT (RB,N3,INPF)
IF (IPFL,EQ,2) CALL PRAFPLOT (RB,N3,INPF)
IF (RS.GE,RRBT(2),0R,IFE0F,EQ,1) RETURN $ PRINT 279 $ CALL BYERYE NEWP 130
275 FORMAT (5X,OPROGRAM ABORTED, TWO SOUND SPEED PROFILES INPUT REFORERENEWNEWP 139
1 SECOND BOTTOM POSITION)
70 IF(NN(2),EQ,0) GO TO 75 $ NB=NN(2) $ DO 71 I=1,NB
ZIL(1,I)=ZIL(2,I)
71 VIL(1,I)=VIL(2,I)
RA=RB
73 NN(1)=NN(2)
IF (IFE0F,EQ,0) GO TO 76
RB=RB+1,E6
GO TO 82
76 IF(LPN,EQ,60)READ (LPN ,903) NCUR,RB,TITLE
IF(LPN,EQ, 6)READ (LPN) NCUR,RB,TITLE
IF(E0F,LPN ) 77,78
77 IFE0F#1 $ IFE+IFE0F
RB=RA+1,E6 $ IF (LA,EQ,1) ENDFILE 6
IF (LA,EQ,1,OR.IS,EQ,1) REWIND 6 $ GO TO 82
78 IL=1 $ IF (LA,EQ,1) WRITE (6) NCUR,RB,TITLE $ RS=RB
79 IH=IL+4
IF(LPN,EQ,60)READ (LPN ,900) (ZIL(2,I),VIL(2,I),I=IL,IH)
IF(LPN,EQ, 6)READ (LPN) (ZIL(2,I),VIL(2,I),I=IL,IH)
IF(LA EQ 1)WRITE ( 6) (ZIL(2,I),VIL(2,I),I=IL,IH)
IF(VIL(2,IH).LE,0,) GO TO 81
IL=IL+5
80 GO TO 79
81 IH=IH+1
IF(VIL(2,IH).LE,0,) GO TO 81
NN(2)=IH
N3=IH
INPF=0
IF ((IPROP,EQ,0)) GO TO 74

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PRINT 904,RB,TITLE          NEWP 169
PRINT 914                  NEWP 170
74 DO 20 I=1,1H             NEWP 171
  IF (VIL(2,I).LT.1400.0)BR,VIL(2,I),GT;1650.0) 58,57    NEWP 172
58 PRINT 920,RB,ZIL(2,I),VIL(2,I)                      NEWP 173
52A FORMAT (1H1,5X,•INPLT ERROR IN PROFILE AT RANGE•,F10.4,5X,•VALUE AT•NEWP 174
  1 DEPTH•,F10.3,••E0,F10.3,• H/SEC•)                   NEWP 175
  CALL BYEBYEF                                         NEWP 176
57 IF (ZIL(2,I).NE.SDS) GO TO 257 S PRINT 258,ZIL(2,I),RB$CALL BYEBYEENEWP 177
258 FORMAT (5X,•PROGRAM ABARTED, INPUT PROFILE DEPTH•,F10.3,1X,••SBURCNEWP 178
  1E DEPTH, AT RANGE•,F10.3,• KM•)                      NEWP 179
257 IF (I,EQ.1) GO TO 157 S IF (ZIL(2,I).LT.ZIL(2,I-1)) 60 TA 50    NEWP 180
157 IF (IPROP,EQ.0) GO TO 28  SNV=VIL(2,I)-.495.5           NEWP 181
  IF (NV,LT,4.0R,NV,GT,114) 60 TA 38 S LIN(NV)=1HV        NEWP 182
  PRINT 915,ZIL(2,I),VIL(2,I),LIN                         NEWP 183
  LIN (NV)=1H                                           NEWP 184
  GO TO 29                                         NEWP 185
38 PRINT 915,ZIL(2,I),VIL(2,I)                         NEWP 186
2A CONTINUE                                         NEWP 187
  IF (NCUR,GT,0) GO TO 80                           NEWP 188
  DO 80 I=1,1H                                     NEWP 189
    V,L(2,I)=VIL(2,I)*(1.+7IL(2,I)/6371221.3)          NEWP 190
  80 ZIL(2,I)=ZIL(2,I)*(1.+.5*ZIL(2,I)/6371221.3)        NEWP 191
  89 IF (IPFL,EQ,1) CALL PRAFPLOT (RB,N3,INPF)          NEWP 192
  IF (IPFL,EQ,2) CALL PRMFPLIT (RB,N3,INPF)          NEWP 193
  IF (NN(1),EQ,0)          GO TO IRET,(6,20,23)          NEWP 194
  82 ICN(1,1)=1                          NEWP 195
  ICN(2,1)=1                          NEWP 196
  NA=2                                NEWP 197
  NB=2                                NEWP 198
  NR=2                                NEWP 199
  83 IF (ZIL(2,NB).EQ.ZIL(1,NB)) GO TO 92            NEWP 200
  IF (NB,LE,NN(2)) GO TO 84                  NEWP 201
  IP=2                                NEWP 202
  GO TO 88                               NEWP 203
  84 IF (NA,LE,NN(1)) GO TO 85            NEWP 204
  IP=1                                NEWP 205
  GO TO 88                               NEWP 206
  85 DVMA=VIL(1,NA)-VIL(1,NA-1)          NEWP 207
  DVLA=DVMA                           NEWP 208
  DVHA=DVMA                           NEWP 209
  IF (NA,GT,2) DVLA=VIL(1,NA-1)-VIL(1,NA+2)          NEWP 210
  IF (NA,LT,NN(1)) DVHA=VIL(1,NA+1)-VIL(1,NA)          NEWP 211
  DVMB=VIL(2,NB)-VIL(2,NB-1)          NEWP 212
  DVLB=DVMB                           NEWP 213
  DVHB=DVMB                           NEWP 214
  IF (NB,GT,2) DVLB=VIL(2,NB-1)-VIL(2,NB+2)          NEWP 215
  IF (NB,LT,NN(2)) DVHB=VIL(2,NB+1)-VIL(2,NB)          NEWP 216
  PM(1)=ABS(ZIL(1,NA-1)-ZIL(2,NB))          NEWP 217
  IF (DVLA=DVMB,GE,0.,AND.DVMA=DVHB,GE,0,) PM(1)=PM(1)+250,
  PM(2)=ABS(ZIL(1,NA)-ZIL(2,NB+1))          NEWP 218
  IF (DVMA=DVLB,GE,0.,AND.DVHA=DVMB,GE,0,) PM(2)=PM(2)+250,
  PM(3)=ABS(ZIL(1,NA)-ZIL(2,NB))          NEWP 219
  IF (DVMA=DVMB,GE,0.,AND.DVHA=DVHB,GE,0,) PM(3)=PM(3)+250,
  BP=PM(1)                                NEWP 220
  IP=1                                NEWP 221
  NEWP 222
  NEWP 223
  NEWP 224

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D0 87 I=2,3          NEWP 225
IF(pH(I).GE,BP) GO TO 87      NEWP 226
IP=1                      NEWP 227
BP=PH(I)                  NEWP 228
CONTINUE                  NEWP 229
GO TO (90,91,92),IP      NEWP 230
ICON(1,NIB)=NA-1          NEWP 231
ICON(2,NIB)=NB            NEWP 242
NB=NB+1                  NEWP 233
GO TO 93                  NEWP 234
ICON(1,NIB)=NA            NEWP 235
ICON(2,NIB)=NB-1          NEWP 236
NA=NA+1                  NEWP 237
GO TO 93                  NEWP 238
ICON(1,NIB)=NA            NEWP 239
ICON(2,NIB)=NB            NEWP 240
NA=NA+1                  NEWP 241
NB=NB+1                  NEWP 242
IF(NA.GT.NN(1).AND.NB.GT.NN(2)) GO TO 1RET,(6,20,23)  NEWP 243
NIB=NIB+1                  NEWP 244
IF (NIB.LE.50) GO TO 83      NEWP 245
PRINT 905                  NEWP 246
CALL WVEBYE                NEWP 247
FORMAT(10F8.4)              NEWP 248
FORMAT(24H0LISTING OF BOTTOM TRACK/1H0.4X,9(6H R(KM),6X,4H2(M),4X)NEWP 249
1 //((1X,10F10.3))          NEWP 250
FORMAT(30H0INTERPOLATED PROFILE AT RANGE,F10.0,2H M//)    NEWP 251
FORMAT(11,F7.3,9A8)          NEWP 252
FORMAT(23H1INPUT PROFILE AT RANGE,F11,3,3H KM,5X,9A8//)  NEWP 253
FORMAT(3X,.DEPTH (M)=.2X,.VELOCITY=.0,1460=.6X,.1470=.6X,.1480=.6X,NEWP 254
1.1490=.6X,.1500=.6X,.1510=.6X,.1520=.6X,.1530=.6X,.1540=.6X,.1550=.6X,NEWP 255
2,6X,.1560=.6X,.1570=.6X,/)  NEWP 256
FORMAT (1X,F11.4,F10.4,114A1)  NEWP 257
FORMAT ( 29H0*00 MANY POINTS (INTERPOLATED)  NEWP 258
END                         NEWP 259

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| | | | | | |
|------------------|----------|-------|----------|----|---|
| DS | NEWPROF | | 07/30/73 | ED | 0 |
| | | IDENT | NEWPROF | | |
| PROGRAM LENGTH | | 03072 | | | |
| ENTRY POINTS | NEWPROF | 00471 | | | |
| BLOCK NAMES | | | | | |
| | INFO | 00024 | | | |
| | PROFIL | 00316 | | | |
| | INPUT | 01442 | | | |
| | TLE | 00012 | | | |
| | PRO | 00006 | | | |
| | ABC | 00026 | | | |
| | IFC | 00007 | | | |
| | RANST | 00004 | | | |
| EXTERNAL SYMBOLS | | | | | |
| | THEEND, | | | | |
| | Q1010500 | | | | |
| | Q80DICT, | | | | |
| | PROFPLOT | | | | |
| | PROFPLIT | | | | |
| | BYEBYE | | | | |
| | OBGIFEOF | | | | |
| | EFT, | | | | |
| | REW, | | | | |
| | TSH, | | | | |
| | TSB, | | | | |
| | STH, | | | | |
| | STD, | | | | |
| | SLG, | | | | |
| | SLI, | | | | |
| | GNSINGL, | | | | |

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SUBROUTINE CONNECT
C6MMON /PROFIL/ N1,N1,Z1(50),V1(50),R2,N2,Z2(50),V2(50),IBOTC,IPFL,CONN 1
C6MMON /THIANG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZERO(100),CONN 2
1 RZERG(100),AA(100),ER(100),SST(100),CCT(100),NTRI,CONN 3
NA=NB=1
NTRI=0
IADD=0
10 NTRI=NTHI=1
IF(NB,BN,N2) GO TO 12
IF (IADD,EO,1,FR,NA,EO,V1) GO TO 30
12 RZERG(NTRI)=R2
ZZERG(VTRI)=Z2(NH)
AL(NTRI)=Z1(NA+1)
BL(NTRI)=(Z2(NB)-Z1(NA+1))/(R2-R1)
AA(NTRI)=1./V2(NH)**2
R2=(1.,BN/V1(NA)**2+1.,DC/V1(NA)**2)/(Z1(NA)-Z1(NA+1))
R3=(1.,BN/V2(NB)**2+1.,DC/V2(NA)**2+BL*(Z2(NB)-Z1(NA)))/(R2-R1)
NA=NA+1
IADD=1
GO TO 40
30 RZERG(NTRI)=R1
ZZERG(NTRI)=Z1(NA)
AL(NTRI)=Z1(NA)
BL(NTRI)=(Z1(NA)-Z2(NA+1))/(R1-R2)
AA(NTRI)=1./V1(NA)**2
R2=(1.,BN/V2(NA)**2+1.,DC/V2(NA)**2)/(Z2(NB)-Z2(NA+1))
R3=(1.,BN/V1(NA)**2+1.,DC/V1(NA)**2+BL*(Z1(NA)-Z2(NA)))/(R1-R2)
NB=NA+1
IADD=2
GO TO 40
40 RZ(NTRI)=SIGN(SQRT(B2**2+BR**2),BZ)
IF(BR(NTRI),EC,0.) GO TO 41
SST(NTRI)=BR/BB(NTRI)
CCT(NTRI)=BZ/BR(NTRI)
GO TO 46
41 CCT(NTRI)=1,
SST(NTRI)=0,
42 AL(NTRI)=AL(NTRI)+BL(NTRI)*R1
TANT=SST(NTRI)/AMAY1(CCT(NTRI),1,E=100)
BP(NTRI/2)=(BL(NTRI)*TANT)/(1.+BL(NTRI)*TANT)
BR=BL(NTRI)*1)
IF(NTRI,EO,1) BR=0
BP(NTRI/1)=(B*TANT)/(1.-B*TANT)
AP(NTRI/1)=AP(NTRI/2)=0,
IF(NA,LT,1,V1,FR,NB,LT,N2) GO TO 10
RETURN
END

```

CONN 1
CONN 2
CONN 3
CONN 4
CONN 5
CONN 6
CONN 7
CONN 8
CONN 9
CONN 10
CONN 11
CONN 12
CONN 13
CONN 14
CONN 15
CONN 16
CONN 17
CONN 18
CONN 19
CONN 20
CONN 21
CONN 22
CONN 23
CONN 24
CONN 25
CONN 26
CONN 27
CONN 28
CONN 29
CONN 30
CONN 31
CONN 32
CONN 33
CONN 34
CONN 35
CONN 36
CONN 37
CONN 38
CONN 39
CONN 40
CONN 41
CONN 42
CONN 43
CONN 44
CONN 45
CONN 46
CONN 47

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DS CONNECT

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| | ICENT | CONNECT |
|------------------|-------|---------|
| PROGRAM LENGTH | 00414 | |
| ENTRY POINTS | 00003 | CONNECT |
| BLACK NAMES | | |
| PROFILE | 00316 | |
| THIANG | 02261 | |
| EXTERNAL SYMBOLS | | |
| 01C1021J | | |
| 01C0421U | | |
| 085DCY, | | |
| SURT | | |
| MAXIF | | |

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SUBROUTINE PR6FPLOT (RI,N3,INPF) PL0T 1
COMMON /PRCFIL/ RI,N1,Z1(50),V1(50),R2,N2,Z2(50),V2(50),IBOTC,IPFLPLOT 2
DIMENSION X(10),X(4),XP(50),Y(50),PLTARRAY(254),ZDEPTH(250),XRANGPLOT 3
1E (250),XL(50),YL(400),YP(10) PL0T 4
COMMON/INPUT/ RBOT(250),ZBOT(250),ZIL(2,50),VIL(2,50),NN(2),ICON(2PL0T 5
1,50) PL0T 6
COMMON /LIMITS/R0(10),DR(10),R02(10) PL0T 7
COMMON /PR0/ IP00,IKNM,PLTL,RM,IPC0,IFPR PL0T 8
COMMON /TLE/STITLE (10) PL0T 9
COMMON/ABC/PUNCHDB (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1 PL0T 10
DATA (IPLGT=0),(IST=0),(IFT2=0),(IRH=0),(IJ=0) PL0T 11
IF (IPC0.EQ.1.AND.IPL0T.EQ.0,IR,IST,FQ,1) GO TO 100 PL0T 12
IF (IPL0T,EQ,1) GO TO 1 $ CALL PLOTS (PLTARRAY,254,3) PL0T 13
100 IF (IFT1.EQ.IFT2) GO TO 952 SIBH=0 $ IFT2=IFT1 PL0T 14
552 IF (IFT1.EQ.0.AND.IJ.EQ.1,IR,IRH,EQ,1) RETURN PL0T 15
IBH=1 $ IPL0T=1 $ IPC0=1 $ IST=0 $ IJ=1 PL0T 16
RM= MAX1F(R02(1),R02(2),R02(3),R02(4),R02(5),R02(6),R02(7),R02(8),PL0T 17
1R02(9),R02(10)) $ IDI=0 $ K00 PL0T 18
20 K=K+1 $ IF (RM,GT,RBOT(K)) 20.21 PL0T 19
21 ZMAX=ZBOT(1) PL0T 20
22 CG22 J=2,K PL0T 21
22 ZMAX= MAX1F(ZBOT(J),ZMAX) PL0T 22
IF (ZMAX.LE. 250.0,AND,ZMAX.GT. 0.0 ) ZMAX= 250.0 PL0T 23
IF (ZMAX.LE. 500.0,AND,ZMAX.GT. 250.0 ) ZMAX= 500.0 PL0T 24
IF (ZMAX.LE. 1000.0,AND,ZMAX.GT. 500.0 ) ZMAX= 1000.0 PL0T 25
IF (ZMAX.LE. 2000.0,AND,ZMAX.GT.1000.0 ) ZMAX= 2000.0 PL0T 26
IF (ZMAX.LE. 4000.0,AND,ZMAX.GT.2000.0 ) ZMAX= 4000.0 PL0T 27
IF (ZMAX.LE. 5000.0,AND,ZMAX.GT.4000.0 ) ZMAX= 5000.0 PL0T 28
IF (ZMAX.LE.10000.0,AND,ZMAX.GT.5000.0 ) ZMAX=10000.0 PL0T 29
DG 25 J=1,11 PL0T 30
A=(ZMAX/10.0)*(J-1) PL0T 31
IF (J,EQ,6) CALL SYMBOL (-1.00,5.0,0.14,9HDEPTH (H),90,0,9) PL0T 32
XL(J)=0.0 PL0T 33
Y(J)=(11-J) PL0T 34
25 CALL NUMBER(-0.80,Y(J),0.140,A,0,0,4HF5,0) PL0T 35
CALL LINE (XL,Y,11,1,3,0.105,1) PL0T 36
DG 26 J=1,250 PL0T 37
26 YL(J)=0.0 PL0T 38
IF (PLTL.GT.156.0) CALL BYEBYE PL0T 39
RSCALE=PLTL/RM PL0T 40
NTM=AMIN1(PLTL+1.,40.5) PL0T 41
RT=1. PL0T 42
RMAN=RM PL0T 43
IF (IKNM.GT,0) RMAN=RM /1.852 PL0T 44
56 NT=RMAN/RT PL0T 45
IF (NT,LE,NTM) GO TO 57 PL0T 46
RT=2.*RT PL0T 47
NT=RMAN/RT PL0T 48
IF (NT,LE,NTM) GO TO 57 PL0T 49
RT=2.*RT PL0T 50
NT=RMAN/RT PL0T 51
IF (NT,LE,NTM) GO TO 57 PL0T 52
RT=2.*RT PL0T 53
GO TO 56 PL0T 54
C PLOT SURFACE AXIS PL0T 55
57 CALL PLOT(0., 0.,3) PL0T 56

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XN=0,
RSCALE1=RSCALE
IF (IKNM.GT.0) RSCALE1=1.852*RSCALE
DX=RT*RSCALE1
R=0,
IF=0
50 CALL PLOT(XN,0.,2)
CALL PLOT(XN,-0.05,2)
RK=R
CALL NUMBER(XN,-48,-0,19,1,4E-1,RK,0.,4HF4,0)
IF (R.LT.RMAN/2.) GO TO 59
IF (IF,EO,1) GO TO 59
IF (IKNM.EQ.0) 4,7
7 CALL SYMBGL(XN-0.30,-0.40,0,14,10HRANGE (NM),0.,10)
GO TO 8
4 CALL SYMBGL(XN-0.30,-0.40,0,14,10HRANGE (NM),0.,10)
8 CALL SYMBGL (XN-7.20,10,15,0.21,3TITLE,0.,80)
IF=1
59 CALL PLOT(XN,0.,3)
IF (R.GE.RMAN) GO TO 60
XN=XN+DX
R=R+RT
GO TO 58
60 IDP=0
1 IF (IFPR.EQ.1) GO TO 5
X(3)=(R2/1000.0)*RSCALF
IF (INPF.EQ.0) X(3)=PI*RSCALE
X(1)=X(3)*1.5
IF (INPF.EQ.1) GO TO 2   S IF (X(3).GT.PLTL) GO TO 35
DE 15 J=1,N3
15 XP(J)=((0.5*VIL(2,)-735.0)*0.1)*X(3)
IDI=IDI+1
XL(IDI)=X(3)
IF (IDI.GE.2) GO TO 50
CALL SYMBEL (X(1)*0.02,10,27,0,10,16HVELOC!TV (M/SEC),0.0,16)
TX=0.5
50 N=2
DG 55 J=1,N
XT(J)=X(1)*(J-1)*TX
YP(J)=10.02
XM=1500.0
DX=10.0
PL=XM*(J-1)*DX
IF (IDI.EQ.1) CALL NUMBER(XT(J)-0.07,10,10.,105,PL,0.0,4HF4,0)
55 CONTINUE
IF (X(3).LE.PLTL) CALL LINE (XT,YP,N,1,13,0,07,1)
IF (INPF.EQ.1) GO TO 2
DO 3 I=1,N3 SY(I)=10.0*(1.0-(ZIL(2,I)/ZMAX))
3 IF (Y(I).LT.0.0) Y(I)=0.0
IF (X(3).LE.PLTL) CALL LINE (XP,Y,N3,1,-2,0,0,0)
35 INPF=1
GO TO 5
2 DO 6 I=1,N2 SY(I)=10.0*(1.0-(Z2(I)/ZMAX))
6 IF (Y(I).LT.0.0) Y(I)=0.0
IDP=IDP+1
ZDEPTH(IDP)=Y(N2)
XRANGE (IDP)=X(3)
9 IF (IFPR.EQ.0) GO TO 30
CALL LINE (XRANGE,ZDEPTH,IDP,1,1,0,0,0)
CALL LINE (XL, YL,IDI, 1,3,0.140,*1)
CALL PLOTS (0,0)  S CALL PLOT (PLTL*10.0,n,-3)  S IST=1
30 RETURN
END

```

| | |
|------|-----|
| PLOT | 57 |
| PLOT | 58 |
| PLOT | 59 |
| PLOT | 60 |
| PLOT | 61 |
| PLOT | 62 |
| PLOT | 63 |
| PLOT | 64 |
| PLOT | 65 |
| PLOT | 66 |
| PLOT | 67 |
| PLOT | 68 |
| PLOT | 69 |
| PLOT | 70 |
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| PLOT | 72 |
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| PLOT | 100 |
| PLOT | 101 |
| PLOT | 102 |
| PLOT | 103 |
| PLOT | 104 |
| PLOT | 105 |
| PLOT | 106 |
| PLOT | 107 |
| PLOT | 108 |
| PLOT | 109 |
| PLOT | 110 |
| PLOT | 111 |
| PLOT | 112 |
| PLOT | 113 |
| PLOT | 114 |
| PLOT | 115 |
| PLOT | 116 |
| PLOT | 117 |
| PLOT | 118 |
| PLOT | 119 |

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DS PREFPLOT

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| PROGRAM LENGTH | IDENT | PREFPLOT |
|----------------|-------|----------|
| ENTRY POINTS | 03700 | PREFPLOT |
| BLOCK NAMES | 02503 | |

| | |
|---------|-------|
| PROFILE | 00316 |
| INPUT | 01442 |
| LIMITS | 00036 |
| PRO | 00006 |
| TLE | 00012 |
| ABC | 00026 |

EXTERNAL SYMBOLS

Q1Q10100
Q8QDICT,
PLOTS
SYMBOL
NUMBER
LINE
BYEBYE
PLOT
MIN1F
MAX1F

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SUBROUTINE PRBFPLT (RI,NJ,INPF)
COMMON /PRBFIL/ R1,N1,Z1(50),V1(50),R2,N2,Z2(50),V2(50),IBETC,IPPLPL,T
DIMENSION X(4),XP(50),Y(50),PLTARRAY(254),ZDEPTH(250),XRANGPL,T
1E (250),XL(50),YL(400),YP(10),X(100)
COMMON/INPUT/ RB0T(250),ZB0T(250),ZIL(2,50),VIL(2,50),NN(2),ICBN(2PL,T
1,50) PL,T 1
COMMON /LIMITS/R0,10,DR,10,R02,10,PL,T 2
COMMON /PRBF/ IPRF,IKNM,PLTL,RM,IPC0,IFPR PL,T 3
COMMON /TLE/STITLE (10)
COMMON/ABC/PUNCHDB (16),INCR,NSRS,NSRS,ALIM,IFT,IFT1 PL,T 4
DATA (IPL0=0),(IST=0),(IFT2=0),(IBH=0),(IJ=0) PL,T 5
IF (IPC0.EQ.1.AND.IPL0.EQ.0,DR,1,0,1) GO TO 10
IF (IPL0,EQ.1) GO TO 1 $ CALL PLOTS (PLTARRAY,254,3) PL,T 6
100 IF (IFT1.EQ,IFT2) GO TM 952 $ IBH=0 $ IFT2=IFT1 PL,T 7
152 IF (IFT1.EQ.0.AND.IJ.EQ.1,DR,IBH,EQ.1) RETURN PL,T 8
IBH=1 $ IPL0=1 $ IPC0=1 $ IST=0 $ IJ=1 PL,T 9
RM= MAX1F(R02(1),R02(2),R02(3),R02(4),R02(5),R02(6),R02(7),R02(8),PLT,T
1R02(9),R02(10)) $ K=0 $ IDI=0 $ ITL=0 PL,T 10
20 K=K+1 PL,T 11
IF (RM.GT,RB0T(K)) 20,21 PL,T 12
21 ZMAX=ZB0T(1) PL,T 13
D022 J=2,K PL,T 14
22 ZMAX= MAX1F(ZB0T(J),ZMAX) PL,T 15
IF (ZMAX.LE. 250.0,AND,ZMAX.GT. 0.0 ) ZMAX= 250.0 PL,T 16
IF (ZMAX.LE. 500.0,AND,ZMAX.GT. 250.0 ) ZMAX= 500.0 PL,T 17
IF (ZMAX.LE. 1000.0,AND,ZMAX.GT. 500.0 ) ZMAX= 1000.0 PL,T 18
IF (ZMAX.LE. 2000.0,AND,ZMAX.GT. 1000.0 ) ZMAX= 2000.0 PL,T 19
IF (ZMAX.LE. 4000.0,AND,ZMAX.GT.2000.0 ) ZMAX= 4000.0 PL,T 20
IF (ZMAX.LE. 5000.0,AND,ZMAX.GT.4000.0 ) ZMAX= 5000.0 PL,T 21
IF (ZMAX.LE.10000.0,AND,ZMAX.GT.5000.0 ) ZMAX=10000.0 PL,T 22
D0 25 J=1,11SA=(ZMAX/10,0)*(J-1) PL,T 23
IF (J.EQ.6) CALL SYMBOL (-1,40,5,0,0,14,9HDEPTH (M),90,0,9) PL,T 24
Y(J)=(11-1) $ XL(J)=0,4 PL,T 25
25 CALL NUMBER(-1,20,Y(J),0,140,A,0,0,0,4HF5,0) PL,T 26
CALL LINE (XL,Y,11,1,3,0,105,1) $ RSCALE=PLTL/RM $ RJBPM=RSCALE PL,T 27
IF (PLTL.GT.,5A,0) CALL BYEBYE $ D0 26 J=1,250 PL,T 28
26 YL(J)=0.0525 $ IDP=0 PL,T 29
CALC SYMBOL (1,02,10,20,0,10,16HVELOCITY (M/SEC),0,0,16) PL,T 30
1 IF (IFPR.EQ.1) GO TO 5 $ X(3)=(R2/1000,0)*RSCALE PL,T 31
X(1)=X(3)+0,0 $ X(2)=0.94 PL,T 32
X(4)=R2/1000,0 PL,T 33
IF (IKNM.GT.0) X(4)=X(4)/1,852 PL,T 34
IF (INPF.EQ.0) GO TO 60 PL,T 35
D0 15 J=1,N2 PL,T 36
15 XP(J)=V2(J) PL,T 37
CALL SCALE (XP,N2,1,0,XM,Dx,1,TX) PL,T 38
D0 30 J=1,N2 PL,T 39
30 XP(J)=XP(J)+X(1) PL,T 40
50 N=1,0/TX=0.50 PL,T 41
N=N+1 PL,T 42
D0 55 J=1,N PL,T 43
XT(J)=X(1)+(J-1)*TX PL,T 44
YP(J)=10.02 PL,T 45
PL=XM*(J-1)*DX PL,T 46
IF (PL.GE.1600.0.AND.PL.LE.1650.0) PL=PL-1600.0 PL,T 47
IF (PL.GE.1500.0.AND.PL.LE.1600.0) PL=PL-1500.0 PL,T 48

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      IF (PL,GE,1400.0,AND,PL,LE,1500.0) PL=PL-1400.0          PLIT  57
 55 CALL NMBEN (XT(J)=0.07,10,10,0,07,PL,0,0,4HF2.0)          PLIT  58
 CALL LINE (XT,YP,N,1,13,0,07,1)                                PLIT  59
 IF (INPF,EO,1) GO TO 2                                      PLIT  60
 60 INPF=1
 IDI=IDI+1
 XI(IDI)=X(3)
 IF (X(3),GE,RJ/4.0,AND,ITL,EO,0) 35,5                  PLIT  61
 35 ITL=1
 IF (IKNM,EO,0) CALL SYMBOL (RJ/2.0=0.6,-0.40,0.14,10HRANGE (KM),0,PLIT  66
 10,10)                                              PLIT  67
 IF (IKNM,GT,0) CALL SYMBOL (RJ/2.0=0.6,-0.40,0.14,10HRANGE (NM),0,PLIT  68
 10,10)                                              PLIT  69
 CALL SYMBOL (RJ/2.0=4.0,10.20,0.14,STITLE,0.0,0)          PLIT  70
 GO TO 5                                      PLIT  71
 2 DO 6 I=1,N2
 Y(I)=10.0*(1.0-(Z2(I)/ZMAX))  S IF(Y(I),LT,0.0) Y(I)=0.0    PLIT  72
 XL(I)=X(3)
 6 CALL NUMBER (X(2)*X(1),Y(I),0,07,Z2(I),0.0,4HF4.0)          PLIT  73
 CALL LINE (XL,Y,N2,1,3,0,07,1)                                PLIT  74
 CALL LINE (XP,Y,N2,1,1,0,07,1)                                PLIT  75
 CALL NUMBER (X(3)*0.30,-0.25,0.105,X(4),0.0,4HF4.0)          PLIT  76
 IDP=IDP+1
 ZDEPTH(IDP)=Y(N2)
 XRANGE (IDP)=X(3)
 IF (X(3),GE,RJ/4.0,AND,ITL,EO,0) 45,5                  PLIT  77
 45 ITL=1
 IF (IKNM,EO,0) CALL SYMBOL (RJ/2.0=0.6,-0.40,0.14,10HRANGE (KM),0,PLIT  78
 10,10)                                              PLIT  79
 IF (IKNM,GT,0) CALL SYMBOL (RJ/2.0=0.6,-0.40,0.14,10HRANGE (NM),0,PLIT  80
 10,10)                                              PLIT  81
 CALL SYMBOL (RJ/2.0=0.6,10.20,0.14,STITLE,0.0,48)          PLIT  82
 5 IF (IPR,EO,0) GO TO 130
 CALL LINE (XRANGE,ZDEPTH,IDP,1,1,0,0,0)          PLIT  83
 CALL LINE (XRANGE,YL,IDP,1,3,0,105,1)          PLIT  84
 CALL LINE (X,YL,IDI,1,3,0,2,1)          PLIT  85
 CALL PLOTS (0,0)  S CALL PLOT (PLTL=10.0,0,0,-3)  S IST=1    PLIT  86
 130 RETURN
 END

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S PROFPLIT

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ED 0

| | IDENT | PROFPLIT |
|------------------|-------|----------|
| PROGRAM LENGTH | 03745 | |
| ENTRY POINT'S | 02654 | PROFPLIT |
| BLOCK NAMES | | |
| PROFIL | 0^316 | |
| INPUT | 01442 | |
| LIMITS | 00036 | |
| PRO | 00006 | |
| TLE | 00012 | |
| ABC | 00026 | |
| EXTERNAL SYMBOLS | | |
| Q1710100 | | |
| RECDICT, | | |
| PLOTS | | |
| SYMBOL | | |
| NUMBER | | |
| LINE | | |
| BYEBYE | | |
| SCALE | | |
| PLOT | | |
| MAX1F | | |

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SUBROUTINE ADVANCE          ADVA0000
COMMON /THIANG/ AP(100,2),BP(100,2),AL(100),RL(100),ZZERO(100),    ADVA0001
1  HZERO(100),AA(100),EB(100),SST'100),CCT(100),NTRI           ADVA0002
COMMON /RAYS/ NRAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),      ADVA0003
1  NCOUNT(1000),PHASE(1000)                                     ADVA0004
COMMON /INFO/ RSTART,RMAX,EMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,    ADVA0005
1  ISCP,IT1,IT2,IT3,IPEH,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT       ADVA0006
COMMON /PIDEF/ PI,ETA,TWEP1                                     ADVA0007
COMMON /MIRRORS/ SL,BRLT(200),BPSL(200)                         ADVA0008
COMMON /ARC/PUNCHDB(16),INCR,NBRS,NSRS,ALIM,IFT,IFT1            ADVA0009
DIMENSION RPNEW(4),RAEK(1),ZAEK(4),ZPNEW(4)
LOGICAL BNUP,GNLW
TANSUM(A,B)=(A+B)/(1,-A*B)
CELT(Y,R,T,S)=ABS(YR)*SCHT(CH(S)*(1,(T+(T+S)*S*S)/3,)

C   LOOP OVER ALL THE RAYS
DO 100 IRAY=1,NRAY  S IHOST=0  * SSR=SS(IRAY)
IF (NBRS,EQ,2500,AND,NSHS,EQ,2500) GO TO 10
NN=NCOUNT(IRAY)  SM=NN/ITN  SNR=M>NN/ITN  SH=NN/ITN  SNBR=MADV0017
10 IF (ABS(SSH),LT,ALIM,ER,NHR,GT,NBRS,UR,NSR,GT,NSRS) GO TO 100
ZR=ZZ(IRAY)  S HR=RSTART
TGR=TGAM(IRAY)
TRAY=TIME(IRAY)
-R=PHASE(IRAY)
NCTR=NCOUNT(IRAY)
DE 20 I=1,NTRI
      FIND CORRECT LAYER
P=ZR=AL(I)-BL(I)*HR
IF (P,,0001,GT,0,) GO TO 20
NTRR=I
IF (ABS(P),GT,,0001,GR,TGR,GT,-BL(I)) GO TO 30
CONTINUE
GO TO 80
30 CT=CCT(NTRR)
IF (IPRAY,NE,0) PRINT 666,IRAY,NTRR,ZR,RR,TGR,NCTR
ST=SST(NTRR)
ZR=ZZERO(NTRR)
C   TRANSFORM TO PRIMED COORDINATES
R0=HZERO(NTRR)
ZRP=CT*(ZR-Z0)+ST*(RR-R0)
RRP=CT*(RR-R0)+ST*(ZR-Z0)
CIS=AA(NTRR)+BB(NTRR)*ZRP
TANT=ST/AMAX1(CT,1,E-300)
TGRP=TANSUM(TANT,-TGR)
CMIS=CIS/(1,-TGRP*2)
C   CALCULATE PARABOLIC RAY PATH, ALPHA IS THE CURVATURE
ALPHA=250BB(NTRR)/CMIS
TA=2,*ALPHA
C   FIND INTERSECTIONS WITH UPPER AND LOWER LAYER BOUNDARIES
DE 40 I=1,2
APNTR=AP(NTRR,I)
BNPTR=BP(NTRR,I)
C=APNTR+BNPTR*RRP-ZRP
P=BNPTR-TGRP
IF (ABS(ALPHA),GT,1,E-25) GO TO 303
      RAY PATH IS LINEAR FOR THESE STATEMENTS
CMIS=C/M
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ADVA0049
ADVA0050
ADVA0051
ADVA0052
ADVA0053
ADVA0054
ADVA0055

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K2=1
RPNEW(K)=RRP+CRP
ZPNEW(K)=ZRP+TGRP+CRP
ZNEW(K)=CT*ZPNEW(K)+ST*RPNEW(K)+Z0
RNEW(K)=CT*RPNEW(K)+ST*ZPNEW(K)+R0
ZNEW(K+1)=1,E300
ZPNEW(K+1)=1,E300
RNEW(K+1)=1,F300
RPNEW(K+1)=1,E300
G6 TO 40
C      SOLVE QUADRATIC EQUATION FOR PARABULIC RAY PATH
303  DISC=P*P+4.*ALPHA*C
      IF(DISC<LT,0,) GO TO 32
      DISC=SQRT(DISC)
      D6 31 J=1,2
      K2=1+J*2
      S=2+J*3
      F=P*S*DISC
      DRP=F/TA
      C      ITERATION TO IMPROVE ACCURACY FOR SMALL CURVATURE RAYS
      IF(ABS(F),LT,,1=ABS(F)) CRP=(ALPHA*((ALPHA*DHP**2-C)/P)**2-C)/P
      RPNEW(K)=ZRP+CRP
      ZPNEW(K)=ZRP+CRP*(TGRP+ALPHA*CRP)
      ZNEW(K)=CT*ZPNEW(K)+ST*RPNEW(K)+Z0
      RNEW(K)=CT*RPNEW(K)+ST*ZPNEW(K)+R0
      G6 TO 40
      32  D6 33 J=1,2
      K2=1+J*2
      33  RNEW(K)=1,E300
      40  CONTINUE
      ENLW=ABS(ZR=AL(NTRR)=BL(NTRR)*RR),LT,,01,AND,TGR,GT,=BL(NTRR)
      C      SELECT CORRECT INTERSECTION AS NEXT POSITION
      IF(NTRR,LT,0) GO TO 405
      ENUP=ABS(AL(NTRR+1)+EL(NTRR+1)*RR-ZH),LT,,01
      1  AND1 TGR,LT,=BL(NTRR+1)
      GE 41
      405  ENUP=ABS(ZR),LT,,01,AND,TGR,LT,0,
      41  ILP=IDN=3
      IF(,NLT,0NUP) GO TO 411
      ILP=1
      IF(ABS(MR=RNEW(1)),LT,ABS(RR=RNEW(2))) ILP=2
      IF(RNEW(ILP),LT,RR,OR,RNEW(ILP),GT,RMAX) ILP=0
      411  IF(,NLT,0NLU) GO TO 412
      IDN=3
      IF(ABS(MR=RNEW(3)),LT,ABS(RR=RNEW(4))) IDN=4
      IF(RNEW(IDN),LT,RR,OR,RNEW(IDN),GT,RMAX) IDN=0
      412  IF(ILP,UE,0) GO TO 414
      ILP=0
      RTRY=RMAX
      GE 413 1=3/2
      IF(RNEW(1),LT,RR,UE,RNEW(1),GT,RTRY) GO TO 413
      RTRY=RNEW(1)
      ILP=1
      413  CONTINUE
      IF(IDN,UE,0) GO TO 416
      IDN=0
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      ADVAB110
      ADVAB111

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RTHY=RMAX
415  I=314
IF(RHNEW[],LT,RH,RR,RNEW[],GT,RTRY) GE TO 415
IDN=I
RTHY=RNEW[]
415  CONTINUE
416  IF([DN,EQ,0) GE TO 420
IF([UP,NE,0) GE TO 418
417  ITRY=IDN
RTHY=RNEW([DN])
GE TO 429
418  IF(RHNEW[UP],GE,RHNEW[DN]) GE TO 427
419  ITRY=JUP
RTRY=RNEW(JUP)
GE TO 429
420  IF([UP,EQ,0) GE TO 50
GE TO 419
429  TGRPN=TAO*(RPAEW(ITRY)-RHP)+TGRP
THAY=THAY+DELT(RPAEW([ITRY])-RHP,TGRP,TGRPN)
TGRV=TANSUM(TGRPN,+TANT)
RH=THY
Z=ZNEW([ITRY]
C      CHECK FOR SURFACE AND BOTTOM HITS, TURNOVERS AND TURNUNDERS
IF(TGR>1.0,GE,0,) GE TO 44
IF(TGR,GT,1,) GO TO 43
NTHR=NTHR+1
43  NTHR=NTHR+1
IF([ITRY,GT,2) GO TO 45
NTHR=NTHR+1
IF(NTHR,GT,0) GO TO 46
NTHR=1
SSRSSH=SL
PHR=PHR+P
NTHR=NTHR+1
'GR=0TGZN
GE TO 30
45  NTHR=NTHR+1
IF(NTHR,LE,NTHR) GE TO 46
NTHR=NTHR+1
NTHR=NTHR+1
TGRZE=TANSUM(TGRN,BL([NTR]))+
S=100,*ABS(TGRZE)+1,
NS
SSON
IF(N,GT,199) N=199
SSRSSH=((1,-S)*RMLT(N)+S*RALT(N+1))
PHR=PHR+((1,-S)*RPSL(N)+S*RPST(N+1))
TGRB=TANSUM(TGRAZE,BL([NTR]))+
IF(TGR,LT,1.0L(NTHR)) 80,30
46  TGRB=TGRN
GE TO 30
C      CALCULATE MAX INTERSECTION WITH VERTICAL BOUNDARY, RURMAX
50  IF(ABS(ST),LT,2,E=4) GF TO 60
BV=CT/ST
AV=(RMAX+R0)/ST
ADVA0112
ADVA0113
ADVA0114
ADVA0115
ADVA0116
ADVA0117
ADVA0118
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ADVA0120
ADVA0121
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ADVA0123
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ADVA0167

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| | | |
|-----|---|----------|
| | PSAV=RRP=RVR=ZRP | ADVA0168 |
| | PSH=RTGMP | ADVA0169 |
| C | IF(ABS(ALPHA),GT,1,E-25) GO TO 501 | ADVA0170 |
| | LINERAY RAYS | ADVA0171 |
| C | RPNEW(1)=RRP+C/P | ADVA0172 |
| | RPNEW(2)=1,E100 | ADVA0173 |
| | GO TO 505 | ADVA0174 |
| C | PARABOLIC RAYS | ADVA0175 |
| 501 | TISC=P=0.4,ALPHAC=0 | ADVA0176 |
| | IF(DISC,LT,0,) GO TO 80 | ADVA0177 |
| | TISC=SQR(TDISC) | ADVA0178 |
| | S=1, | ADVA0179 |
| | TE 503 I=1,2 | ADVA0180 |
| | FEP+S=TDISC | ADVA0181 |
| | DRP=F/TA | ADVA0182 |
| | IF(ABS(F),LT,,1=ABS(F)) DRP=(ALPHA=((ALPHA+DRP**2+C)/P)**2+C)/P | ADVA0183 |
| | RPNEW(1)=RRP+DRP | ADVA0184 |
| 503 | S=5 | ADVA0185 |
| 505 | TE > 1 I=1,2 | ADVA0186 |
| | ZHNEW(1)=ZRP+(RPNEW(1)-RRP)*(TGRP+ALPHA*(RPNEW(1)-RRP)) | ADVA0187 |
| 51 | ZNEW(1)=CT*ZPNEW(1)+ST*HPNEW(1)*ZD | ADVA0188 |
| | I=2 | ADVA0189 |
| C | SELECT CORRECT INTERSECTION | ADVA0190 |
| | IF(ZRS(ZNEW(1)-ZR),LT,ABS(ZNEW(2)-ZR)) I=1 | ADVA0191 |
| | TGRP=ST*(RPNEW(1)-RRP)+TGRP | ADVA0192 |
| | TRAY=TRAY+DEL(TPNEW(1)-RRP,TGRP,TGRPN) | ADVA0193 |
| | TGRN=STANSUM(TGRPN,=TART) | ADVA0194 |
| C | CHECK FOR TURNOVERS AND TURNUNDERS | ADVA0195 |
| 52 | IF(TGH>IGHY,GE,0,) GO TO 54 | ADVA0196 |
| | IF(TGR,LT,0,) GO TO 53 | ADVA0197 |
| | NCTR=NCTR+1 | ADVA0198 |
| | GO TO 54 | ADVA0199 |
| 53 | NCTR=NCTR+1 | ADVA0200 |
| 54 | TGAM([RAY])=TGRN | ADVA0201 |
| | IF(NTRH,LE,1) GO TO 545 | ADVA0202 |
| C | CHECK THAT RAY IS WITHIN THE PROPER LIMITS | ADVA0203 |
| | IF(ZNEW(1),LT,AL(NTRH-1)+BL(NTRR+1)*RMAX+,1) ,0 TO 80 | ADVA0204 |
| 545 | IF(ZNEW(1),GT,AL(NTRH)+HI(NTRH)*RMAX+,1) GO TO 80 | ADVA0205 |
| C | THROA IN VOLUME ATTENUATION | ADVA0206 |
| | IF(IATT1,E,0)SSR=SSR+10,0001*ATT*(TRAY*TIME([RAY])/SQRT(CIS)) | ADVA0207 |
| 55 | SS([RAY])=SSR | ADVA0208 |
| | ZZ([RAY])=ZNEW(1) | ADVA0209 |
| | TIME([RAY])=TRAY | ADVA0210 |
| | NCOUNT([RAY])=NCTR | ADVA0211 |
| | PHASE([RAY])=PHR | ADVA0212 |
| | GO TO 100 | ADVA0213 |
| 60 | I=I+1 | ADVA0214 |
| C | WHEN SMALL OR ZERO HORIZONTAL GRADIENTS, EQUATION FOR SECTION | ADVA0215 |
| C | 50 IS SINGULAR, THIS IS AN ITERATIVE SOLUTION FOR SUCH A CASE | ADVA0216 |
| C | GUESS VALUE FOR ITERATION | ADVA0217 |
| | ZNEW=ZH+(RMAX+RH) | ADVA0218 |
| 66 | DRP=CT*(RMAX-R0)+ST*(ZNEW-ZD) | ADVA0219 |
| | DRP=DRP,=RRP | ADVA0220 |
| | TGRPAV=TRAY+ALPHA*DRP | ADVA0221 |
| | ZRP=DRP*TGRPAV | ADVA0222 |
| | | ADVA0223 |

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ZPNH=ZRR=DZP          ADVA0224
ZRW2=CT=ZPNH=ST=RPA=ZD  ADVA0225
D=A8S(ZNW2=ZRN)        ADVA0226
IF(I,EQ,3) DD=0        ADVA0227
ZRN=ZRW2               ADVA0228
47
      CHECK FOR CONVERGENCE   ADVA0229
      IF(D,L,T1,01) GE TG 6E  ADVA0230
      IF(D,L,1,0000) GE TG 6E  ADVA0231
      IHIST=0,3            ADVA0232
      GE TG 80               ADVA0233
      RPNEW(1)=RPNEW(2)=RPAW  ADVA0234
      GE TG 505              ADVA0235
C      PRINT ERROR MESSAGE  ADVA0236
80      SJR=0,
      PRINT 81,IRAY,IHIST,RR,ZR,TGR  ADVA0237
      PRINT 82,RMAX,ZNEW(1),TGRA  ADVA0238
      666  FFORMAT(*RAY*,15,* I A LAYER*,15,* Z** ,F10,2,* R**,F10,2,* TGR** ,FADVA0240
      1 10,5,* NCTR*,0,G16)          ADVA0241
      81  FFORMAT(* RAY *,15,* TERMINATED*,5X,*IHIST*,12,5X,*STARTING RANGE*ADVA0242
      10,F12,2,5X,*RAY DEPTH*,F12,2,5X,*STARTING TANGENT*,F12,6)          ADVA0243
      82  FFORMAT(5X,*MAXIMUM RANGE**,F12,2,5X,*NEW RAY DEPTH*,F10,2,5X,*FINADVAD244
      1AL TANGENT*,F12,6)          ADVA0245
      GE TG 59               ADVA0246
100    CONTINUE             ADVA0247
      RETURN                ADVA0248
      END                  ADVA0249

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IDENT ADVANCE

PROGRAM LENGTH 01720
ENTRY POINTS ADVANCE 00125
BLOCK NAMES

TRIANG 02261
RAYS 13961
INFE 00024
PIDEF 00003
MIRRORS 00621
ABC 00026

EXTERNAL SYMBOLS

THEAD,
QJC10140
QJC00040
Q1C10100
Q1C03100
Q2C07111
Q82DICT,
SORTF
MAX1F
STH,
ONSINGL,

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SUBROUTINE CHANNEL(ZR,T,ZTG,ZTU)
COMMON /VBLPRF/ N,Z(100),C(100)
CALL VBLCALC
20  DO 29 1B2,N
      IF(ZR,GT,Z(I)) GO TO 29
      1B2|
      F=(ZR-Z(I))/Z(I)*Z(I+1)
      CM=SQRT(1.+T*T)*(F+C(I)*(1.+F)*C(I+1))
      GO TO 30
29  CONTINUE
      ZTU$Z$=3.
      RETURN
30  IN=1
31  IF(C(IN),GT,CM) GO TO 39
      IN=N+1
      IF(IN,NE,0) GO TO 31
      ZT000,
      GO TO 4U
35  F=(CM+C(N+1))/(C(IN)+C(N+1))
      ZT0SF=Z(N)*(1.+F)*Z(N+1)
40  IN=1Z
41  IF(C(IN),GT,CM) GO TO 45
      IN=N+1
      IF(IN,LE,N) GO TO 41
      ZTUBZ(N)
      RETURN
45  F=(CM+C(N+1))/(C(IN)+C(N+1))
      ZTUSF=Z(N)*(1.+F)*Z(N+1)
      RETURN
      ENTRY RUCALC
      IF(ZTG,GT,.5) GO TO 50
      RCYCLE=.3,E3)
      RETURN
50  IN=1
      RCYCLE$BU,
      TG2$0,
      DO 60 1B1,N
      IF(Z(I),GT,ZTG,A'U,Z(I),LT,ZTU) GO TO 55
      IF(IN,EU,1) GO TO 50
      RCYCLE$HCYCLE=(ZTU-Z(I+1))/(.5+TG1)
      RETURN
55  TG1$QR=((CM/C(I))+2-1)
      IF(.5,Q1,1) GO TO 59
      IF(IN,EU,1) GO TO 56
      DR=(Z(I)-Z(I+1))/(.5+(TG1+TG2))
      GO TO 57
56  DR=(Z(I)-ZTG)/(.5+TG1)
57  RCYCLE$HCYCLE=DR
59  TG2$TG1
      IN=2
60  CONTINUE
      RETURN
      ENTRY WUENS
      IF(RCYCLE,GT,1,E100) GO TO 73
      IN=1Z
      IF(Z(IN),GT,ZR) GO TO 70

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CHAN0055

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IF(Z(|N=1|),GT,ZR) GO TO 75  
IN=|N=1  
IF(|N,GE,N) GO TO 71  
GO TO 69  
70 IF(Z(|N=1|),LE,ZR) GO TO 74  
IN=|N=1  
IF(|N,GE,1) GO TO 69  
71 T=0  
RETURN  
74 IN=|N=1  
V=C(|N)*(C(|N+1|-C(|N)))*(ZR-Z(|N))/(Z(|N+1|-Z(|N))  
T=1/(SURT((CH/V)**2+1,)*RCYCLE)  
RETURN  
END
```

CHAN0056
CHAN0057
CHAN0058
CHAN0059
CHAN0060
CHAN0061
CHAN0062
CHAN0063
CHAN0064
CHAN0065
CHAN0066
CHAN0067
CHAN0068
CHAN0069

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S CHANNEL

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ED 0

| | IDENT | CHANNEL |
|------------------|-------|---------|
| PROGRAM LENGTH | 00506 | |
| ENTRY POINTS | 00003 | |
| CHANNEL | | |
| RCALC | 00151 | |
| WDENS | 00257 | |
| BLOCK NAMES | | |
| VELPRF | 00311 | |
| EXTERNAL SYMBOLS | | |
| OBJDCT, | | |
| VELCALC | | |
| SQRTF | | |

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| | | |
|--|------|----|
| SLROUTINE VELCALC | VELC | 1 |
| CMMON /INFO/ DDDDC, RMAX, DCDCDD(18) | VELC | 2 |
| CMMGR /VELPRF/ N, Z(100), C(100) | VELC | 3 |
| CMMON /THIANG/ AP(100,2), BP(100,2), AL(100), BL(100), ZZER0(100), | VELC | 4 |
| 1 RZERO(100), AA(100), RW(100), SST(100), CCT(100), NTR | VELC | 5 |
| CMMON/ABC/PLNCHD8 (16), INCR, NBRS, NSRS, ALIM, IFT, IFT1 | VELC | 6 |
| DATA (RULUP=1,E300),(IFT2=0),(IBH=0) | VELC | 7 |
| IF (IFT1,EO,IFT2) GO TO 13 | VELC | 8 |
| IBH=0 | VELC | 9 |
| IFT2=IFT1 | VELC | 10 |
| 13 IF (IFT1,EO,0,ER,IBH,EC,1) GO TO 3 | VELC | 11 |
| RELD=41, E300 | VELC | 12 |
| IBH=1 | VELC | 13 |
| 3 IF (ABS(RMAX-RELD),LT,1,) GO TO 20 | VELC | 14 |
| RELD=RMAX | VELC | 15 |
| N=NTR+1 | VELC | 16 |
| DE 10 :41,N | VELC | 17 |
| IF (1,EO,1) GO TO 1 | VELC | 18 |
| J=1+1 | VELC | 19 |
| ZZ=AL(J)+BL(J)+RMAX | VELC | 20 |
| GO TO 2 | VELC | 21 |
| 1 J=1 | VELC | 22 |
| 2 ZZ=0, | VELC | 23 |
| ZP=CCT(J)*(ZZ-ZZEHE(J))+SST(J)*(RMAX-RZERO(J)) | VELC | 24 |
| C(J)=1./SURT(AA(J)+BB(J)+ZP) | VELC | 25 |
| 10 Z(J)=ZZ | VELC | 26 |
| 20 RE=LBN | VELC | 27 |
| END | VELC | 28 |

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DS VELCALC

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ED 0

| | IDENT | VELCALC |
|------------------|-------|---------|
| PROGRAM LENGTH | 00132 | |
| ENTRY POINTS | 00006 | VELCALC |
| BLOCK NAMES | | |
| INFO | 00024 | |
| VELPRF | 00311 | |
| TRIANG | 02261 | |
| ABC | 00026 | |
| EXTERNAL SYMBOLS | | |
| GCDICT, | | |
| SQRTF | | |

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SUBROUTINE INTENSTY

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C JUNE 14, 1971 LLOYD'S MIRROR ADDED FOR ALL RECEIVERS AND TYPES      INTE  1
C UNUSED SWITCH IFIMS IS NOW LLMR, 0 FOR NO LLOYD'S MIRROR, AND      INTE  3
C NON-ZERO FOR LLOYD'S MIRROR. THIS SWITCH IS THE COLUMN AFTER      INTE  4
C IPER ON THE INPUT CARDS      INTE  5
C 6/15/71 RECEIVERS BELOW BOTTOM FIXED      INTE  6
COMMON /LOUDNESS/ LNRC,RCD(100),TYPEIIS(100),TYPEIRP(100),      INTE  7
1 TYPEIII(100),TYPEIIP(100)      INTE  8
COMMON /TITLE/ STITLE (1B)      INTE  9
COMMON /RAYS/ NRAY,IGAM(1000),ZZ(1000),SS(1000),TIME(1000)*      INTE 10
1 NCOUNT(1000),PHASE(1000)      INTE 11
COMMON /INFO/ RSTART,BMAX,OMEGA,ATT,IPLY,ITN1,ITN2,ITN3,IBIG,      INTE 12
1 ISCP,IT1,IT2,IT3,IPER,LLMK,LTRT,LTER,LTRP,LIN,ITATT      INTE 13
COMMON /PIDEF/ PI,DTR,TWOP1      INTE 14
COMMON /VELPRF/ MN,Z(100),C(100)      INTE 15
COMMON /TMPSTR/ DUD(102)      INTE 16
DIMENSION QUAD(100),IMP(100),SINT(100,4),SSL(100),QUS(100),TPS(100)      INTE 17
10)
EQUIVALENCE (QUAD,DDD)      INTE 18
COMMON /ABC/PUNCHDU(410)=INCR,NBRS,NSPS,ALIM,IFT,IFT1      INTE 19
DATA (IENT=0),IFT2=0,(IBH=0),(IMH=100,0)      INTE 20
SEC(T)=FVA(SORT(1..T))      INTE 21
IF (IFT1.EQ.0,IFT2) GO TO 2 S IBH=0 S IFT2=IFT1      INTE 22
2 IF (IFT1.EQ.0.OR.IBH.EQ.1) GO TO 3 S IENT=0 S IBH=1      INTE 23
3 FVA=1.
IF (IATT.EQ.0.AND.ATT.NE.0.) FVA=10.**(-.0001*ATT*RMAX)      INTE 24
CALL VELCALC SWAVEL,TWOP1=C(1)/OMEGA SAK=TWOP1/WAVEL  S PLM=1.      INTE 25
DO 5 I=1,LNRC      INTE 26
5 TYPEIS(1)=TYPEIP(1)=TYPEII(1)=TYPEIII(1)=QUAD(1)=0.
IF (IT1.EQ.0.AND.IT2.EQ.0) GO TO 60      INTE 27
SW=0      INTE 28
SDZ=0.      INTE 29
DO 10 I=2,NRAY      INTE 30
W=AMINI(SS(I),SS(I-1))      INTE 31
SDZ=SDZ+W*ABS(ZZ(I)-ZZ(I-1))      INTE 32
10 SW=SW+1      INTE 33
DZBAR=SDZ/SW      INTE 34
IF (DZBAR.LT.WAVEL) DZBAR=WAVEL      INTE 35
CALL CHANNEL(1..1000,ZZ,ZB)      INTE 36
DZM=ZB/SQRT(FLOAT(NRAY))      INTE 37
IF (DZBAR.GT.DZM) DZBAH=DZM      INTE 38
IF (IT1.EQ.0) GO TO 25      INTE 39
DO 20 I=1,NRAY      INTE 40
N=NCOUNT(I)      INTE 41
M=N/ITV      INTE 42
NT0=N-4*ITN      INTE 43
NM=M/ITV      INTE 44
NSR=M-V*ITN      INTE 45
MB=M/ITV      INTE 46
NTU=N-4*ITN      INTE 47
NBR=M      INTE 48
IF (I.EQ.1) GO TO 19      INTE 49
NTU0=IABS(NT0-NT00)+IABS(NTU-NTU0)      INTE 50
NDSBR=IABS(NSR-NSR0)+IABS(NBR-NBR0)      INTE 51
ID=NDSBR      INTE 52
ID=ID+NTU0      INTE 53
19

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IF(IU.GT.3) ID=3          INTE 57
W=AMIN1(SS(I),SS(I-1))  INTE 58
IF(W.LE.ALIM.OR.NBR.GT.NBRS.OH.NSR.GT.NSRS) ID=3  INTE 59
NCOUNT(I)=NCOUNT(I)+IU*IRIG  INTE 60
19 NSRO=NSR  INTE 61
NBR0=NBR  INTE 62
NTU0=NTU  INTE 63
NTO0=NTO  INTE 64
CONTINUE  S DO 21 I=1,LNRC  INTE 65
SSL(I)=0.0  INTE 66
QUR(I)=0.0  INTE 67
20 TYP5(I)=0.0  INTE 68
IMH(I)=0  S IPR=0  INTE 69
INW=NCOUNT(2)/IBIG  INTE 70
DC 30 I=2,NRAY  INTE 71
NCOUNT(I)=NCOUNT(I)+INW*IBIG  INTE 72
INXT=NCOUNT(I+1)/IBIG  S IF(I+2.LE.NRAY) INXTT=NCOUNT(I+2)/IBIG  INTE 73
IF(INW.GE.2) GO TO 29  INTE 74
IQ1=0  S IQ2=0  S IQ3=0  INTE 75
Z1=ZZ(I-1)  INTE 76
S1=SEC(TGAM(I-1))*SS(I-1)  INTE 77
DS=SEC(TGAM(I))*SS(I)-S1  INTE 78
T1=TIME(I-1)  INTE 79
DT=TIME(I)-T1  INTE 80
TG1=TGAM(I-1)  INTE 81
UTG=TGAM(I)-TG1  INTE 82
DZ=ZZ(I)-Z1  S DO 25 J=1,LNRC  S IQ1=0  S IQ2=0  S IQ3=0  INTE 83
ZR=RCD(J)  S IF(ZR.GT.38) GO TO 25  INTE 84
F=(ZR-Z1)/DZ  S DZ1=Z1(I+1)-Z1(I)  S F1=(ZR-ZZ(I))/DZ1  INTE 85
IF(F.LT.-0.5.OR.F.GT.3.5) GO TO 25  INTE 86
IF(INW.EQ.0.AND.F.LE.-1.0.AND.F.GE.0..AND.IHP(J).EQ.0) 23,24  INTE 87
23 IQ1=1  INTE 88
GO TO 26  INTE 89
24 IF(F.GT.1.0.AND.INW.EQ.0 .AND.INXT.NE.INW.AND.IHP(J).EQ.0) 31,32  INTE 90
31 IQ2=1  INTE 91
GO TO 26  INTE 92
32 IF(F.LT.0.0.AND.IPR.NE.INW.AND.INW.EQ.0) 33,34  INTE 93
33 IQ3=1  INTE 94
GO TO 26  INTE 95
34 IU1=0 $IQ2=0 $IQ3=0  INTE 96
GO TO 25  INTE 97
26 SL=(S1*F*DS)/(RMAX*ABS(DZ))  INTE 98
IF(SL.LE.0.0) GO TO 499  S IF(ABSF(DZ).LT.0.001) GO TO 25  INTE 99
TG=TG1,F=DTG  S IF(IQ1.EQ.1) IHP(J)=1  INTE 100
TH=OTR*ATANF(TG)  S IF(INW.GE.1.AND.INXT.GE.1) GO TO 25  INTE 101
IF(LLMR.NE.0) FLM=2.0*SIN(ZR*AK*TG/SQRT(1.+TG**2))**.  INTE 102
T=T1*F*DT  INTE 103
IF(IQ1.EQ.1.AND.SINT(J,1).EQ.0.0) SINT(J,4)=FLM  INTE 104
IF(IQ1.EQ.1.AND.SINT(J,1).EQ.0.0) SINT(J,1)=SL  INTE 105
IF(IQ2.EQ.1.AND.SINT(J,2).EQ.0.0.AND.SINT(J,2).EQ.0.0.AND.SINT(J,2).EQ.0.0) SINT(J,2)=0.0  INTE 106
13).EQ.0.0) SINT(J,4)=FLM  INTE 107
IF(IQ2.EQ.1.AND.SINT(J,1).EQ.0.0.AND.SINT(J,2).EQ.0.0.AND.SINT(J,2).EQ.0.0) SINT(J,1)=0.0  INTE 108
13).EQ.0.0) SINT(J,2)=SL  INTE 109
IF(IQ3.EQ.1.AND.SINT(J,1).EQ.0.0.AND.SINT(J,2).EQ.0.0.AND.SINT(J,2).EQ.0.0) SINT(J,1)=0.0  INTE 110
13).EQ.0.0) SINT(J,4)=FLM  INTE 111
IF(IQ3.EQ.1.AND.SINT(J,1).EQ.0.0.AND.SINT(J,2).EQ.0.0.AND.SINT(J,2).EQ.0.0) SINT(J,1)=0.0  INTE 112

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13).EQ.0.0) SINT(J,3)=SL          INTE 113
IF(IPER.EQ.0) GO TO 20          INTE 114
IF (IEVT.EQ.0) WRITE(LTER,1899),STITLE    INTE 115
IF (IEXT.EQ.0) WRITE( 69,1879),STITLE    INTE 116
1879 FORMAT (10AB)                INTE 117
1899 FORMAT (1H100 EIGENRAY SET      10AB,
IF(IEXT.EQ.0) WRITE(LTER,899)
PR=10.*ALOG10(SL)
N=NCOUNT(I)
IEXT=1
M=N/IT4
NTO=N-4*ITN
NM=IT4
NSR=M-4*ITN
NTU=N-4*ITN
NBR=M
IF (IQ3.EQ.1) IQUAL=3          INTE 121
IF (IQ2.EQ.1) IQUAL=2          INTE 122
IF (IQ1.EQ.1) IQUAL=1          INTE 123
IREM=2
IF (IQ3.EQ.1.AND.SINT(J,3).NE.0.0) IREM=2H0  INTE 124
IF (SINT(J,3).NE.0.0.AND.IQ1.EQ.1) IREM=2H00 INTE 125
WRITE(LTER,900) I,NBR,NTU,NSR,NTO,RMAX,ZR,TH,T,PR,IQUAL,IREM
RMKM=RMAX/1000.0                INTE 126
WRITE(69,1878) I,NBR,NTU,NSR,NTO,RMKM,ZR,TH,T,PR          INTE 127
1878 FORMAT (5S,F10.4,FIU,4,F10.4,F15.5,F10.1)          INTE 128
899 FORMAT (0NRAY NBR NTU NSR NTO,10X,*CHANGE DEPTH THETA INTE 129
1 TIME*, 9X,*SL(DB)*,5X,*IQUAL*,4X,*REM*)           INTE 140
900 FORMAT (5S,F15.0,F10.4,F10.4,F13.5,F10.1,6X,IS,5X,A2) INTE 141
22 FLM=SINT(J,0)
IF (SINT(J,1).NE.0.1) SL=SINT(J,1)          INTE 142
IF (SINT(J,2).NE.0.4 D=SINT(J,1)+EQ.0.0) SL=SINT(J,2) INTE 143
IF (SINT(J,3).NE.0.4 D=SINT(J,1)+EQ.0.0) SL=SINT(J,3) INTE 144
IF (SINT(J,3).EQ.0.0) GO TO 27          INTE 145
IF (IQ1.EQ.1.AND.SINT(J,1).NE.0.0) 71,72          INTE 146
71 TYPEIRP(J)=SSL(J)          INTE 147
IF (ISCP.EQ.0) GO TO 27          INTE 148
TYPEISC(J)=TYP5(J)          INTE 149
QUAD(J)=QUS(J)          INTE 150
GO TO 27          INTE 151
72 SSL(J)=TYPEIRP(J)          INTE 152
27 TYPEIRP(J)=TYPEIRP(J)+SL+FLM          INTE 153
IF (ISCP.EQ.0) GO TO 2H          INTE 154
PR=SQRT(SL)          INTE 155
P=OMEGA*T+PHASE(P)
IF (IQ3.EQ.1.AND.IQ1.EQ.0) QUS(J)=QUAD(J)          INTE 156
QUAD(J)=QUAD(J)+PR*SIN(P)          INTE 157
IF (IQ3.EQ.1.AND.IQ1.EQ.0) TYP5(J)=TYPEISC(J)          INTE 158
TYPEISC(J)=TYPEISC(J)+PR*COS(P)          INTE 159
25 IF (INXT.GE.1.OR.IPR.NE.INW.AND.INW.NE.INAT) IHP(J)=0          INTE 160
29 IPR=INd          INTE 161
INW=INXT          INTE 162
IF (INd.EQ.0.OR.INW.LT.1.AND.INXTT.LT.1) GO TO 30          INTE 163
DO 28 LL=1,LNRC          INTE 164
SINT(LL,1)=0.0          INTE 165
          INTE 166
          INTE 167
          INTE 168

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SINT(LL,2)=0.0          INTE 169
SINT(LL,3)=0.0          INTE 170
SINT(LL,4)=0.0          INTE 171
28 CONTINUE              INTE 172
30 CONTINUE              INTE 173
35 DO 37 I=1,LNRC        INTE 174
    TYPEI5C(I)=TYPEI8C(I)*2+QUAD(I)**2
37 QUAD(I)=EXP(-RCD(I)/DZBAR)   INTE 175
    IF(IT2.EQ.0) GO TO 60      INTE 176
    F=2.0*RMAX*DZBAR          INTE 177
    EZ=EXP(-ZB/DZBAR)         INTE 178
    DO 50 I=1,NRAY           INTE 179
    IF(ABS(SS(I)).LT.ALIM)   GO TO 50
    EZ=EXP(-ZZ(I)/DZBAR)     INTE 180
    SL=SEC(TGAM(I),.985(I)/F) INTE 181
    SGK=TGAM(I)*AK/SQRT(1.+TGAM(I)**2) INTE 182
    SL=SEC(I,-.98*(EZ/EZ+E6)) INTE 183
    DO 40 J=1,LNRC           INTE 184
    IF(RCD(J).GT.ZB) GO TO 50
    ER=QUAD(J)               INTE 185
    IF(LLMR.NE.0) FLM=2.*SIN(RCD(J)*SGK)**2 INTE 186
    IF(EH.GT.EZ) GO TO 39      INTE 187
    S=SL*ER/EZ                INTE 188
    GO TO 40                  INTE 189
39 S=SL*EZ/ER                INTE 190
40 TYPEII(J)=TYPEIII(J)+5*FLM  INTE 191
50 CONTINUE                  INTE 192
50 IF(I>3.EQ.0) RETURN      INTE 193
50 DO 70 I=1,NRAY           INTE 194
    CALL CHANNEL(ZZ(I)+TGAM(I),ZTO,ZTU)
    CALL RCALC
    IF(LLMR.NE.0) CALL WDENS(ZZ(I)*CTR)
    SL=FVA*SS(I)/RMAX
    DO 65 J=1,LNRC           INTE 195
    IF(RCD(J).GT.ZTU) GO TO 70
    IF(MCH(J).LT.ZTO) GO TO 65
    CALL WJENS(RCD(J),S1)
    IF(LLMR.EQ.0) GO TO 64
    TG=TGAM(I)*CTR/S
    FLM=2.*SIN(AK*R.B(J)*TG/SQRT(1.+TG**2))**2
    S=SL*FLM
64 TYPEIII(J)=TYPEIII(J)+S*SL
65 CONTINUE
70 CONTINUE
RETURN
END

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5.40S INTENSTY

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| | IDENT | INTENSTY |
|------------------|-------|----------|
| PROGRAM LENGTH | Q3451 | |
| ENTRY POINTS | 01540 | |
| BLOCK NAMES | | |
| LOUDNESS | 00765 | |
| TLE | 00012 | |
| RAYS | 13561 | |
| INFO | 00024 | |
| PIDEF | 00003 | |
| VELPRF | 00311 | |
| TNPSTR | 00266 | |
| ABC | 00026 | |
| EXTERNAL SYMBOLS | | |
| Q2007111 | | |
| FMEND. | | |
| Q8QDICT. | | |
| VELCALC | | |
| CHANNEL | | |
| RCALC | | |
| WDENS | | |
| ALOG10 | | |
| SQRTF | | |
| SINF | | |
| MINIF | | |
| EXPF | | |
| COSF | | |
| ATANF | | |
| STH. | | |
| SLO. | | |
| QNSINGL. | | |

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SUBROUTINE ITAPRINT (NINT)
COMMON /INFO/ RSTART,RMAX,PMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1  ISCP,IT1,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT
COMMON /TMPCTH/ DLC(102)
COMMON/LIM1/ H1 (10), ER (10), R2 (10)
COMMON/AHC/PUNCHD# (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1
COMMON /TLE/STITLE (10)
DATA (JNCRB1)
DIMENSION LINE(90),DE(4),FMT(6),AAL(400),IS(4),ABDDD(102)
EQUIVALENCE (LINE,DEC)
COMMON /LOUDNESS/ LNRC,RCD(100),AL(100,4)
EQUIVALENCE (AL,AAL)
DATA (HA6=3HA7),(HF6=5HF7,1),(B=1H ),(S=1HS,1HR,1H2,1H3)
DATA (FMT(1)=6(F8,3),(FMT(6)=8H6X,90A1))
DIMENSION ITT(4)
EQUIVALENCE (ISCP,ITT)
DATA (IENT=0),(IFT2=0),(IBL=0)
IF (IFT1,EC,IFT2) GE TE 3 S IBM=0 S IFT2=IFT1
3 IF (IFT1,EC,0,CR,IEH,EC,1) GE TE 2 S INCR=1 S IENT=0 S HA6=3HA7,
HF6=5HF/,1, S B=1H SIS(1)=1HS S IS(2)=1HR S IS(3)=1H2 SIS(4)=1H3
FMT(1)=6(F8,3), S FMT(6)=8H6X,90A1) S IBH=1
2 IF(NINT,EJ,1) GE TE 40 S AH=0, S DB 10 I=1,400
IF(AAL(1),GT,AM) AM=AAL(1)
10 CONTINUE S DBM=10,0 AINT(ALEG10(AM)) S DBL=DBM=90,
RK#,001*RMAX
ISK=0
IF (IEN1,EC,0) WRITE (39,1) STITLE
IF(LNRC,GE,35) ISK=1
WHITE (39,900),ISK,RK,CBL,CBM
DE 30 I=1,LNRC
DE 15 J=1,90
15 LINE(J)=1H
DE 25 J=1,4
IF(AL(I,J),LT,ALIM) GE TE 20
FMT(J+1)=HF6
DB(J)=1U,0 ALEG10(AL(I,J))
IL=(DB(J)=DBL)=1,D
IF(IL,LE,0,WR(IL,GT,90) GE TE 25
LINE(IL)=IS(J)
GE TE 29
20 FMT(J+1)=HA6
DB(J)=B
25 CONTINUE
30 WRITE (39,FMT) RCD(I),DB,LINE S IENT=1
RETURN
40 IF(IEN1,NE,0) GO TE 41
WRITE(39,1) STITLE
1 FORMAT (1M1,10AB)
WHITE (36,920) STITLE,LNRC,ITT(1),ITT(2),ITT(3),ITT(4)
IF (IEN1,EC,0) WRITE (35,941) STITLE,(RCD(J),J=1,19)
941 FORMAT (10AB,/,10F8,3)
IF (IEN1,EC,0,AND,ITT(1),GT,0) WRITE (45,912) STITLE
912 FORMAT (* COHERENT PHASE VALUES*,/,10AB)
IF (IEN1,EC,0,AND,ITT(2),GT,0) WRITE (46,913),STITLE
913 FORMAT (* RANDOM PHASE VALUES*,/,10AB)
IF (IEN1,EC,0,AND,ITT(3),GT,0) WRITE (47,914),STITLE

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| | | |
|-----|--|---------|
| 914 | FORMAT(1, TYPE 2 VALUES//,10AB) | ITNP 57 |
| | IF (IEN1,EQ,1,AND,ITT(4),GT,0) WRITE (48,915),STITLE | ITNP 58 |
| 915 | FORMAT(1, TYPE 3 VALUES//,10AB) | ITNP 59 |
| | IEN1,I | ITNP 60 |
| | WHITE(JY,YC5) (HCU(I),I=1,LNRC) | ITNP 61 |
| | WHITE (J9,908) | ITNP 62 |
| 900 | FORMAT(110,INTENSITIES AT*,F10,3,0 KM, */*0 DEPTH ISC IRP | ITNP 63 |
| 1 | II III ,F0,1,84X,F6,1) | ITNP 64 |
| 905 | FORMAT(*0RECEIVED INTENSITY VS RANGE*,15X,*AT DEPTHS*/ | ITNP 65 |
| 1 | *0 R(KM) TYPE *,13F9,3//,19X,13F9,3) | ITNP 66 |
| 908 | FORMAT(1X) | ITNP 67 |
| 41 | RK=RMAX/1000, | ITNP 68 |
| | IP=0 | ITNP 69 |
| | DE 50 I=1,4 | ITNP 70 |
| | IF (ITT(I),EQ,0) GE TE 50 | ITNP 71 |
| | DE 45 J=1,LNRC | ITNP 72 |
| | DLU(J)= 10.*ALG10(AMAX1(ALIM ,AL(J,1))) | ITNP 73 |
| | PLNCHDR(INCH)=AHSF(WED(J)) | ITNP 74 |
| | ABDDD(J)=PUNCHDR(INCR) | ITNP 75 |
| | INCR=INCR+1 | ITNP 76 |
| | IF (INCR,LT,17) GE TE 45 | ITNP 77 |
| | INCR=1 | ITNP 78 |
| | WHITE (J6,909) (PLNCHDR(I)),I=1,16) | ITNP 79 |
| 45 | CENTINUE | ITNP 80 |
| | IF (I,EU,1,AND,ITT(1),GT,0) WRITE (45,911) (ABDDD(J),J=1,19) | ITNP 81 |
| | IF (I,EU,2,AND,ITT(2),GT,0) WRITE (46,911) (ABDDD(J),J=1,19) | ITNP 82 |
| | IF (I,EU,3,AND,ITT(3),GT,0) WRITE (47,911) (ABDDD(J),J=1,19) | ITNP 83 |
| | IF (I,EU,4,AND,ITT(4),GT,0) WRITE (48,911) (ABDDD(J),J=1,19) | ITNP 84 |
| | IF (IP,EU,0) GE TE 46 | ITNP 85 |
| | WRITE (J9,906) IS(I),(CDC(J),J=1,LNRC) | ITNP 86 |
| 906 | FORMAT(16X,A1,2X,13F9,1//,19X,13F9,1) | ITNP 87 |
| | GE TE 50 | ITNP 88 |
| 46 | IP=1 | ITNP 89 |
| | WHITE(3Y,907) RK,IS(I),(CDC(J),J=1,LNRC) | ITNP 90 |
| 907 | FORMAT(1,9,3,7X,A1,2X,13F9,1//,19X,13F9,1) | ITNP 91 |
| | 50 CENTINUE | ITNP 92 |
| 909 | FORMAT(10F5,1) | ITNP 93 |
| 911 | FORMAT(10F8,3) | ITNP 94 |
| 920 | FORMAT(10AB//,515) | ITNP 95 |
| | RETURN | ITNP 96 |
| | END | ITNP 97 |

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S ITNPRINT

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ED 0

| | ICENT | ITNPRINT |
|------------------|----------|----------|
| PROGRAM LENGTH | 01560 | |
| ENTRY POINTS | ITNPRINT | 00511 |
| BLOCK NAMES | | |
| INFO | 00024 | |
| TEMPSTR | 00266 | |
| LIMITS | 00076 | |
| ABC | 00026 | |
| TLE | 00012 | |
| LOUDNESS | 00765 | |
| EXTERNAL SYMBOLS | | |
| THEND, | | |
| D101010U | | |
| QSELECT, | | |
| ALEG10 | | |
| MAX1F | | |
| STH, | | |
| SLG, | | |
| QNSINGL, | | |

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SUBROUTINE IVSRPL6T(ITF)
COMMON /INFO/ RSTART,RMAX,CHEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1 ISCP,IT1,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT
COMMON /LOUDNESS/ LNRC,HCD(100),AL(100,4)
COMMON /THPSYM/ DUE(102)
COMMON /TITLE/SITLE(10)
COMMON /ABC/PLACHDB(16),INCR,NBRS,NSRS,ALIM,IFT1,IFT2
DATA (IEN=0),(IFT2=0),(IBH=0)
DIMENSION LINE(105)
EQUIVALENCE (LINE,EDC)
IF (IFT1,EQ,IFT2) GE TE 13
IBH=0
IFT2=IFT1
13 IF (IFT1,EQ,0,SH, IBS,EQ,1) GE TE 3
IEN=0
IBH=1
3 IF (IEN,NE,0) GO TO 10
WHITE (38,1),SITLE
1 FORMAT (1H1,1UAB)
IEN=1
IT=ITP+1
IF (IT,EU,5) IT=1
GO 2 I=1,11
2 LINE()=-170*10*
NBM1=0(LNHC,9)
WRITE(38,900) (HCD(I),I,I=1,N)
WRITE (38,901) (LINE(I),I=1,11)
DE 25 I=1,11
25 LINE()=1H+
WRITE (38,903) (LINE(I),I=1,11)
900 FORMAT(*0*,15A,*RECEIVED INTENSITY VS RANGE*/*RECEIVER AT DEPTH P*)VSR 31
1LGTS AS///(F18,3.19)
901 FORMAT(*0 R(KM)*,5X,11I1C) VSR 32
903 FORMAT (14X,11(9X,A1))
10 IF (IT,LE,0,SH,IT,GT,4) HETLRN
DE 15 I=1,105
15 LINE()=48
DE 20 I=1,V
DB#10,*AL&G10(AMAX1(1,E=25,AL(1,IT)))
IP#161,5*D9
IF (IP,LE,0,SH,IP,GT,105) GE TE 20
LINE(IP)=
20 CONTINUE
RK=RMAX/1000,
WRITE(38,902) RK,LINE
902 FORMAT(9,3,14X,1U$H1)
RETURN
END
IVSR 1
IVSR 2
IVSR 3
IVSR 4
IVSR 5
IVSR 6
IVSR 7
IVSR 8
IVSR 9
IVSR 10
IVSR 11
IVSR 12
IVSR 13
IVSR 14
IVSR 15
IVSR 16
IVSR 17
IVSR 18
IVSR 19
IVSR 20
IVSR 21
IVSR 22
IVSR 23
IVSR 24
IVSR 25
IVSR 26
IVSR 27
IVSR 28
IVSR 29
IVSR 30
IVSR 31
IVSR 32
IVSR 33
IVSR 34
IVSR 35
IVSR 36
IVSR 37
IVSR 38
IVSR 39
IVSR 40
IVSR 41
IVSR 42
IVSR 43
IVSR 44
IVSR 45
IVSR 46
IVSR 47
IVSR 48

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; IVSRPLOT

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ED 0

IDENT IVSRPLOT

| | |
|----------------|----------|
| PROGRAM LENGTH | 00432 |
| ENTRY POINTS | IVSRPLOT |
| BLOCK NAMES | 00064 |
| INFO | 00024 |
| LOUDNESS | 00765 |
| TMPSTR | 00266 |
| TLE | 00012 |
| ABC | 00026 |

EXTERNAL SYMBOLS

| |
|----------|
| THEND, |
| 01G1010U |
| 28CDICT, |
| ALEG10 |
| XMINUF |
| MAX1F |
| STH, |
| SLG, |
| ONSINGL, |

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SUBROUTINE RAY PL6T(KP,ZMAX)
COMMON /INFO/ RSTART,RMAX,EHGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1 ISCP,IT1,IT2,IT3,IPER,IFTMS,LTRT,LTER,LTRP,LPIN,IATT
COMMON /RAYS/ NRAY,TGAP(1000),ZZ(1000),SS(1000),TIME(1000),
1 NCOUNT(1000),PHASE(1000)
COMMON /THPSTR/ DDC(182)
COMMON/ABC/PUACHDW(16),INCR,NBRS,NSRS,ALIM,IFT,IFT1
DIMENSION IR(25),ISYM(25),LINE(115),INUM(9)
COMMON /THIARG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZERO(100),
1 RZEHU(100),AA(100),BB(100),SST(100),CCT(100),NTR
EQUIVALENCE (LINE,CDC)
DATA (ISYM=1H,A,1H,C,1H,D,1H,E,1H,F,1H,G,1H,H,1H,I,1H,J,1H,K,1H,L,1H,M,1H,N,1H,O)RAYP 1
1 ,1H,P,1H,Q,1H,R,1H,T,1H,U,1H,V,1H,W,1H,X,1H,Y,1H,Z,1H*)RAYP 2
COMMON /TLE/STITLE(10)
DATA (IENT=0, (IBLK=1F), (IB=1H), (IS=1HS), (IFT2=0), (IBH=0))RAYP 3
DATA (INUM=1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9,1H9)RAYP 4
IF (IFT1,0,IFT2) GO TO 2
IBH=0
IFT2=IFT1
2 IF ((IFT1,0,0,0R,IBH,EC,1) GO TO 3
IENT=0 S IBH=1
3 IF ((IENT,NE,0) GO TO 10
WRITE (LTRP,1),STITLE
IENT=1
AMP=FLGAT(NRAY)/FLOAT(KP)
DE 5 I=1,NP
AMP=(FLGAT(1)+D)*1,
IR()=A
IF((IR(),GT,0RAY) IR()=RAY
5 CONTINUE
SZ=ZMAX/114,
WRITE (LTNP,900) SZ
10 ZB=AL(NIR)+BL(NTR)*RMAX
RMAX,001*RMAX
IB=(ZMAX-ZB)/SZ+1,5
IB1=1
IF((IB,LE,0) GO TO 12
IF((IB,GT,115) IB=115
DE 11 IB1,IB
11 LINE()=IBH
IB1=IB+1
12 DE 15 IB1,114
LINE()=IBLNW
LINE(115)=IS
DE 20 IB1,NP
K=IR()
IF ((IB45,0,2500,AKD,NSRS,EG,2500) GO TO 17
1N=ACOUNT(K) SMNN/ITN SNBNP/ITN SNBRMN=NNN/ITN SMNN/ITN SNBRM
17 IF (ABS(SS(K)),LT,ALIM,ER,NBR,GT,NBRS,0R,NSR,GT,NSRS) GO TO 20
ZR=ZZ(K)
IP=(ZMAX-ZR)/SZ+1,5
IF (IP,GT,115) IP=115
IF (IP,LE,0) GO TO 20
IF (LINE(IP),EG,IBLK,0R,LINE(IP),EQ,IS,0R,LINE(IP),EQ,IBR) GOTOB 19RAYP 19RAYP 19
DE 16 J=1,B
IF (LINE(IP),NE,INUM(.)) GO TO 16
RAYP 20
RAYP 21
RAYP 22
RAYP 23
RAYP 24
RAYP 25
RAYP 26
RAYP 27
RAYP 28
RAYP 29
RAYP 30
RAYP 31
RAYP 32
RAYP 33
RAYP 34
RAYP 35
RAYP 36
RAYP 37
RAYP 38
RAYP 39
RAYP 40
RAYP 41
RAYP 42
RAYP 43
RAYP 44
RAYP 45
RAYP 46
RAYP 47
RAYP 48
RAYP 49
RAYP 50
RAYP 51
RAYP 52
RAYP 53
RAYP 54
RAYP 55
RAYP 56

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LINE(|P|=|NUM|J+1)
G6 TO 2U
16 CONTINUE
LINE(|P|=|NUM|1)
G6 TO 2U
19 LINE(|P|=|SYM|I)
20 CONTINUE
WRITE (LTYP,901) MM,LINE
1 FORMAT (1H1,1D4.0)
900 FFORMAT(27H0PL0T OF RAY PATHS SCALE,F8.2,2X,10HM/POSITION/
1 10H0CHANGE(KM),JX,114(1HX),1HS)
901 FFORMAT(11,3,2X,115A1)
RETURN
END

```

| | |
|------|----|
| RAYP | 57 |
| RAYP | 58 |
| RAYP | 59 |
| RAYP | 60 |
| RAYP | 61 |
| RAYP | 62 |
| RAYP | 63 |
| RAYP | 64 |
| RAYP | 65 |
| RAYP | 66 |
| RAYP | 67 |
| RAYP | 68 |
| RAYP | 69 |
| RAYP | 70 |

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S RAYPLOT

06/04/73

ED 0

| | ICENT | RAYPLOT |
|----------------|---------|---------|
| PROGRAM LENGTH | 00605 | |
| ENTRY POINTS | RAYPLOT | 00145 |
| BLOCK NAMES | | |
| INFO | 00024 | |
| RAYS | 13561 | |
| TMPSTR | 00266 | |
| ABC | 00026 | |
| TRIANG | 02261 | |
| TLE | 00012 | |

EXTERNAL SYMBOLS

THEEND,
Q1G10100
Q8G10CT,
STH,
SLG,
QNSINGL,

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SUBROUTINE RAYZDIST (NP)
COMMON /RAYS/ NRAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),
1 NCOUNT(1000),PHASE(1000)
COMMON /INFO/ RSTART,RMAX,CMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1 ISCP,IT1,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT
COMMON /THPSTR/ DUC(182)
COMMON /TLE/STITLE (10)
DIMENSION LINE(71)
DIMENSION ISYM(25),IR(25)
COMMON /PIDEF/ PI,CTR,THPPI
EQUIVALENCE (LINE,CDI)
COMMON/AHG/PUNCHDR (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1
DATA (IEN=0),(IFT2=0),(IBH=0)
DATA (ISYM=1HA,1HC,1HD,1HE,1HF,1HG,1HH,1HI,1HJ,1HK,1HL,1HM,1HN,1H)
1 ,1HP,1HO,1HR,1HT,1HL,1HV,1HW,1HX,1HY,1HZ,1H*)
IF (IFT1,EQ,IFT2) GO TO 7
IBH=0
IFT2=IFT1
7 IF (IFT1,EQ,0,OR,IBH,EC,1) GE TO 6
IEN=0
IBH=1
6 IF (IEN,EQ,1) GO TO 3
LTRD=37
ANP=FLOAT(NRAY)/FLOAT(NP)
D6 4 I=1,NP
ANP=(FLOAT(I)=,0)*1,
IR(I)=A
IF (IR(I),GT,NRAY) IR(I)=NRAY
CONTINUE
IEN=1
3 WRITE (LTRD,2),STITLE
INC=1
1 CALL CHANNEL(1,,1000,,25,ZB)
D6 5 I=1,71
LINE(I)=1HX
RK=RMAX/1000,
SCALE=ZB/71,0
WRITE(LTRD,900) RK,ZB,SCALE,LINE
D6 8 I=1,71
8 LINE(I)=1M
D6 40 I=1,NRAY
SS=SS()
IF (NBRS,EQ,2500,AND,NSRS,EC,25) GO TO 35
NONCOLN()
NON/ITN
NOM/ITN
NSRSH=NO/ITN
NON/ITN
NOMH
35 IF (S,GT,AL(1),AND,NBR,LE,NBRS,AND,NSH,LE,NSHS) GO TO 12
IF (I,EQ,1,IR(INC))10,15
10 WRITE (LTRD,1901),ISYM(INC),I
INC=INC+1
GO TO 40
15 WRITE(LTRD,901) I
900 FORMAT(26HCRAY DEPTH DISTRIBUTION AT,F10.4,4H KM,,10X,*BOTTOM DEPTRAYZ
RAYZ   1
RAYZ   2
RAYZ   3
RAYZ   4
RAYZ   5
RAYZ   6
RAYZ   7
RAYZ   8
RAYZ   9
RAYZ  10
RAYZ  11
RAYZ  12
RAYZ  13
RAYZ  14
RAYZ  15
RAYZ  16
RAYZ  17
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RAYZ  49
RAYZ  50
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RAYZ  52
RAYZ  53
RAYZ  54
RAYZ  55
RAYZ  56

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1H80,F10,3,0 M,,1UX,,SCALE,,F10,3,0 M/POSITION,,/,29WLD NRAY RAYZ 97
2NR NRY NSR NT6,3X,5MCERT,5X,5HT-ETA,6X,4HTIME,1X,6HL0SES,1X,RAYZ 98
371A1) RAYZ 99
901 FERMAT(4,10X,11HTERMINATED,) RAYZ 60
1901 FERMAT (2X,A1,1X,14,10X,11HTERMINATED,) RAYZ 61
GE TO 4C RAYZ 62
12 TH=10,ALOG1C(S) RAYZ 63
T=TIME(i) RAYZ 64
Z=Z2(i) RAYZ 65
N=NCENH(I) RAYZ 66
M=N/ITN RAYZ 67
NTOBN=M*ITN RAYZ 68
NSM*ITN RAYZ 69
NSH=H*ITN RAYZ 70
PN=M/ITN RAYZ 71
NTUBN=M*ITN RAYZ 72
NBR=M RAYZ 73
LINE(1)=1HE RAYZ 74
LINE(71)=1HS RAYZ 75
CALL CHANNEL(Z,TGAM(I),ZTB,ZTU) RAYZ 76
IZP=70,*(1,-ZTL/ZB)+1,5 RAYZ 77
IF (IZP,GT,71,ER,IZP,LT,1) GE TO 45 RAYZ 78
LINE(IZP)=1H* RAYZ 79
45 IZM=70,*(1,-ZTB/ZB)+1,5 RAYZ 80
IF (IZM,GT,71,ER,IZM,LT,1) GE TO 55 RAYZ 81
LINE(IZM)=1H* RAYZ 82
55 IZH=70,*(1,-Z/ZB)+1,5 RAYZ 83
IF (IZH,GT,71,ER,IZH,LT,1) GE TO 60 RAYZ 84
LINE(IZH)=1H* RAYZ 85
60 THUTR=ATAN(TGAM(I)) RAYZ 86
IF (I,EG, IR(INC))20,25 RAYZ 87
20 WRITE (LTHD,902) ISYM(INC), I,NBP,NTU,NSR,NTB,Z,TH,T,DB,LINE
INC=INC+1 RAYZ 88
GE TO 30 RAYZ 89
RAYZ 90
902 FERMAT(2X,A1,1X,515, FE,2,F10,5,F10,3,F7,1,1X,71A1) RAYZ 91
25 WRITE (LTHD,1902) I,NBP,NTL,NSR,NTB,Z,TH,T,DB,LINE RAYZ 92
1902 FERMAT(4X,515, FE,2,F10,5,F10,3,F7,1,1X,71A1) RAYZ 93
30 IF (IZP,LE,71,AND,IZP,GE,1) LINE(IZP)=1H RAYZ 94
IF (IZM,LE,71,AND,IZM,GE,1) LINE(IZM)=1H RAYZ 95
IF (IZH,LE,71,AND,IZH,GE,1) LINE(IZH)=1H RAYZ 96
40 CONTINUE RAYZ 97
2 FERMAT (1H1,10AB,/)
RETURN RAYZ 98
END RAYZ 99
RAYZ 100

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18 RAYZDIST

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ED 0

| | ICENT | RAYZDIST |
|----------------|----------|----------|
| PROGRAM LENGTH | 01054 | |
| ENTRY POINTS | RAYZDIST | 0L234 |
| BLOCK NAMES | | |
| RAYS | 13561 | |
| INFG | 00024 | |
| THPSTR | 00266 | |
| TLE | 00012 | |
| PIDEF | 00003 | |
| AHC | 00026 | |

EXTERNAL SYMBOLS

G1G1010U
THEAD,
CGCDICT,
CHANNEL
ALEG10
ATANF
STH,
SLC,
ONSINGL,

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14A

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```
SUBROUTINE BYEBYE
DIMENSION LEAVE(1)
J=1
LEAVE(J)=630000000000000B
END
```

| | |
|------|---|
| BYBY | 1 |
| BYBY | 2 |
| BYBY | 3 |
| BYBY | 4 |
| BYBY | 5 |

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S HYEBYE

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ED 0

PROGRAM LENGTH
ENTRY POINTS HYEBYE
EXTERNAL SYMBOLS
ORCCICT,

ICENT HYEBYE

00017
00004

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IDS RECOVERY

| PROGRAM LENGTH
ENTRY POINTS | DUMP
RESTART | 00125
00000
00057 | EVENT | RECOVERY | 08/02/72 | EN 0 | PAGE NO. 1 | 00001 |
|--------------------------------|-----------------|-------------------------|--------|----------|----------|------|------------|-------|
| | ABSTATUS | MACH0 | PI | | | | | 00002 |
| | ST | STATUS | ((PI)) | | | | | 00003 |
| | NJUP | 0+07+ST | | | | | | 00004 |
| | NJUP | 0+00+ST | | | | | | 00005 |
| | EUM | | | | | | | 00006 |

| TITLE == DUMP AND RESTART FACILITY | 00008 |
|--|-------|
| IDENT NAME == Q-NHL-RECOVERY | 00009 |
| IDENT NUMBER == 00000000 | 00010 |
| LANGUAGE == COMPASS 5+3 | 00011 |
| COMPUTER == CDC 3600 | 00012 |
| CONTRIBUTOR == ANNA BYRD MAYS, CODE 7817+1 | 00013 |
| JOSEPHAS P. SHANNON, CODE 7817+3 | 00014 |
| RESEARCH COMPUTATION CENTER | 00015 |
| MATH. AND INFO. SCIENCES DIVISION | 00016 |
| DATE == JUNE 1970 | 00017 |
| PURPOSE == ALLOWS PROGRAMS WITH A LONG RUN-TIME TO HAVE A RESTART CAPABILITY | 00018 |
| | 00019 |

| 00V17 | MTI | E+HIV | DUMP+RESTART | 00021 | |
|-------|-----------|-------|--------------|---------------------------------------|-------|
| 00V06 | THIES | E0U | 15 | ALWAYS INPUT TAPE, FIRST OUTPUT TAPE | 00022 |
| 50V00 | LOCUME | E0U | 5+1 | PARTITY RE-HIV COUNTEN | 00023 |
| 00V52 | HANLITY | E0U | 50000B | OCTAL NUMBER ON DEMAND CANU | 00024 |
| 00V00 | UNLOADAUT | E0U | 42 | PARTITY STATUS BIT | 00025 |
| 00V00 | FRA | E0U | 0 | 1 IF UNLOAD TAPE AFTER USE. LAH SMITH | 00026 |
| | | | | | 00027 |

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| RS | RECOVERY | | | | 08/02/72 | EN | O | PAGE NO. | 2 |
|-------|----------|---|--------|--------|----------|---------------------|----------------------------------|----------|-------|
| 00000 | 63 | 0 | 00000 | DUMP | UJJP | ee | | | 00020 |
| | 90 | 0 | 77777 | | | | | | |
| 00001 | 77 | 2 | 00000 | | USTA | (0)SAVEAU | SAVE REGISTERS TO DUMP ON TAPE | 00030 | |
| | 20 | 0 | P00110 | | | | | | |
| 00002 | 00 | 7 | 00053 | | NAT | DeA | | | 00031 |
| | 20 | 0 | P00112 | | SIL | SAV12,0 | | | 00032 |
| 00003 | 96 | 1 | P00113 | | SIL | SAV12,1 | | | 00033 |
| | 97 | 2 | P00113 | | SIL | SAV12,2 | | | 00034 |
| 00004 | 96 | 3 | P00114 | | SIL | SAV13,0 | | | 00035 |
| | 97 | 4 | P00114 | | SIL | SAV13,1 | | | 00036 |
| 00005 | 94 | 5 | P00115 | | SIL | SAV13,2 | | | 00037 |
| | 97 | 6 | P00115 | | SIL | SAV13,3 | | | 00038 |
| 00006 | 90 | 1 | 00017 | | ENI | SAV56,0 | | | 00039 |
| | 90 | 0 | 00000 | | ENI | MT1=1 | | | 00039 |
| 00007 | | | | MOUE | MOUE | ((0,1),0,MIN,LO) | MODE TAPE 200 BPI | | |
| 00012 | 90 | 6 | 00004 | | ENI | TRIE5=0 | SET ME-THY COUNTER | 00040 | |
| | 90 | 0 | 00000 | | | | | | 00041 |
| 00013 | | | | MEW51 | MEW51NU | ((0,1),0,0) | | | |
| 00016 | | | | | MEB0 | ((0,1),0,CHM=0) | | 00042 | |
| 00021 | | | | | ASTATUS | ((0,1),0,0) | | 00043 | |
| 00029 | 63 | 0 | 38052 | | ZHJP | Q,PARITY,CONT=1 | JUMP IF NO PARITY ERNOR | 00044 | |
| | 64 | 0 | P00050 | | | | | | |
| 00024 | | | | | MEW51NU | ((0,1),0,0) | | 00044 | |
| 00031 | | | | | MEB0 | ((0,1),0,NSKIPCR,0) | MAKE SURE OF PARITY ERNOR | 00045 | |
| 00040 | 63 | 0 | 38052 | | ASTATUS | ((0,1),0,0) | | 00046 | |
| | 64 | 0 | P00050 | | ZHJP | Q,PARITY,CONT=1 | JUMP IF NO PARITY ERNOR | 00047 | |
| 00041 | 55 | 0 | P00013 | | IJP | REW=1+0 | | 00048 | |
| | 51 | 1 | 00001 | | INI | 1+1 | | 00049 | |
| 00042 | | | | | RELEASE | ((1,1),0,0) | | 00050 | |
| 00044 | 62 | 0 | 00022 | | MOUPINE | W10MT1=3:MOUE | BAU TAPE --- THY ANOTHER UNIT | 00051 | |
| | 30 | 1 | P00007 | | | | JUMP IF NOT OVER TAPE UNIT LIMIT | 00052 | |
| 00045 | 12 | 1 | P00102 | | LUA | ERROR=MT1=1+1 | ABORT MESSAGE | 00053 | |
| | 20 | 0 | P00067 | | STA | 0+0+1 | | 00054 | |
| 00046 | | | | | ASORT | 0+ | KILL JOB | 00055 | |
| 0r | 62 | 0 | 00017 | CONT=1 | IJP | UNLOAD=1+2 | | 00056 | |
| | 30 | 1 | P00045 | | MOUPINE | W10MT1=0,3 | JUMP IF NOT FIRST TAPE | 00057 | |
| 00041 | | | | | MEW51NU | ((0,1),0,0) | PERFORM PREF REWIND | 00058 | |
| 00054 | 92 | 1 | P00113 | | IJP | UNLOADMT | | 00059 | |
| | 93 | 0 | P00115 | | LUA | SAVE12+1 | RELLOAD USED INDEX REG. | 00060 | |
| 00055 | 77 | 2 | 00000 | | LIL | SAVE56+0 | | 00061 | |
| | 12 | 0 | P00110 | | ULDA | SAVEAO | RESTORE A AND Q | 00062 | |
| 00056 | 75 | 0 | P00000 | | UJP | DUMP | EXIT! | 00063 | |
| | 90 | 0 | 00000 | | | | | | 00064 |

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| 405 RECOVERY | | | 04/02/72 | E | D | PAGE NO. | J |
|--------------|-------------|--------------|----------|-----------------|------------------------------|----------|---|
| 00047 | 00 0 00000 | RESIDENT UCT | 0 | | | 00078 | |
| 00048 | 00 0 00000 | | | | | 00079 | |
| 00049 | 77 1 00000 | | E40 | * | | 00080 | |
| | | | | | | 00081 | |
| 00050 | 50 0 00000 | | ENI | TRIES=0 | REGISTERS NEED NOT BE SAVED | 00082 | |
| 00051 | | | MODE | (MT1),0,LU,MIN) | SET MODE TO 200 BPI | 00083 | |
| 00052 | | | HEWIND | MT1,0 | | 00084 | |
| 00053 | | | HEAD | MT1,RCA,0 | HEINGAHNATE CONF | 00085 | |
| 00054 | | | ASTATUS | MT1 | | 00086 | |
| 00055 | 63 0 30052 | | ZJP | U,PAHITY,CONT,2 | | 00087 | |
| 00056 | 64 0 P00102 | | | | | 00088 | |
| 00057 | 55 0 P00066 | | IJP | HEW,2,0 | | 00089 | |
| 00058 | | | ABONI | BAU READ | KILL JOB IF TAPE UNREADABLE | 00090 | |
| 00059 | 12 0 P00112 | CONT,2 | LUA | SAVED | REVITALIZE MACHINE REGISTERS | 00091 | |
| 00060 | 00 7 00555 | | NAT | A,U | | 00092 | |
| 00061 | 77 2 00000 | | ULDA | SAVEAQ | | 00093 | |
| 00062 | 12 0 P00110 | | | | | 00094 | |
| 00063 | 52 1 P00113 | | L1U | SAVE12,1 | | 00095 | |
| 00064 | 53 2 P00113 | | L1L | SAVE12,2 | | 00096 | |
| 00065 | 52 3 P00114 | | L1U | SAVE34,0 | | 00097 | |
| 00066 | 53 4 P00114 | | L1L | SAVE34,1 | | 00098 | |
| 00067 | 52 5 P00115 | | L1U | SAVE86,5 | | 00099 | |
| 00068 | 51 6 P00115 | | L1L | SAVE86,6 | | 00100 | |
| 00069 | 75 0 P00057 | | IPN | UNLOAD<7>1 | | 00101 | |
| 00070 | 50 0 00000 | | UJP | RESTART | | | |

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| RECOVERY | | | | | | | 04/02/72 | EN | O | PAGE NO. | 6 |
|----------|----|---|--------|---------|-------|-----------------------------------|---------------------------|----|---|----------|---|
| 00110 | | | SAVEAU | 035 | 2 | | | | | 00103 | |
| 00112 | | | SAVEU | 035 | 1 | | | | | 00104 | |
| 00113 | 00 | v | COV00 | SAVE12 | ULT | 0 | | | | 00105 | |
| 00114 | 00 | v | 00V00 | SAVE14 | ULT | 0 | | | | 00104 | |
| 00115 | 00 | v | 00V00 | SAVE54 | ULT | 0 | | | | 00107 | |
| 00116 | 00 | v | 00V00 | SAVE56 | ULT | 0 | | | | 00109 | |
| 00117 | 50 | v | 17177 | HC#A | IUTwL | (1)000000-7777H | ALL OF BANK ONE | | | 00109 | |
| | 00 | 1 | 00V00 | | | 77776H=LOUNGE,FWA=77778H=LOUNGE=1 | | | | 00110 | |
| 00120 | 50 | v | P50V00 | | IUTwL | | | | | 00111 | |
| | 00 | 0 | 27776 | | | | | | | 00112 | |
| 00121 | 10 | v | 00V06 | | IUTw | (0)SAVEAU,A | SPACE FOR INDEX REGISTERS | | | 00113 | |
| | 00 | 0 | P00V10 | | | | | | | 00114 | |
| 00122 | 20 | 0 | 17177 | HC#A | EJU | HC#A | | | | 00115 | |
| | 00 | 0 | 77177 | HSKIPCD | IJSR | 00,00 | | | | 00116 | |
| 00123 | 22 | 2 | 12986 | EHMLH | 0GU | 1,0ADW=15 | | | | 00116 | |
| | 51 | 0 | 00106 | | | | | | | 00117 | |
| 00124 | 22 | 2 | 12986 | | BLD | 1,0ADW=17 | | | | 00118 | |
| | 51 | 0 | 00107 | | | UNLOADMT,1 | | | | 00119 | |
| | | | | IPT | | | | | | 00121 | |
| | | | | END | | | | | | | |

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PROGRAM TRIPLT
C THIS VERSION IS COMPATIBLE WITH 4-5-72 VERSION OF TRIMAIN      TPLT   1
C DISK VERSION OF TRIPLT                                         TPLT   2
C IF INFO WILL FIT IN CORE DISK IS NOT OPENED                  TPLT   3
C THIS DETERMINED BY NRMAX AND THE NUMBER OF RAYS TO PLOT        TPLT   4
C                                                               TPLT   5
C                                                               TPLT   6
COMMON /INFO/ ID,NR,RMAX,ZMAX,SCALE,AL,RR(2000),ZBOT(2000),IKNM  TPLT   7
DIMENSION TITLE(10),BUF(254),NRPLOT(512),ZR(1000),TR(1000),SS(1000)TPLT   8
1),NCOUNT(1000)
CUMMON /1/ ZSTAR(16384)
CUMMON /2/ TSTAR(16384)
900 FORMAT(10A8)
901 FORMAT(28H1CALCUMP PLOT FROM RAY TAPE ,10A8)                TPLT  13
902 FORMAT(2F8.3,I4,6I5,I10,J)                                     TPLT  14
903 FORMAT(8HULENGTH,F10.2,3X,10HMAX DEPTHs,F12.1,3X,14HN0, OF RECORD)TPLT  15
15,I10,5X,*IKNM*,13,5X,*IFMC*,13,5X,*NFSK*,13,5X,*ITTR*,13,/,  TPLT  16
21X,*DBL LIMIT*,F8.3,5X,*MAXIMUM NUMBER OF SURFACE REFLECTIONS*,  TPLT  17
J15,5X,*MAXIMUM NUMBER OF BOTTOM REFLECTIONS*,15)                 TPLT  18
904 FORMAT(20I4)                                                 TPLT  19
905 FORMAT(5HUNRAY,20I5)                                         TPLT  20
906 FORMAT(11HONG OF HAs,16,3X,15HLENGTH OF BLOCK,I6,3X,12HN0 OF BLOC)TPLT  21
1KS,16)                                                       TPLT  22
9039 FORMAT(24HOPARITY ERROR IN RECORD ,16)                         TPLT  23
1DFO=0 $ IC0=0 SREAD 4,1TNC SKEWIND 1                           TPLT  24
4 FORMAT (1Z)
CALL PLOTS(BUF,254,10)                                         TPLT  25
2 READ Y02, AL,ZMAX,NRMAX,IKNM,IFMC,NFSK,ITTR,NSR1,NBR1,ALIM1
IF (EOF,60)2,
7 IL=IL+1
DO J=1,NFSK
3 CALL SKIPFILE (1)
READ (1),TITLE,ALIM,NBRS,NSRS,ITNSIF(ITTR,LT,0)READ 900,TITLE
IF (ALIM1,NE.0.0,AND,ALIM1,GT,ALIM) ALIM=PWRWF(10.0,(ALIM1/10.0))TFL-T 33
IF (ALIM1,EQ.0.0) ALIM1=10.0*ALBG10(ALIM) S PRINT 901,TITLE
IF (NSR1,NE.0.0,AND,NSR1,LT,NSRS) NSRS=NSR1
IF (NBR1,NE.0.0,AND,NBR1,LT,NBRS) NBRS=NBR1
PRINT 903,AL,ZMAX,NRMAX,IKNM,IFMC,NFSK,ITTR,ALIM1,NSRS,NBRS
IF (AL,LE.0.,OR,AL,GT,120.) STOP $ IF (ZMAX,LE.0.) STOP $ IL=1
IF (NRMAX,LE,0.0,NRMAX,GT,2000) STOP
5 IH=IL+19
IF (IH,GT,511) STOP
READ Y04,(NRPLOT(1),I=IL,IH)
PRINT 905,(NRPLOT(1),I=IL,IH)
IF (EOF,60) 10,15
10 IH=IL-1
GO TO 25
15 IF (NRPLOT(IH),EQ,0) GO TO 20
IL=IL+20
GO TO 5
20 IH=IH+1
IF (NRPLOT(IH),NE,0) GO TO 25
IF (IH,GT,0) GO TO 20
25 NODPLT IH
IF (IH,LE,0) STOP
LBLK=32*(512/NTPLT)
MULK=(NRMAX-1)/LBLK+1

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PHINT 906,NTOPLT,LBLK,MULK      TPLT 57
NDISK=MBLK=LBLK=NTOPLT=0        TPLT 58
IF (NDISK.GT,2*20) STOP        TPLT 59
IF (MBLK.EQ.1,0R,1) GO TO 30   TPLT 60
IDF#01                           TPLT 61
CALL UKOPEN(2,3HRAN,0)          TPLT 62
C     PLUT TITLE AND Z-AXIS    TPLT 63
30 CALL SYMBOL(1,,0,,14,TITLE,90,,80) TPLT 64
CALL SYMBOL(2,0,9,9,14,1HCG,0,,2) TPLT 65
Z#0,                            TPLT 66
DO J1 I=1,10                   TPLT 67
CALL PLOT(3,,11,-1,3)          TPLT 68
CALL PLOT(3,,10,-1,2)          TPLT 69
CALL PLOT(3,05,10,-1,2)         TPLT 70
CALL PLOT(2,95,10,-1,2)         TPLT 71
Z=Z+ZMAX/10,                   TPLT 72
CALL NUMBER(2,32,9,93-I,,14,Z,0,,4HF5,0) TPLT 73
IF (I,EQ.5,AND,IFMC,GE,0) CALL SYMBOL (2,,4.5,,14,9HDEPTH (H),90,, TPLT 74
19)                             TPLT 75
IF (I,EQ.5,AND,IFMC,LT,0) CALL SYMBOL (2,,4.5,,14,10HDEPTH (FT), TPLT 76
190,,10)                         TPLT 77
31 CONTINUE                      TPLT 78
IF (IFMC,LT,0) ZMAX=ZMAX=0,3U48 TPLT 79
NR=NRMAX                         TPLT 80
M=1                             TPLT 81
IREC=0                           TPLT 82
32 DO 50 IR=1,LBLK              TPLT 83
IREC=IREC+1 S IFEF=0            TPLT 84
READ(1) NHAY,HR(IREC),ZBKT(IREC),(TR(I),I=1,NHAY),(ZR(I),I=1,NRAY) TPLT 85
1,(SS()),I=1,NHAY),(NCOUNT(I),I=1,NRAY)                         TPLT 86
IF (EOF,1) 36,38                 TPLT 87
36 IFEF=1                        TPLT 88
IF (NRMAX,LT,IREC-1) GO TO 22  TPLT 89
NRMAX=IREC-1                    TPLT 90
NK=NRMAX                         TPLT 91
GO TO 52                         TPLT 92
38 IF (IOCHECK,1) 39,40           TPLT 93
39 PHINT 9039,IREC               TPLT 94
40 DO 45 I=1,NTOPLT & KENPBLT() SJBLBLK=(I-1)*IR + 7STOR(J)=ZR(K) TPLT 95
IF (NSRS.EQ,2500,AND,NSRS.EU,2500) GO TO 41 TPLT 96
NN=NCOUNT (K)SMMBNN/[INSNNMM/]TNNSR=MM-NN/[TN SMMBNN/]TNSNBR=MM TPLT 97
41 IF (SS(K),LE,ALIM,0H,NSH,GE,NSRS,0R,NBR,GE,NSRS) ZSTOR(J)=ZR(K) TPLT 98
IF (ZH(K),LT,0.0) ZSTOR(J)=ZR(K) TPLT 99
42 TSTOR(J)=TR(K)                TPLT 100
50 CONTINUE                      TPLT 101
51 IF (MBLK.EQ.1) GO TO 60 & IDEL=MULK=LBLK TPLT 102
MDISK=(M-1)*LBLK               TPLT 103
DO 55 I=1,NTOPLT                TPLT 104
CALL UKLOCATE(MDISK)             TPLT 105
J=(I-1)*LBLK+2                  TPLT 106
K=J+LBLK-1                      TPLT 107
CALL UKWRITE(ZSTOR(J),7STOR(K))  TPLT 108
MDISK=MDISK+1DEL                TPLT 109
CALL UKLOCATE(MDISK)             TPLT 110
CALL UKWRITE(TSTOR(J),TSTOR(K))  TPLT 111
55 MULK=MDISK+1DEL               TPLT 112

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60 IF(M,EQ,MBLK,0R,1FEF,EQ,1) GO TO 65          TPLT 113
M=M+1
GO TO 35
65 NREC=J2*(J1*RMAX-1)/J2+1                  TPLT 114
RMAX=RMAX(NH)
RSCALE=AL/RMAX
CALL PL0T0FT
IF(MBLK,EG,1) GO TO 80                      TPLT 115
IU=1
MLISK=0
DO 70 I=1,N,TPLT
CALL URLCATE(MDISK)
CALL LKREAD(TSTUR(1),LSTOH(NREC))           TPLT 116
MLISK=MDISK+1UFL
CALL URLCATE(MDISK)
CALL LKREAD(TSTUR(1),LSTOH(NREC))           TPLT 117
MLISK=MDISK+1UFL
CALL HAYPLCT(ZSTOR,TSIPH)
100=IU
70 GO TO 90
80 IU=1
DO 85 I=1,N,TPLT
L=(I-1)*LBLK+1
CALL HAYPLCT(ZSTOR(L),TSTUR(L))
85 IU=IU
90 CALL PL0T(AL+10.,0.,-3)                    TPLT 118
IF(1FEF,EG,1) GO TO 91  $ IREC=0              TPLT 119
91 IREC=IREC+1
READ(1) NRAY,HR(IREC),ZB0T(IREC),(TR(I),I=1,NRAY),(ZR(I),I=1,NRAY) TPLT 120
1,(SS(I)),(I=1,NRAY),(NFIINT(I)),(I=1,NRAY)
IF(EUF,1) 91,92                                TPLT 121
92 IF((IC0,LT,1TAC) GO TO 2                  TPLT 122
CALL STOPPL0T
STOP
END                                              TPLT 123
TPLT 124
TPLT 125
TPLT 126
TPLT 127
TPLT 128
TPLT 129
TPLT 130
TPLT 131
TPLT 132
TPLT 133
TPLT 134
TPLT 135
TPLT 136
TPLT 137
TPLT 138
TPLT 139
TPLT 140
TPLT 141
TPLT 142
TPLT 143
TPLT 144
TPLT 145
TPLT 146
TPLT 147

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, TRIPLET

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IDENT TRIPLET

| | |
|----------------|---------|
| PROGRAM LENGTH | 12/71 |
| ENTRY POINTS | TRIPLET |
| FILE NAMES | 11432 |
| | |
| INFO | U764/ |
| 1 | 4P00U |
| 2 | 4P00U |

EXTERNAL SYMBOLS

QCENTRY
 TEND,
 Q82STOP
 Q200700C
 Q1003106
 Q82DICT,
 PLGTS
 SKIPFILE
 CKOPEN
 SYMbal
 PLGTS
 NUMBER
 CKLOCATE
 CKWRITE
 PLAYBKT
 CKREAD
 PAYPLAT
 STCPPLAT
 AL@G10
 POWRF
 CACIFEGF
 CACIFEGC
 REW,
 TSH,
 TSQ,
 STM,
 SLI,
 QNSINGL,

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| | | |
|----|--|----------|
| | SUBROUTINE PLUTOT | TPLT 148 |
| | COMMON /INFO/ ID, NR, RMAX, ZMAX, RSCALE, AL, PR(2000), ZBOT(2000), IKNM | TPLT 149 |
| | NIMINIM1(AL+1,,40,5) | TPLT 150 |
| | R1=1. | TPLT 151 |
| | RMAN=RMAX | TPLT 152 |
| 50 | IF (IKNM,LT,0) RMAN=RMAX/1.852 | TPLT 153 |
| | NRMAN/RT | TPLT 154 |
| | IF (NT,LE,NTM) GO TO 51 | TPLT 155 |
| | R1=2.0RT | TPLT 156 |
| | NRMAN/RT | TPLT 157 |
| | IF (NT,LE,NTM) GO TO 51 | TPLT 158 |
| | R1=2.0RT | TPLT 159 |
| | NRMAN/RT | TPLT 160 |
| | IF (NT,LE,NTM) GO TO 51 | TPLT 161 |
| | R1=2.0RT | TPLT 162 |
| | GO TO 56 | TPLT 163 |
| C | PLUT SURFACE AXIS | TPLT 164 |
| 51 | CALL PLUT(3.,10.,,3) | TPLT 165 |
| | X=3, | TPLT 166 |
| | RSCALE1=RSCALE | TPLT 167 |
| | IF (IKNM,LT,0) RSCALE1=1.852*RSCALE | TPLT 168 |
| | DX=RT*RSCALE1 | TPLT 169 |
| | R=0, | TPLT 170 |
| | IF #0 | TPLT 171 |
| 52 | CALL PLUT(X,10.,,2) | TPLT 172 |
| | CALL PLUT(X,9.95,2) | TPLT 173 |
| | RK=R/1000, | TPLT 174 |
| | CALL NUMBER(X-.24,10.05,,4E-1,RK,0,,4WF4,0) | TPLT 175 |
| | IF (R,LT,RMAN/2.) GO TO 59 | TPLT 176 |
| | IF (IF,EQ,1) GO TO 59 | TPLT 177 |
| | IF (IKNM,LT,0) CALL SYMBOL(X-.3U,10.25,,14,10HRANGE (NM),0,,10) | TPLT 178 |
| | IF (IKNM,GE,0) CALL SYMBOL(X-.3U,10.25,,14,10HRANGE (KM),0,,10) | TPLT 179 |
| | IF #1 | TPLT 180 |
| 53 | CALL PLUT(X,10.,,3) | TPLT 181 |
| | IF (R,GE,RMAN) GO TO 60 | TPLT 182 |
| | X=X+DX | TPLT 183 |
| | R=R+RT | TPLT 184 |
| | GO TO 58 | TPLT 185 |
| C | PLUT PTTAM CONTOUR | TPLT 186 |
| 60 | DO 63 I=1,NR | TPLT 187 |
| | K=NR+1-I | TPLT 188 |
| | Y=10.*((1.-ZBOT(K))/ZMAX) | TPLT 189 |
| | X=RR(K)*RSCALE+3. | TPLT 190 |
| | IP#2 | TPLT 191 |
| | IF (I,EQ,1) IP#3 | TPLT 192 |
| | IF (Y,GE,0,) GO TO 63 | TPLT 193 |
| | IP#3 | TPLT 194 |
| | Y=0, | TPLT 195 |
| 63 | CALL PLUT(X,",IP) | TPLT 196 |
| | RETURN | TPLT 197 |
| | END | TPLT 198 |

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S PLOTBOT

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IDENT PLOTBOT

| | |
|------------------|---------|
| PROGRAM LENGTH | U0303 |
| ENTRY POINTS | PLOTBOT |
| BLOCK NAMES | U0010 |
| INFO | U7647 |
| EXTERNAL SYMBOLS | |
| 01010100 | |
| QQUICKT, | |
| PLOT | |
| NUMBER | |
| SYMBOL | |
| MINIF | |

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SUBROUTINE RAYPLAT(ZSTAR,ISTAR) TPLT 199
DIMENSION ZSTAR(2000),TSTAR(2000) TPLT 200
DIMENSION Z(25),R(25) TPLT 201
COMMON /INFO/ ID,NR,MAX,ZMAX,RSCALE,AL,RH(2000),ZBOT(2000),IKNM TPLT 202
NID=1 S IRHS=1 IPHS=1 IHT=1 SIRI=0 S IST=0 SJT=0 TPLT 203
IF(ID,LT.0) NIDENH S IF (NID,NE,1) IPR=1 TPLT 204
Z=BSHSE(ZSTAR(NID)) S IF (ZSTAR(1),LT,0.0) RETURN TPLT 205
T=ZSTAR(NID) TPLT 206
RSHR(NID) TPLT 207
ZB=ZBOT(NID) TPLT 208
X=RSHSCALE S IF (ZB,G1,ZB) ZB=ZB TPLT 209
Y=1.0*(1.-ZB/ZMAX) TPLT 210
IF(Y,LT.0,) Y=0. TPLT 211
CALL PLOT(X+3.,Y,3) TPLT 212
DO 90 LL=2,NR TPLT 213
IF(ID,GT,0) GO TO 73 TPLT 214
L=NID-LL+1 TPLT 215
GO TO 74 TPLT 216
73 L=LL TPLT 217
74 ZN=BSHSE(ZSTAR(L)) S TN=TSTAR(L) SRN=RR(L) SZBN=ZBOT(L) SDR=RN-R0 TPLT 218
IF(ZN,GT,ZBN) ZN=ZN S IF (ZSTAR(L),LT,0.0,AND,IPR,E0,1) 91,93 TPLT 219
93 IF (NID,NE,1,AND,IRH,E0,0) 94,95 TPLT 220
94 X=RSHSCALE YY=1.0*(1.-ZB/ZMAX) S IF (Y,LT.0,) Y=0.0 TPLT 221
CALL PLOT (X+3.,Y,3) S IRHS=1 S IPR=0 SIRI=1 S IF (ZSTAR(L+1),GE,0,) IST=1 TPLT 222
95 ZN=ZV-DR*TN TPLT 223
ZU=ZU+DR*T0 TPLT 224
IF (ZNU,GE,0,) GO TO 75 TPLT 225
IF (ZNU,GE,0,) GO TO 75 TPLT 226
ZB=-ZB TPLT 227
ZNU=ZPN TPLT 228
T0=T0 TPLT 229
75 TB=(ZB-ZB)/DR TPLT 230
IF (ZNB,LE,ZB) GO TO 78 TPLT 231
IF (ZDN,LE,ZB) GO TO 78 TPLT 232
IF (TB,EQ,0.) GO TO 76 TPLT 233
DZ=ZB-ZB TPLT 234
ZU=ZB+0.0Z/(1.+TB*0.2) TPLT 235
RSHR=ZB+0.0Z/(TB+1./TP) TPLT 236
T0=(TB-TB)/(1.+TB*TB) TPLT 237
T0=(TB-TB)/(1.+TB*TB) TPLT 238
GO TO 77 TPLT 239
76 ZU=2.*ZB-ZB TPLT 240
T0=T0 TPLT 241
77 DR=RN-R0 TPLT 242
ZU=ZU+DR*T0 TPLT 243
ZN=ZV-DR*TN TPLT 244
78 DX=ABS(DR*RSCALE) TPLT 245
N=DX/.02+.2 TPLT 246
C INTERPOLATION TO FIFTIETHS WILL BE DONE TPLT 247
IF (N,GT,25) N=25 TPLT 248
I1=1 TPLT 249
DI=1./(N-1) TPLT 250
F=0. TPLT 251
C SPLINE FIT BY CONTINUED LINEAR INTERPOLATION TPLT 252
DZ=ZB-ZB TPLT 253
DZ=ZB-N-76 TPLT 254

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DZN=ZN-RZN
74 Z1=Z0+F*DZ
Z2=Z0+F*DZ
Z3=Z0+F*DZ
G=1,-1
Z4=G*Z2+F*Z1
Z5=G*Z1+F*Z3
Z(II)=G*Z4+F*Z5
R(II)=R0+F*DR
II=II+1
F=F+DF
IF(II,LE,N) GO TO 79
DF=0.9 II=1,N
IN=0
IF(Z(II).LT.0.) IN=1
IF(Z(II).GT.ZBN*(R(II)-RN)*TB) IN=-1
IF(II,EQ,1) GO TO 82
IF(IN,EQ,10) GO TO 82
IF(IN,NE,1,AND,10,NE,1) GO TO 80
RHIT=,9*(H(II)+4*(II-1)*(R(II)-R(II-1))*(Z(II)+Z(II-1))/(Z(II)-1)-Z(TPLT 274
1II)))
X=RHIT*RSCALE$IP=3$IF (IBT,EO,1,0R,NID,EO,1,0R,IST,EC,1) IP=2$IR=1 TPLT 275
CALL PLOT(X+3.,10,IP)$ IF (7STOR(L),GE,0,0) GO TO 82 5 IPR=1 TPLT 276
GO TO 91 TPLT 277
80 D=(Z(II)-Z(II-1))/(H(II)-H(II-1))-TB TPLT 278
RHIT=(Z(II-1)-ZBN*(H(II-1)-RN)*TR)/D+R(II-1) TPLT 279
F=(RHIT-R(II-1))/(R(II)-R(II-1)) TPLT 280
IF(F,GT,1,) GO TO 82 TPLT 281
IF(F,LT,0,) GO TO 82 TPLT 282
X=RHIT*RSCALE$IP=3$IF (IBT,EO,1,0R,NID,FQ,1,0R,IST,FQ,1) IP=2 TPLT 283
IR=1 TPLT 284
Y=10.*(1.-(ZBN*(RHIT-RN)*TR)/ZMAX)$IF (7STOR(L),LT,0,0) IPR=1 TPLT 285
IF(Y,GT,0,) GO TO 81 TPLT 286
Y=0, TPLT 287
IP=3 TPLT 288
81 CALL PLOT(X+3.,Y,IP) TPLT 289
82 IF(Z(II).GT,0.) GO TO 83 TPLT 290
Y=10.*(1.+Z(II)/ZMAX) TPLT 291
X=R(II)*RSCALE$IF (Z(II),EO,0,0,AND,IP,EO,1) IJT=1 TPLT 292
IF (Z(II),EQ,0,0,AND,ZSTOR(L),LT,0,0) IPR=1 $ GO TO 86 TPLT 293
83 IF(Z(II).GT,ZBN*(H(II)-RN)*TB) GO TO 84 TPLT 294
Y=10.*(1.-Z(II)/ZMAX)$IF (Z(II),EQ,ZBN*(R(II)-RN)*TR,AND,ZSTOR(L),LT) TPLT 295
1T,0,0) IPR=1 TPLT 296
X=R(II)*RSCALE$IF (Z(II),EO,ZBN*(R(II)-RN)*TR,AND,IP,EO,1) IJT=1 TPLT 297
GO TO 86 TPLT 298
84 DZ=Z(II)-(ZBN*(H(II)-RN)*TB) TPLT 299
Z=Z(II)-2.*DZ/(1.+TB**2) $ RH=R(II) TPLT 300
IF(TB,NE,0,) RRP=RP+2.*DZ/(TB+1./TB) $ Y=10.*(1.-ZP/ZMAX) TPLT 301
IF(ZP,EQ,ZBN*(RP-RN)*IR,AND,ZSTOR(L),LT,0,0) IPR=1 TPLT 302
IF(ZP,EQ,ZBN*(RP-RN)*IR,AND,IR,EO,1) IJT=1 $ X=RP*RSCALE TPLT 303
IF (IBT,EO,1,AND,NID,NE,1,0R,IST,EO,1) GO TO 86 TPLT 304
IF (NID,NE,1) GO TO 107 TPLT 305
IF (IPR,EO,1,0R,ZSTOR(L),GE,0,0) GO TO 86 TPLT 306
187 IF (II,EO,4) GO TO 108 TPLT 307
DZS=Z(II+1)-(ZBN*(R(II+1)-RN)*TB) TPLT 308
ZHS=Z(II+1)-2.*DZS/(1.+TB**2) TPLT 309
TPLT 310

```

B. G. ROBERTS

5A

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| | |
|---|----------|
| IF (ZP.GE,ZPS.AND,NID.EQ.1,UR,DZS.LE.0.0.AND,NID,EQ,1) IPR=1 | TPLT 311 |
| IF (ZP.GE,ZPS.AND,NID.NE.1,UR,DZS.LE.0.0.AND,NID,NE,1) IJT=1 | TPLT 312 |
| G0 T0 86 | TPLT 313 |
| 106 IF (IPR.EQ.0.AND,ZSTM(L).LT.0,0) IPR=1 | TPLT 314 |
| IF (INT.EQ.0.AND,ZSTM(L+1).LT.0,0.AND,NID,NE,1) IJT=1 | TPLT 315 |
| 86 IP=2 | TPLT 316 |
| IF(Y.LT.10.,AND,Y,GT.0.) G0 T0 87 | TPLT 317 |
| IP=3 | TPLT 318 |
| Y=AMIN1(10.,AMAX1(Y,0.)) | TPLT 319 |
| IF(X.LT.AL+1.,AND,X,GE,-.01) G0 T0 88 | TPLT 320 |
| IP=3 | TPLT 321 |
| X=AMIN1(AL+1.,AMAX1(X,0.)) | TPLT 322 |
| 88 IF (INT.E,0.AND,IRI,E0.1.AND,IST,E0.0)IP=3 S CALL PLOT(X+3,,Y,[P])TPLT 323 | |
| I0=IN S IF(IJT,EQ,1) IBT=1 S IF (IPR,EQ,1) G0 T0 91 | TPLT 324 |
| 89 CONTINUE | TPLT 325 |
| 91 ZM0=ZN S ZB=ZN | TPLT 326 |
| T0=TN | TPLT 327 |
| R0=RN | TPLT 328 |
| RETURN | TPLT 329 |
| END | TPLT 330 |

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> RAYPLOT

04/05/78

ED 0

IDENT RAYPLOT

| | |
|------------------|----------|
| PROGRAM LENGTH | 01371 |
| ENTRY POINTS | RAYPLOT |
| BLOCK NAMES | UC062 |
| INFO | U7641 |
| EXTERNAL SYMBOLS | |
| | 01010100 |
| | 0800ICT. |
| | PLST |
| | MIN1F |
| | MAX1F |

Appendix B

COMPARISON OF CALCULATED AND EXPERIMENTAL RESULTS

A comparison was made between the calculated results from TRIMAIN and some experimental data which was furnished by Cdr. P.R. Tatro of the Maury Center for Ocean Science. The input parameters for TRIMAIN were: a frequency of 100 hertz and no volume attenuation, a fan of rays between $\pm 60^\circ$ in 1° steps, a bottom loss of MGS class IV for the entire track, type II intensity calculations, a source depth of 152.4 meters and a receiver depth of 762.0 meters. Figs. B1a, B1b, and B1c are print plots of input sound-speed profiles, Fig. B2 is a Calcomp plot of profiles and the bottom track, Fig. B3a is a list of calculated intensity values, Fig. B3b is a list of experimental intensity values, Fig. B4 is a Calcomp plot of selected rays which were traced (one ray every 15°), and Fig. B5 is a Calcomp comparison of experimental and calculated intensity values. Good agreement exists between the two sets of values.

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| INPUT PROFILE AT 5 KM | | OUTPUT AT | | FIRST PROFILE | |
|-----------------------|--------------|-----------|------|---------------|------|
| EFPM (°) | VLLCITY71460 | 1470 | 1480 | 1490 | 1500 |
| 0.0000 | 1532,1033 | | | | |
| 31.0001 | 1532,6254 | | | | |
| 40.0002 | 1532,7701 | | | | |
| 20.0002 | 1531,5967 | | | | |
| 25.0003 | 1531,6402 | | | | |
| 61.0003 | 1533,1434 | | | | |
| 70.0004 | 1533,1270 | | | | |
| 75.0005 | 1533,3936 | | | | |
| 80.0005 | 1532,14575 | | | | |
| 69.0006 | 1531,5214 | | | | |
| 91.0007 | 1529,1346 | | | | |
| 122.0014 | 1522,1424 | | | | |
| 182.0026 | 1524,15770 | | | | |
| 244.0047 | 1504,1090 | | | | |
| 365.0105 | 1459,3854 | | | | |
| 400.0125 | 1456,17253 | | | | |
| 600.0242 | 1455,14363 | | | | |
| 800.0552 | 1451,17446 | | | | |
| 1600.074 | 1482,16451 | | | | |
| 1500.1764 | 1486,12934 | | | | |
| 2000.3136 | 1451,17224 | | | | |
| 2500.4901 | 1459,12637 | | | | |
| 3000.7058 | 1506,12274 | | | | |
| 3500.9607 | 1516,4107 | | | | |
| 4001.2548 | 1525,77042 | | | | |
| 5000.9608 | 1543,12634 | | | | |
| 8000.0213 | 1599,10338 | | | | |

Fig. B1a — Input profile at 0 km

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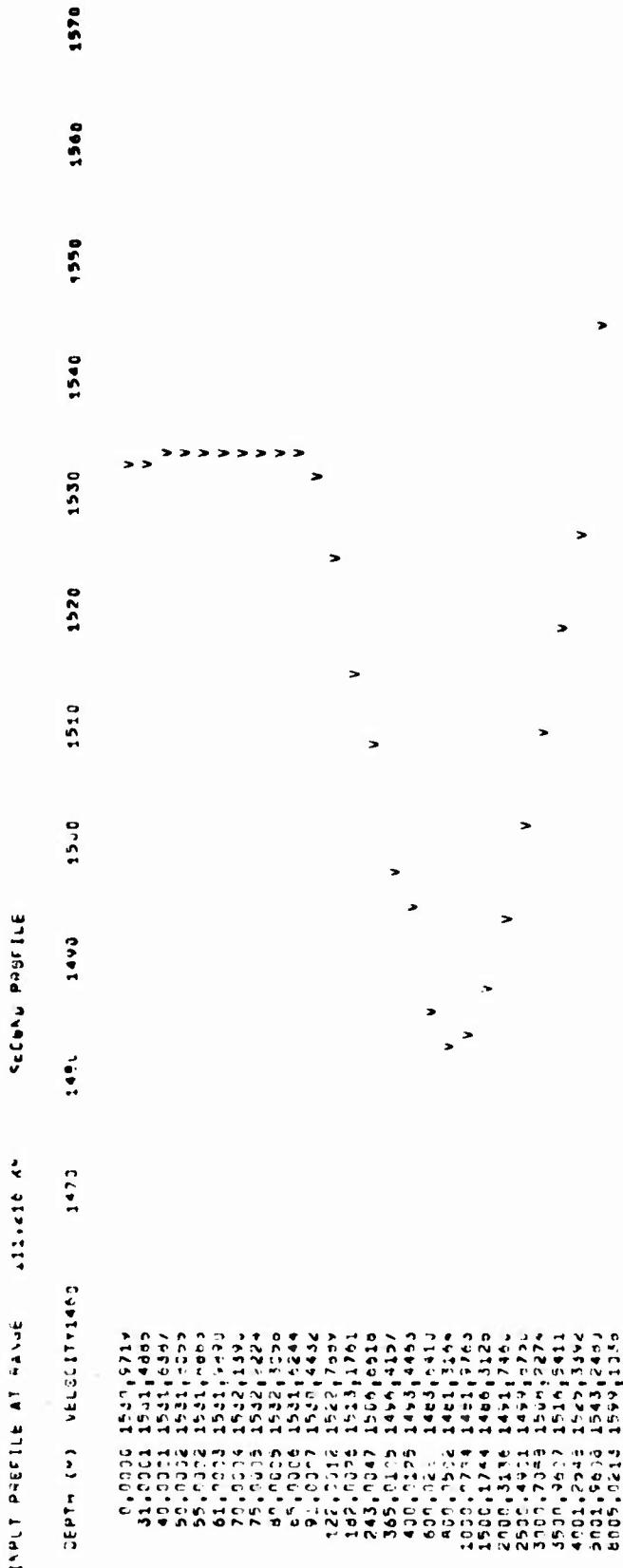


Fig. B1b — Input profile at 111.216 km

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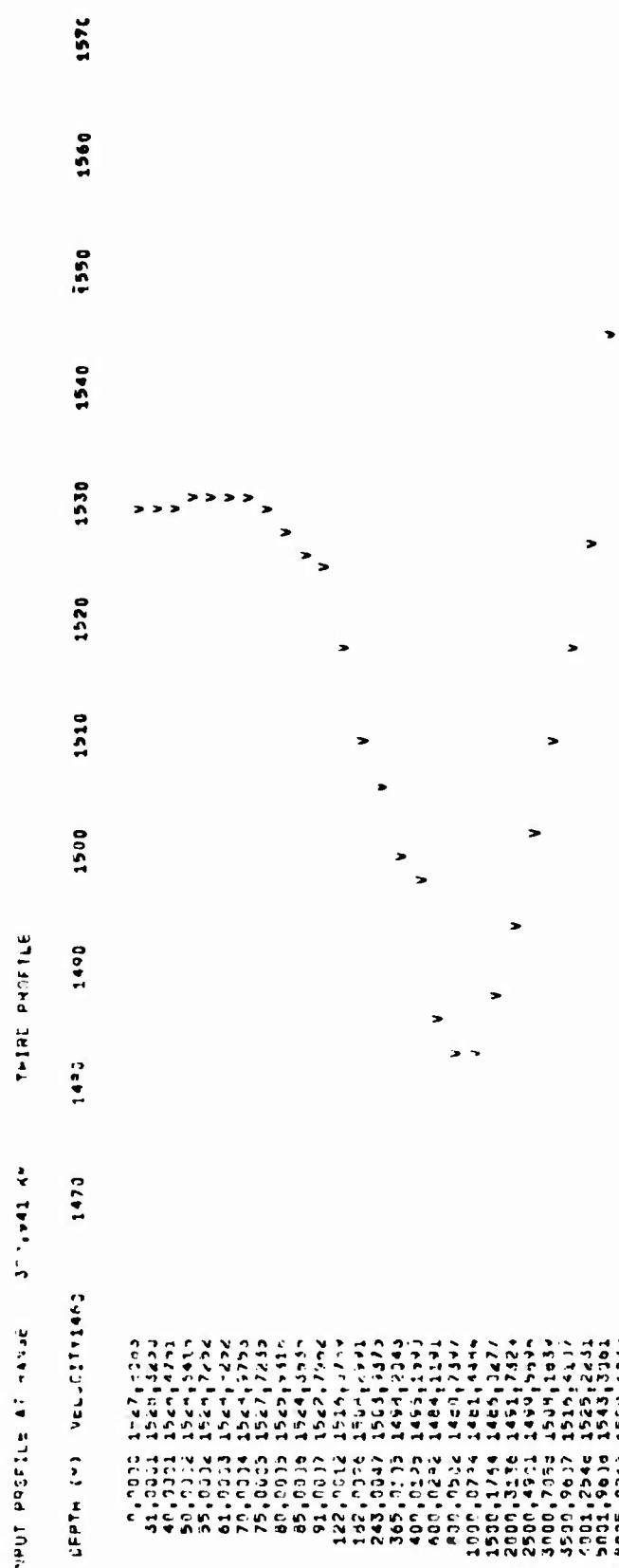


Fig. B1c — Input: Profile at 329941 km

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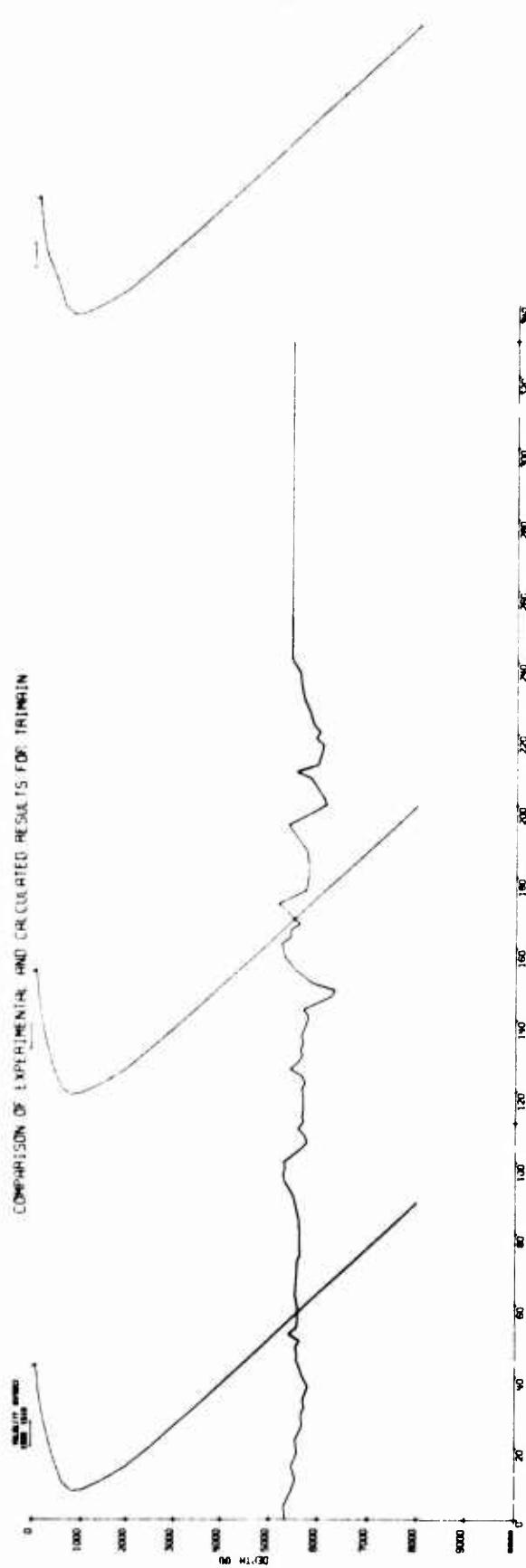


Fig. B2 — Profiles and Bottom Track

Reproduced from
best available copy.

| CALCULATION RANGE | RESULTS LINES | 00,000 | | 00,000 | | 00,000 | | 00,000 | | 00,000 | | 00,000 | |
|-------------------|---------------|---------|---------|---------|--------|---------|---------|---------|---------|---------|---------|---------|--------|
| | | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 | 00,000 |
| 1,000 | 28,000 | 67,000 | 89,000 | 127,000 | 92,000 | 126,000 | 91,000 | 102,000 | 98,700 | 298,000 | 104,000 | 106,100 | |
| 2,000 | 63,400 | 66,000 | 90,000 | 134,000 | 63,400 | 127,000 | 92,300 | 102,000 | 100,300 | 299,000 | 106,100 | 105,400 | |
| 3,000 | 66,600 | 66,000 | 92,000 | 135,000 | 66,600 | 94,000 | 94,000 | 104,000 | 102,400 | 200,000 | 102,000 | 104,000 | |
| 4,000 | 68,500 | 70,000 | 92,700 | 134,000 | 68,500 | 94,000 | 101,400 | 102,000 | 103,900 | 201,000 | 103,000 | 103,300 | |
| 5,000 | 69,700 | 71,000 | 92,400 | 137,000 | 69,700 | 92,400 | 102,400 | 103,000 | 106,200 | 202,000 | 103,000 | 103,300 | |
| 6,000 | 76,400 | 72,000 | 92,000 | 138,000 | 76,400 | 93,000 | 103,000 | 104,000 | 107,400 | 203,000 | 104,000 | 104,300 | |
| 7,000 | 83,200 | 73,000 | 92,000 | 138,000 | 83,200 | 93,000 | 105,000 | 105,000 | 106,500 | 205,000 | 106,500 | 106,500 | |
| 8,000 | 85,800 | 74,000 | 92,000 | 140,000 | 85,800 | 94,000 | 107,000 | 106,000 | 108,600 | 206,000 | 107,200 | 106,200 | |
| 9,000 | 87,400 | 75,000 | 94,000 | 141,000 | 87,400 | 95,000 | 107,000 | 107,000 | 108,800 | 207,000 | 106,900 | 107,000 | |
| 10,000 | 83,400 | 76,000 | 93,500 | 142,000 | 83,400 | 95,700 | 106,500 | 108,000 | 109,800 | 208,000 | 105,800 | 106,100 | |
| 11,000 | 87,100 | 77,000 | 92,300 | 143,000 | 87,100 | 96,000 | 108,000 | 109,000 | 108,000 | 207,400 | 107,000 | 107,000 | |
| 12,000 | 87,000 | 78,000 | 92,300 | 144,000 | 87,000 | 96,000 | 110,000 | 111,000 | 109,000 | 206,000 | 107,200 | 106,600 | |
| 13,000 | 87,400 | 79,000 | 93,000 | 145,000 | 87,400 | 96,000 | 112,400 | 111,000 | 110,000 | 207,000 | 107,600 | 107,000 | |
| 14,000 | 87,200 | 80,000 | 95,300 | 146,000 | 87,200 | 96,000 | 110,700 | 112,000 | 111,000 | 208,000 | 108,000 | 107,700 | |
| 15,000 | 87,400 | 81,000 | 95,000 | 147,000 | 87,400 | 96,000 | 117,400 | 118,000 | 117,000 | 207,000 | 108,800 | 107,400 | |
| 16,000 | 87,500 | 82,000 | 94,000 | 148,000 | 87,500 | 96,000 | 106,100 | 114,000 | 116,000 | 206,000 | 109,000 | 107,400 | |
| 17,000 | 87,100 | 83,000 | 96,000 | 146,000 | 87,100 | 96,000 | 106,000 | 114,000 | 116,000 | 206,000 | 109,000 | 107,400 | |
| 18,000 | 87,700 | 84,000 | 98,000 | 151,000 | 87,700 | 96,000 | 104,100 | 116,000 | 119,000 | 207,000 | 109,000 | 109,000 | |
| 19,000 | 87,400 | 85,000 | 98,000 | 151,000 | 87,400 | 96,000 | 101,400 | 117,000 | 121,000 | 207,000 | 109,000 | 109,000 | |
| 20,000 | 86,700 | 86,000 | 100,000 | 152,000 | 86,700 | 96,000 | 98,000 | 118,000 | 121,000 | 208,000 | 109,000 | 109,000 | |
| 21,000 | 86,100 | 87,000 | 103,000 | 153,000 | 86,100 | 97,000 | 97,000 | 116,000 | 121,000 | 208,000 | 109,000 | 109,000 | |
| 22,000 | 86,200 | 88,000 | 103,000 | 154,000 | 86,200 | 97,400 | 97,400 | 120,000 | 122,000 | 209,000 | 109,000 | 109,000 | |
| 23,000 | 86,100 | 89,000 | 102,000 | 155,000 | 86,100 | 96,300 | 96,300 | 121,000 | 122,000 | 209,000 | 109,000 | 109,000 | |
| 24,000 | 86,200 | 90,000 | 100,000 | 156,000 | 86,200 | 96,000 | 94,600 | 121,000 | 122,000 | 209,000 | 109,000 | 109,000 | |
| 25,000 | 86,700 | 91,000 | 101,000 | 157,000 | 86,700 | 96,000 | 92,600 | 122,000 | 123,000 | 209,000 | 109,000 | 109,000 | |
| 26,000 | 86,600 | 92,000 | 104,000 | 158,000 | 86,600 | 96,000 | 90,000 | 124,000 | 124,000 | 209,000 | 109,000 | 109,000 | |
| 27,000 | 86,500 | 93,000 | 106,700 | 159,000 | 86,500 | 96,000 | 90,700 | 125,000 | 125,000 | 209,000 | 109,000 | 109,000 | |
| 28,000 | 86,900 | 94,000 | 107,500 | 160,000 | 86,900 | 96,000 | 90,000 | 126,000 | 126,000 | 209,000 | 109,000 | 109,000 | |
| 29,000 | 86,400 | 95,000 | 104,000 | 161,000 | 86,400 | 96,000 | 90,000 | 127,000 | 127,000 | 209,000 | 109,000 | 109,000 | |
| 30,000 | 86,400 | 96,000 | 105,000 | 162,000 | 86,400 | 96,000 | 90,000 | 128,000 | 128,000 | 209,000 | 109,000 | 109,000 | |
| 31,000 | 86,700 | 97,000 | 103,000 | 163,000 | 86,700 | 96,000 | 90,000 | 129,000 | 129,000 | 209,000 | 109,000 | 109,000 | |
| 32,000 | 86,000 | 98,000 | 104,000 | 164,000 | 86,000 | 96,000 | 90,000 | 130,000 | 130,000 | 209,000 | 109,000 | 109,000 | |
| 33,000 | 86,700 | 99,000 | 98,000 | 165,000 | 86,700 | 96,000 | 90,000 | 131,000 | 130,000 | 209,000 | 109,000 | 109,000 | |
| 34,000 | 86,100 | 100,000 | 95,000 | 166,000 | 86,100 | 96,000 | 90,000 | 132,000 | 130,000 | 209,000 | 109,000 | 109,000 | |
| 35,000 | 87,100 | 101,000 | 93,000 | 167,000 | 87,100 | 96,000 | 90,000 | 133,000 | 131,000 | 209,000 | 109,000 | 109,000 | |
| 36,000 | 87,000 | 102,000 | 91,000 | 168,000 | 87,000 | 96,000 | 90,000 | 134,000 | 131,000 | 209,000 | 109,000 | 109,000 | |
| 37,000 | 87,200 | 103,000 | 90,000 | 169,000 | 87,200 | 96,000 | 90,000 | 135,000 | 132,000 | 209,000 | 109,000 | 109,000 | |
| 38,000 | 87,600 | 104,000 | 88,500 | 170,000 | 87,600 | 96,000 | 90,000 | 136,000 | 132,000 | 209,000 | 109,000 | 109,000 | |
| 39,000 | 87,600 | 105,000 | 87,000 | 171,000 | 87,600 | 96,000 | 90,000 | 137,000 | 132,000 | 209,000 | 109,000 | 109,000 | |
| 40,000 | 87,900 | 104,000 | 87,000 | 172,000 | 87,900 | 96,000 | 91,700 | 138,000 | 132,000 | 209,000 | 109,000 | 109,000 | |
| 41,000 | 87,900 | 107,000 | 87,000 | 173,000 | 87,900 | 96,000 | 92,500 | 138,000 | 132,000 | 209,000 | 109,000 | 109,000 | |
| 42,000 | 88,500 | 108,000 | 87,700 | 174,000 | 88,500 | 96,000 | 93,300 | 139,000 | 133,000 | 209,000 | 109,000 | 109,000 | |
| 43,000 | 89,500 | 106,000 | 87,000 | 175,000 | 89,500 | 96,000 | 94,500 | 139,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 44,000 | 89,000 | 110,000 | 87,000 | 176,000 | 89,000 | 96,000 | 95,000 | 139,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 45,000 | 89,100 | 111,000 | 87,300 | 177,000 | 89,100 | 96,000 | 95,400 | 139,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 46,000 | 89,200 | 112,000 | 87,100 | 178,000 | 89,200 | 96,000 | 95,300 | 139,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 47,000 | 89,300 | 113,000 | 86,900 | 176,000 | 89,300 | 96,000 | 95,500 | 139,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 48,000 | 89,700 | 114,000 | 87,100 | 180,000 | 89,700 | 96,000 | 93,200 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 49,000 | 89,200 | 115,000 | 87,100 | 181,000 | 89,200 | 96,000 | 93,500 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 50,000 | 89,400 | 116,000 | 87,200 | 182,000 | 89,400 | 96,000 | 93,200 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 51,000 | 89,300 | 117,000 | 87,000 | 183,000 | 89,300 | 96,000 | 92,800 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 52,000 | 89,400 | 118,000 | 87,500 | 184,000 | 89,400 | 96,000 | 93,100 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 53,000 | 89,700 | 119,000 | 88,000 | 185,000 | 89,700 | 96,000 | 93,300 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 54,000 | 89,800 | 120,000 | 88,800 | 186,000 | 89,800 | 96,000 | 93,200 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 55,000 | 89,100 | 121,000 | 90,300 | 187,000 | 89,100 | 96,000 | 93,500 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 56,000 | 89,400 | 122,000 | 90,700 | 188,000 | 89,400 | 96,000 | 95,000 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 57,000 | 89,600 | 123,000 | 91,000 | 189,000 | 89,600 | 96,000 | 96,100 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 58,000 | 89,200 | 124,000 | 91,100 | 190,000 | 89,200 | 96,000 | 97,900 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |
| 59,000 | 89,200 | 125,000 | 91,200 | 191,000 | 89,200 | 96,000 | 97,100 | 140,000 | 134,000 | 209,000 | 109,000 | 109,000 | |

Fig. B3a – Calculated intensity values

| | | | | | |
|-------------------------------|--------|---------|---------|---------|---------|
| EXPERIMENTAL RESULTS
RANGE | LOSSES | 98,567 | 92,750 | 210,979 | 95,370 |
| | | 96,758 | 96,120 | 212,512 | 94,500 |
| | | 102,441 | 96,500 | 216,256 | 96,500 |
| | | 104,113 | 95,870 | 217,427 | 95,750 |
| | | 105,345 | 96,820 | 218,959 | 97,620 |
| | | 106,756 | 98,270 | 220,370 | 97,620 |
| | | 108,128 | 91,880 | 221,742 | 98,420 |
| 2,515 | 97,630 | 106,499 | 97,500 | 223,114 | 98,420 |
| 3,166 | 92,250 | 111,871 | 93,620 | 224,485 | 94,750 |
| 5,752 | 92,140 | 112,243 | 92,000 | 225,857 | 96,500 |
| 6,449 | 93,130 | 113,614 | 91,250 | 227,228 | 98,500 |
| 6,761 | 90,650 | 114,986 | 91,120 | 230,260 | 100,120 |
| 6,773 | 91,880 | 116,757 | 99,500 | 231,572 | 96,120 |
| 10,744 | 93,770 | 117,939 | 97,120 | 232,943 | 94,870 |
| 12,115 | 96,000 | 119,210 | 95,000 | 234,315 | 97,000 |
| 13,487 | 95,770 | 120,582 | 92,870 | 235,487 | 96,620 |
| 14,859 | 92,620 | 121,954 | 98,870 | 237,158 | 97,750 |
| 16,781 | 96,500 | 123,765 | 93,770 | 238,430 | 102,250 |
| 19,460 | 96,750 | 124,497 | 94,260 | 239,801 | 102,370 |
| 21,731 | 94,970 | 126,768 | 104,120 | 241,173 | 104,500 |
| 22,463 | 97,750 | 127,440 | 108,370 | 242,545 | 99,380 |
| 23,714 | 98,250 | 128,912 | 111,120 | 243,916 | 97,750 |
| 25,146 | 97,700 | 130,183 | 113,120 | 246,288 | 103,250 |
| 26,518 | 98,000 | 131,555 | 112,620 | 246,631 | 104,750 |
| 27,869 | 99,500 | 133,907 | 114,370 | 251,103 | 104,250 |
| 29,261 | 91,120 | 136,246 | 110,750 | 252,374 | 103,370 |
| 30,432 | 98,870 | 137,617 | 110,500 | 253,746 | 101,620 |
| 32,704 | 98,250 | 138,969 | 109,620 | 255,118 | 102,000 |
| 33,376 | 97,750 | 140,360 | 112,250 | 256,469 | 102,250 |
| 36,576 | 96,620 | 141,732 | 111,500 | 257,961 | 101,250 |
| 37,248 | 98,770 | 143,104 | 112,120 | 258,242 | 99,120 |
| 39,719 | 91,880 | 144,475 | 111,750 | 260,404 | 97,370 |
| 41,441 | 90,750 | 145,847 | 111,500 | 262,850 | 97,700 |
| 42,762 | 91,500 | 147,218 | 110,370 | 264,262 | 98,370 |
| 43,234 | 92,250 | 149,776 | 107,500 | 265,633 | 98,500 |
| 46,177 | 92,500 | 150,447 | 105,750 | 267,065 | 99,250 |
| 47,549 | 91,750 | 152,119 | 101,370 | 268,376 | 99,500 |
| 48,260 | 97,620 | 153,391 | 99,750 | 269,748 | 99,380 |
| 52,761 | 91,120 | 154,762 | 98,120 | 271,160 | 98,130 |
| 55,043 | 90,700 | 157,505 | 97,370 | 272,431 | 97,120 |
| 56,464 | 92,000 | 158,977 | 96,000 | 273,963 | 97,000 |
| 57,936 | 93,500 | 160,249 | 93,130 | 275,234 | 98,370 |
| 62,746 | 98,750 | 161,420 | 93,250 | 276,406 | 100,250 |
| 64,118 | 94,380 | 162,942 | 93,500 | 283,117 | 96,750 |
| 65,449 | 98,620 | 166,378 | 95,120 | 284,488 | 96,120 |
| 66,270 | 96,700 | 168,250 | 94,120 | 285,860 | 99,380 |
| 68,263 | 94,120 | 170,953 | 93,250 | 287,241 | 99,500 |
| 69,723 | 95,370 | 172,764 | 92,500 | 288,612 | 98,620 |
| 71,095 | 97,370 | 173,735 | 92,420 | 289,975 | 101,870 |
| 72,466 | 97,370 | 175,108 | 94,120 | 291,346 | 103,500 |
| 75,269 | 95,370 | 176,479 | 97,870 | 292,718 | 101,750 |
| 76,561 | 98,370 | 177,951 | 93,500 | 294,089 | 99,500 |
| 77,953 | 95,120 | 179,222 | 95,120 | 295,461 | 97,750 |
| 79,324 | 96,480 | 180,594 | 97,380 | 298,760 | 102,120 |
| 80,496 | 98,000 | 182,764 | 98,130 | 300,152 | 106,120 |
| 82,167 | 97,870 | 185,166 | 93,130 | 301,523 | 102,470 |
| 82,469 | 98,130 | 186,538 | 98,500 | 302,895 | 98,250 |
| 86,182 | 98,000 | 198,535 | 102,500 | 304,267 | 96,250 |
| 87,554 | 96,980 | 199,306 | 102,520 | 305,638 | 99,870 |
| 88,945 | 96,500 | 201,278 | 102,520 | 307,010 | 100,420 |
| 90,297 | 98,130 | 202,449 | 101,620 | | |
| 91,669 | 98,500 | 204,021 | 102,500 | | |
| 92,040 | 99,500 | 205,393 | 99,370 | | |
| 94,412 | 98,420 | 206,764 | 96,980 | | |
| 95,783 | 93,770 | 208,136 | 95,970 | | |
| 97,155 | 98,750 | 209,507 | 95,500 | | |

Fig. B3b — Experimental intensity values

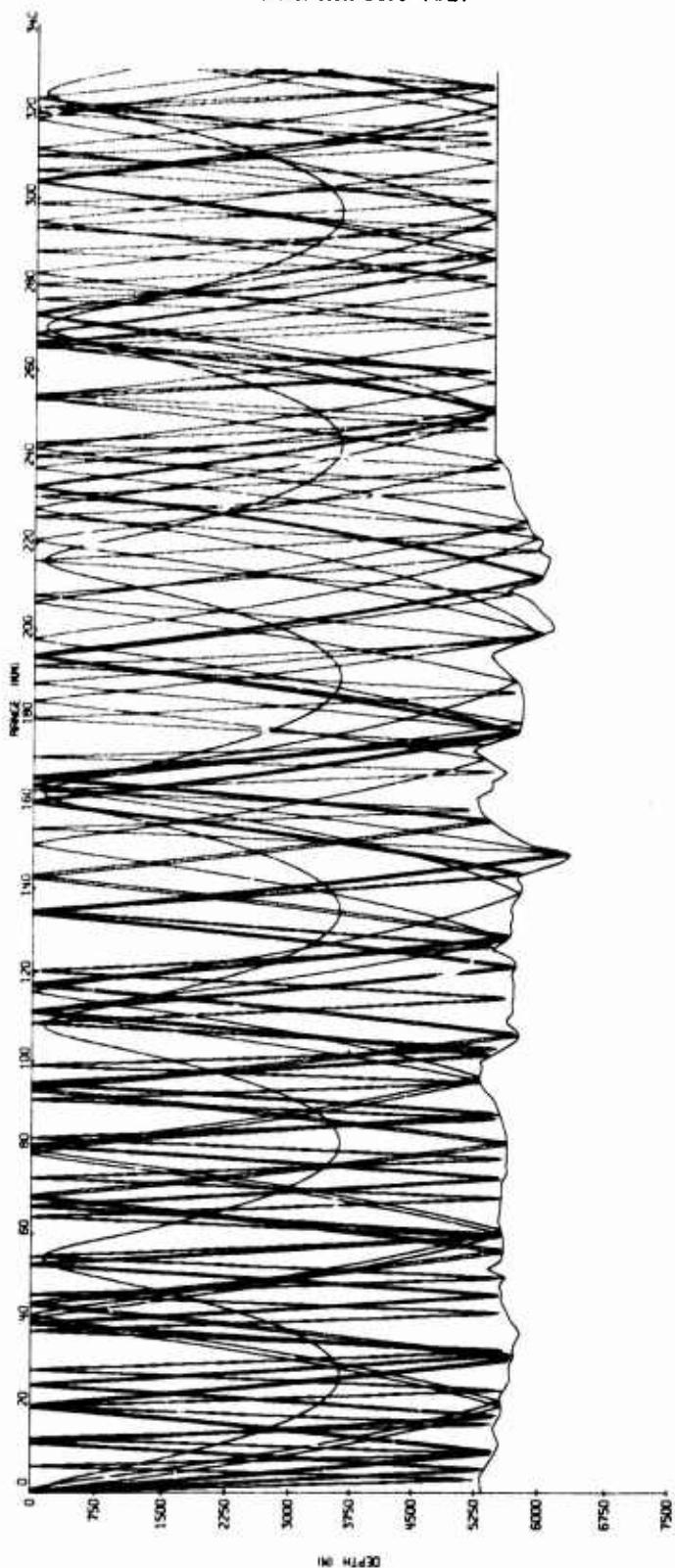


Fig. B4 — Selected rays which were traced (one ray every 15°)

COMPARISON OF EXPERIMENTAL AND CALCULATED RESULTS FOR THERMINI

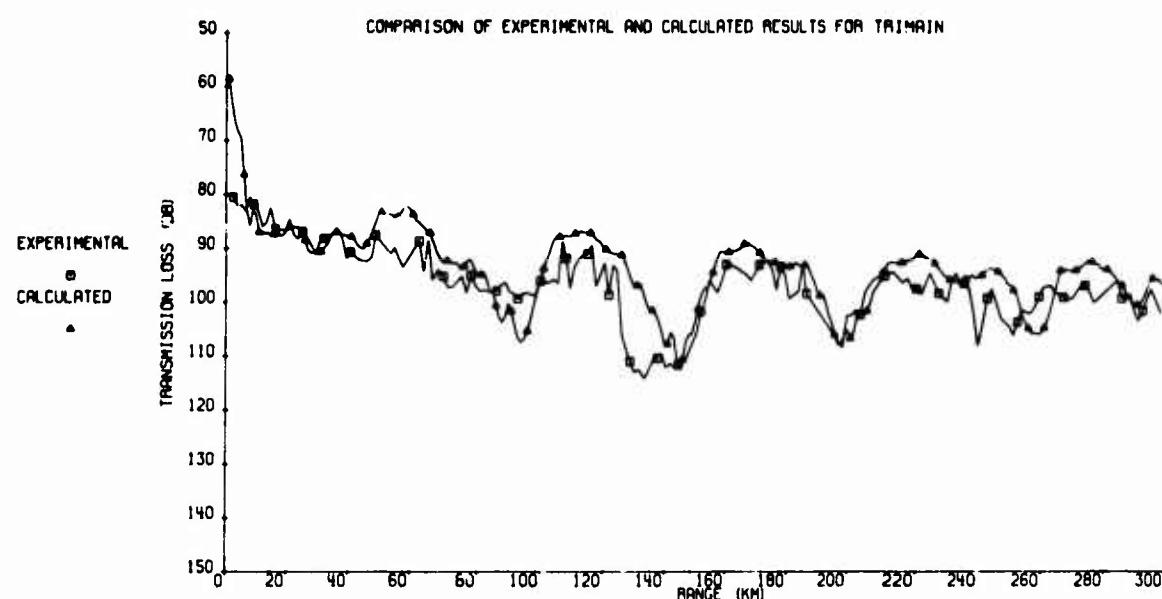


Fig. B5 — Comparison of experimental and calculated intensity values